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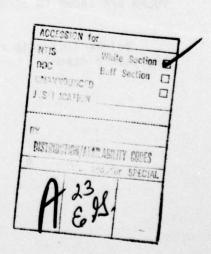
which requires multiple runs, plus subsequent averaging. Typically, VOLAR requires approximately 7 percent of the computer time required for comparable Monte Carlo simulations.

The program includes a general airframe mathematical model suitable for helicopters or fixed-wing aircraft. The airwake of a small ship is also modeled and ship motion models are included. Two alternative models of the human pilot are supplied, one is based on verbal adjustment rules, the other is based on optimal control theory, utilizing performance index parameters deduced from manned simulator experiments. The program is demonstrated for AV-8A recovery on a small ship. The trends predicted by VOLAR are shown to agree with flight test data.

FOREWORD

The work described in this report was sponsored by the Flight Dynamics Branch of Air Vehicle Technology Department of the Naval Air Development Center. Mr. Ronald L. Nave served as project engineer and technical monitor for the Naval Air Development Center Mr. Carmen J. Mazza was NADC program manager.

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SUMMARY

A digital computer program has been developed for simulating the launch and recovery of VSTOL aircraft operating from small ships. The program, known as VOLAR (Vought Launch and Recovery Dynamics Program), employs the computational technique of nonlinear covariance propagation. This permits the time histories of the means and variances of all system state variables to be computed from a single run, as opposed to the Monte Carlo technique, which requires multiple runs, plus subsequent averaging. Typically, VOLAR requires approximately 7 percent of the computer time required for comparable Monte Carlo simulations.

The program includes a general airframe mathematical model suitable for helicopters or fixed-wing aircraft. The airwake of a small ship is also modeled and ship motion models are included. Two alternative models of the human pilot are supplied, one is based on verbal adjustment rules, the other is based on optimal control theory, utilizing performance index parameters deduced from manned simulator experiments. The program is demonstrated for AV-8A recovery on a small ship. The trends predicted by VOLAR are shown to agree with flight test data.

Volume I of this report describes the program, Volume II is the user's manual.

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APPENDIX A

USER'S MANUAL

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APPENDIX A USER'S MANUAL

A.1 Philosophy

VOLAR is designed to be a useful analytical tool for any task involving covariance propagation. It definitely is not limited or restricted to the examples presented in this user's guide. VOLAR is not a simple routine to learn, but once mastered it provides the familiar user with a powerful analytical tool. The intended user should have knowledge of differential equations, matrix algebra, aerodynamics, modeling, control system analysis and synthesis, and Fortran programming.

VOLAR is a relatively flexible program. The basic structure allows one to tailor the routine to his/her particular need or requirement. Then once a problem is run, the user may select from several types of output; including line printer, printer plots, CalComp plots and punch cards.

The program is written in Fortran IV and COMPASS for CDC 6000 or CYBER series computers. Each COMPASS subroutine has a Fortran equivalent.

The subroutines include many comment statements; and for some users, will serve as their own best user's guide. Great care was taken to program in a simple concise manner. When complex programming appears, the authors felt it was necessary due to speed and/or efficiency considerations.

A.2 Some Comments on the Use of VOLAR

The user's guide should be regarded as just that - a guide. VOLAR cannot be completely learned from a book. The prospective user must get hands-on experience. It is highly recommended that VOLAR be activated and exercised thoroughly. The two sample problems presented in this document provide a good starting point.

The first step in the learning process is to review the general purpose and function of each subroutine (Section A.3). Next, the user should read Section A.4 which introduces the I and R arrays and then become familiar with the main program, VOLAR, and its options (Section A.5). After this, select one of the sample cases and compare the problem-specific programming (refer to Appendices B and C) in the subroutines (particularly DEQU, PROP, and SETUP) with the general descriptions in Section A.3. The explanation of the input decks in Section A.8 or Section A.9 is next. Following this,

activate VOLAR on your system. After running the sample cases, try changing a gain or time constant; CalComp plot a new variable: or change output forms. The important point is; roll up your sleeves and dig in.

A.3 Description of Subroutines

This section presents a brief description of the subroutines. There are basically two types of subroutines. The first type falls into the broad category of "support". These subroutines perform canned operations (e.g. matrix multiplication, integration, etc.) and do not change from problem to problem. The second type of subroutine is very much problem dependent. Through these subroutines the user tailors VOLAR to model and solve his particular problem. Subroutines requiring user interface are so noted in the descriptions which follow.

- ADAMS This subroutine performs second order Adams integration. It is the simplest of the three integration techniques available to the user.

 All the integration subroutines are constructed to integrate a set of first order differential equations describing the means and three covariance matrices (three are required when an optimal pilot is used). The calling routine is VOLAR.
- AIRWAKE This subroutine calculates airwake disturbance, means and standard deviations, due to the ship's presence. The programmed equations are from Reference 12. The calling routine is DEQU.
- AIRWTBL The airwake data tables of Reference 12 are contained here in DATA statements. This subroutine is called once by SETUP to construct a case-particular particular (V_{WOD}, \(\frac{\psi}{\text{WOD}}\)) set of airwake tables to be used by AIRWAKE.

AXIS - This subroutine produces a coordinate axis for CalComp plots. The calling routine is CALPLT.

CALPLT - This is a general purpose CalComp plot routine.

The calling program is VOLAR.

DASPLT - This subroutine draws dashed lines on CalComp plots. The calling routine is CALPLT.

DEQU - This subroutine contains the differential equations describing the propagation of the means, the aero data table look ups and open loop control inputs. The reference flight values about which the trajectory is linearized are defined and updated here. DEQU is one of the user defined subroutines. It must be programmed by the user to meet the requirements of his particular application. DEQU is called by SETUP and the integration subroutines ADAMS, RUNGE, and KUTTA.

DESCRIB - This routine calculates single-valued nonlinear describing functions of one variable. TABRD must be called before the first call to DESCRIB.

The calling routine for DESCRIB is DEQU.

ELLIPSE - This routine draws a 50 percent probability ellipse on CalComp trajectories. These ellipses can be scaled differently from the trajectory to increase the clarity of presentation. The calling routine is CALPLT.

 ERF - This routine evaluates the error function associated with the normal distribution curve.
 The calling routine is DESCRIB.

KUTTA - One of three integration subroutines. This subroutine performs third order Runge-Kutta integration. The calling program is VOLAR. MATINV - This subroutine calculates the inverse of a matrix. The calling routine is SOLVR.

MATRIX - This routine handles general matrix operations.

The operations include adding two matrices, subtracting two matrices, multiplying two matrices, multiplying one matrix by the transpose of another matrix, matrix transposition, and laying a matrix into another matrix. MATRIX is programmed in COMPASS. The FORTRAN equivalent operations appear as comments in MATRIX. The COMPASS version executes about 20 percent faster than the FORTRAN version. The calling routines are PROP and SOLVR.

MISCAL - This subroutine handles miscellaneous calculations that have no logical place to go. MISCAL is called by VOLAR before the output file is written. This subroutine is user specified.

PRNPLT - This is a general purpose line-printer plot routine.

A 7 by 7 inch plot is produced. The calling routine is VOLAR.

PROP - This subroutine contains the matrix differential equation for covariance propagation. The user must define the elements of the F and G matrices in PROP. These matrices define the linearized system equations and are normally composed of several smaller submatrices. PROP is called by SETUP and the integration subroutines ADAMS, RUNGE, and KUTTA.

ROTATE - This subroutine rotates a coordinate system through any angle. The calling routines are CALPLT and ELLIPSE.

- RUNGE This subroutine performs fourth order Runge-Kutta integration. It is the more accurate but most time-consuming of the three integration methods available in VOLAR. The calling program is VOLAR.
- SETUP This subroutine initializes the integrators.

 Any calculations to be initialized and one-timeonly calculations also appear in SETUP. For
 example, ship scaling factors and wind over deck
 are calculated here because they are fixed for
 a given run. Because of its problem dependence,
 SETUP is user defined. SETUP is called by
 VOLAR.
- SOLVR This subroutine solves for the steady-state (t→∞) solution of the matrix Riccati equation. It may be used to initialize the covariance matrix, P, before running a time history. It will not work when more than one covariance matrix (e.g. the optimal pilot model case) is involved. The calling routine is PROP.
- TABRD This subroutine decomposes nonlinear functions into even and odd describing function elements. The inputs to TABRD are a table of independent variables, a table of dependent variables, and the number of variables in the tables. TABRD must be called once for each nonlinear element before DESCRIB can calculate the appropriate describing function. The calling routine is SETUP.

- TLU This routine is used to look up a series of dependent variables. Linear interpolation is used to generate the dependent variables. With one call, several dependent variables can be made available to COMMON provided that all the dependent variable tables are associated with the same independent variable table. The calling subroutines are DEOU and PROP.
- VOLAR This routine is the main program and handles almost all the program input and output through its various options.

A.4 Description of the I and R Arrays

The I and R arrays contain all the integer and real variables of the program respectively. The I array is equivalenced to the elements of the labeled common, "INTEGER". The R array is equivalenced to elements of blank common. The arrays not only handle the communication between the subroutines but also all of the programs input and output. The I and R arrays are user defined.

A.4.1 Program Modification

If the user wishes to modify the program, any new variables would be added to the common blocks (I or R arrays). This gives the user the capability of inputting or outputting the variables. The new variables may be added any where within the commons.

A.4.2 Input and Output through the I and R Arrays

All of the programs input and output were designed around the I and R arrays. Since the I and R arrays (common blocks) have many variables and arrays within them, bookkeeping the variables is difficult. To simply the bookkeeping, the I and R arrays are divided into segments and elements. Each segment is defined by a specific number of elements. The segments are classified by groups of elements which are defined by a collection of simple variables or subscripted variables. The lengths of the segments are specified in the problem initialization phase (A.5.1). The initialization phase actually

aligns the commons with the I and R arrays. Care must be taken in setting the lengths of the segments after program modification because the input and output will be malaligned. Figure A.1 is an example of a simple R array. In this example, DTOUT may be referred to as segment 1, element 4. The fifth element of TABV2 is segment 3, element 5. Once the user has established the order of variables in the R array, then each variable may be referred to by its segment number and element number within that segment. This facilitates input/output and simplifies modifications to the program. Understanding the concept of the I and R arrays is extremely important to the use of VOLAR.

CØMMØN TIME, TØ, DTIME, DTØUT, DTØUT2, TMAX
CØMMØN TABV1(6), TABV2(10)

Variable	Segment No.	Element No.
TIME	1	1
TØ	sering weeks to the series of the series	2
DTIME	mana af i ellare de la	3
DTØUT	1	4
DTØUT2	1	5
TMAX	salysk sai l ees all viide	6
TABV1	2	1-6
TABV2	3	1-10

Figure A.1

Appendix E presents the variables in the R and I arrays for the analysis reported in this document.

A.5 The Main Program (Description of Options)

The program is divided into two input phases. The first phase is program initialization which defines the lengths for the R and I arrays. The second phase is user defined and directs the program through the various program options.

A.5.1 Program Initialization (Phase I)

Definition of the R and I array lengths are input through the following namelist. The lengths of the segments, defined in the program input, must be compatible with the number of variables in blank and labeled COMMON. The segment lengths allow the main program to bookkeep the absolute location of a variable in COMMON.

1		2 - 80	
	\$SEGMNT NSEGI=	, NSEGR=, NPRNT=,	
1		2 - 80	
	NI(1)=,,_		
1		2 - 80	
	NR(1)=,,	_,	
1	1201.0	2 - 80	
	\$END		

where:

NSEGI - Number of segments in the I array.

NSEGR - Number of segments in the R array.

NPRNT - Print option to display the segments and elements.

NPRNT = 0 - No print.

NPRNT # 0 - Print.

NI - Array containing the number of elements in each I array segment.

NR - Array containing the number of elements in each R array segment.

NOTE: See paragraph A.5.3.1 for a sample input.

A.5.2 Program Options (Phase II)

The program is divided into 28 options to handle problem execution, input, and output. The definition of the options are as follows:

<u>Option</u>	<u>Task</u>
1	Write I and R array I/O instructions on a file.
2	Store data into the I array and write I array data on a file.
3	Print data from the I array.
4	Store data into the R array and write R array data on a file.
5	Print data from the R array.
6	Setup the differential equations.
7	Designate the time history variables from the R array to be written to a file by option 21.
8-9	Inactive.
10	Read data from input and generate a file compatible for options 14, 15, 17, or 18.
11	Store tabulating or punching instructions on a file. The file will be used in option 14 or 15.
12	Store printer plotter instructions on a file. The file will be used by option 17.
13	Store CalComp plotter instructions on a file. The file will be used by option 18.
14	Print the time history output in a tabular form.
15	Punch cards from the time history output.
16	Inactive.
17	Plot the time history output on the printer.
18	Plot the time history output on a CalComp plotter.
19	Print the contents of a file in blocked form.
20	Inactive.
21	Generate a time history.
22-27	Inactive.
28	Store the R array on Tape 28 or retrieve the R array from Tape 28.

A.5.2.1 Option 1 - Write I and R array I/O instructions on a file

1.	1-5	6-10	11-80	
	NØPT		LBLØUT	

Input the following card if I < 0.

4.	1-40	41-80	
	FMTI	FMTØ	

where:

NOPT	- (Option number (input a 1 for this option).	(15)
LBLØUT	- 1	Description of option.	(7A10)
NLIST	-	File where the instructions will be written.	(15)
I	- 1	Beginning segment number of the I or R array.	(15)
J	- 1	Beginning element number of the I or R array.	(15)
K	-	Ending segment number of the I or R array.	(15)
L	- 1	Ending element number of the I or R array.	(15)
LABEL		Variable names for the elements defined between 1,J and K,L.	(5A10)
SCALE		Scale factor to be applied to the elements. Default is one.	(E10.3)
FMTI	-	Variable input format.	(4A10)
FMTØ	- '	Variable output format	(4A10)

NOTE:

- 1. Multiple sets of cards 3 and 4 may be input.
- 2. FMTI and FMTØ are input only if I < 0.
- 3. Option 1 is terminated when a blank card is input for I, J, K, L.
- 4. See Paragraph A.5.3.2 for a sample input.

A.5.2.2 Option 2 - Store data into the I array

1.	1-5	6-10		11-80	
	NØPT		LBLØUT		

Input the following cards if NLIST = 5.

3.	1-5	6-10	11-15	16-20	21-70	71-80
	I	J	К	:	LABEL	SCALE

Input the following card if I < 0.

4.	1-40	41-80	
	FMTI	FMTØ	

5.	1-5	6-10	11-15	76-80
	IN(K+I)	IN(K+I+1)	IN(K+I+2)	 IN(J+L)

where:

NDATA		File containing I array data.	(15)
NPF	-	File to be created containing I array data. If NPF = 0, no file is created.	(15)
I	-	Beginning segment number of the I array.	(15)
J	-	Beginning element number of the I array.	(15)
K	-	Ending segment number of the I array.	(15)
L	-	Ending element number of the I array.	(15)
LABEL	•	Variable names for the elements defined between I,J and K,L.	(5A10)
SCALE		Scale factor to be applied to the elements in the I array between I,J and K,L.	(E10.3)
FMTI	-	Variable input format.	(4A10)
FMTØ	-	Variable output format.	(4A10)
IN	•	I array elements (Default is 1615 and may be changed to FMTI).	

NOTE:

- 1. Multiple sets of cards 3, 4 and 5 may be input.
- The format for card 5 may be changed by specifying a negative I on card 3 and inputting the format on card 4.
- 3. If NLIST and NDATA are not equal to 5, cards 3, 4, and 5 are input from files NLIST and NDATA.
- Option 2 is terminated when a blank card is input for I,J,K,L.
- 5. See Paragraph A.5.3.3 for a sample input.

A.5.2.3 Option 3 - Print from the I array

1.	1-5	6-10		11-80	
	NØPT		LBLØUT	Y-02-17 4-7%	

2. 1-5 NLIST

Input the following cards if NLIST = 5.

3.	1-5	6-10	11-15	16-20	21-70	71-80
	I	J	К	L	LABEL	SCALE

Input the following card if I < 0.

4. 1-40 FMTØ

- Option number (input a 3 for this option).

where:

NØPT

LBLØUT	-	Option description.	(7A10)
NLIST	-	File where print instructions reside.	(15)
I	-	Beginning segment number of the I array.	(15)
J	-	Beginning element number of the I array.	(15)
K		Ending segment rumber of the I array.	(15)
L		Ending element number of the I array.	(15)
LABEL	-	Variable names for the elements defined between I,J and K,L.	(5A10)
SCALE		Scale factor to be applied to the I array elements between I,J and K,L when printed. Default is one.	(E10.3)
FMTØ	-	Variable output format.	(4A1C)

(15)

NOTE:

- 1. Multiple sets of cards 3 and 4 may be input.
- The print format may be changed by specifying a negative I and inputting the format on card 4.
 The format is maintained until it is reset or another option is specified.
- The option is terminated when a blank card is input for I,J,K,L.
- 4. See Paragraph A.5.3.4 for a sample input.
- A.5.2.4 Option 4 Store data into the R array, and write the R array on to a file

 - 2. 1-5 6-10 11-15 NLIST NDATA NPF

Input the following 2 cards if NLIST = 5.

3. 1-5 6-10 11-15 16-20 21-70 71-80 I J K L LABEL SCALE

Input the following card if I < 0.

4. 1-40 41-80 FMTØ

Input the following card if NDATA = 5.

where:

NØPT	-	Option number (input a 4 for this option).	(15)
LBLØUT	-	Option description.	(7A10)
NLIST	-	File containing input instructions.	(15)
NDATA	-	File containing R array data.	(15)
NPF	•	File containing R array data is to be created. If NPF = 0, no file is created.	(15)
I	-	Beginning segment number of the R array.	(15)
J		Beginning element number of the R array.	(15)
K	-	Ending segment number of the R array.	(15)
L	-	Ending element number of the R array.	(15)
LABEL	-	Variable names for the elements defined between I,J and K,L.	(5A10)
SCALE	-	Scale factor to be applied to the R array elements between I,J and K,L. Default is one.	(E10.3)
FMTI	-	Variable input format.	(4A10)
FMTØ	-	Variable output format.	(4/10)
R	-	R array elements (Default is 8F10.3 and may be changed to FMTI).	

NOTE:

- The format for card 5 may be changed by specifying a negative I on card 3, and inputting the format on card 4. The format is maintained until it is reset or another option is specified.
- 2. If NLIST and NDATA are not equal to 5, cards 3, 4, and 5 are input from files NLIST and NDATA.
- 3. Multiple sets of cards 3, 4, and 5 may be input.
- Option 4 is terminated when a blank card is input for I,J,K,L.
- 5. See Paragraph A.5.3.5 for a sample input.

A.5.2.5 Option 5 - Print from the R array.

1.	1-5	6-10	11-80	
	NØPT		LBLØUT	

2. 1-5 NTAP

Input the following cards if NTAP = 5.

3.	1-5	6-10	11-15	1€-20	21-70	71-80
	I	J	K	L	LABEL	SCALE

Input the following card if I < 0.

4. 1-40 FMTØ

where:

NØPT	-	Option number (input a 5 for this option).	(15)
LBLØUT	-	Option description.	(7A10)
NTAP	-	File where write instructions reside.	(15)
1	-	Beginning segment number of the R array.	(15)
J	-	Beginning element number of the R array.	(15)
K	-	Ending segment number of the R array.	(15)
L	-	Ending element number of the R array.	(15)
LABEL	-	Variable names for the elements defined between I,J and K,L.	(5A10)
SCALE	-	Scale factor to be applied to the R array elements when printed. Default is one.	(E10.3)
FMT0		Variable output format.	(4A10)

NOTE:

- 1. If NTAP is not equal to 5, cards 3 and 4 are input from file NTAP.
- 2. The default print format of (7F14.5) may be changed to FMTØ by specifying a negative I and inputting the new format. The new format remains in effect until reset or a new option is input.
- 3. Multiple sets of cards 3 and 4 may be input.
- Option 5 is terminated by inputting a blank card for I,J,K,L.
- 5. See Paragraph A.5.3.6 for a sample input.
- A.5.2.6 Option 6 Set up differential equations.

This option is composed of five groups of data:

- 1. Derivative indices.
- 2. State indices.
- 3. PDØT and P indices.
- 4. PEDØT and PE indices.
- 5. PXDØT and PX indices.

Groups 3, 4, and 5 above must be input in the order specified. Each group of data is composed of cards 2 and 3 below.

1.	1-5	6-10	1	1-80	
	NØPT		LBLØUT		

2.	1-5	6-10	
	M	N	

3.	1-5	6-10	11-15	16-20	21-70	36
	I	J	K	L	LABEL	

where:

NØPT	-	Option number (input a 6 for this option).	(15)
LBLØUT	-	Option description.	(7A10)
М	-	The segment number of the I array where the R array location of the differential equation elements will be stored.	(15)
N	-	The element number of the I array where the R array location of the differential equation elements will be stored.	(15)
I	-	Beginning segment number of the R array where the differential equation elements will be stored.	(15)
J	•	Beginning element number of the R array where the differential equation elements will be stored.	(15)
K	-	Ending segment number of the R array where the differential equation elements will be stored.	(15)
L	•	Erding segment number of the R array where the differential equation elements will be stored.	(15)
LABEL	-	Variable names for the elements defined between I,J and K,L.	(5A10)

NOTE:

- 1. Multiple sets of card 3 may be specified.
- 2. Each group of indices will be terminated when a blank card is specified for I,J,K,L.
- 3. PDØT and P indices are defined by I,J and K,L respectively.
- 4. PEDØT and PE indices are defined by I,J and K,L respectively.
- 5. PXDØT and PX indices are defined by I,J and K,1 respectively.
- 6. See Paragraph A.5.3.7 for a sample input.

A.5.2.7 Option 7 - Designate the time history variables to be output

1.	1-5 6-10		11-80			
	NØPT		LBLØUT			

2.	1-5	€-10	11-15	16-20	21-70	
	I	J	K	L	LABEL	

where:

NØPT	-	Option number (input a 7 for this option).	(15)
LBLØUT	-	Option description.	(7A10)
I	-	Beginning segment number of the R array to be output.	(15)
J	•	Beginning element number of the R array to be output.	(15)
K	•	Ending segment number of the R array to be output.	(15)
L		Ending element number of the R array to be output.	(15)
LABEL	-	Variable names for the elements defined between I.J and K.L.	(5A10)

NOTE:

- 1. Multiple sets of card 2 may be input
- Option 7 is terminated when a blank card for I,J,K,L is input.
- 3. See Paragraph A.5.3.8 for a sample input.

A.5.2.8 Option 10 - Read data from input and generate a file compatible for options 14, 15, 17, and 18.

1.	1-5	6-10	11-80
	NØPT		LBLØUT

Input the following card K1 times.

4.	1-10	11-20	21-30	71-80
	RØW(1)	RØW(2)	RØW(3)	RØW(K2)

where:

L = 0 - Number of data points equal to the number of rows.

L ≠ 0 - First data point indicates the number of data points in a floating point number.

RØW - Data point array.

NOTE:

1. See Paragraph A.5.3.9 for a sample input.

A.5.2.9 Option 11 - Store tabulating or punching instructions on a file

A. Cards for tabulating instructions.

1.	1-5	6-10		11-80		
	NØPT		LBLØUT			

Input the following card K1 times.

4.	1-5	6-10	11-20	21-70	71-80
	NTAP	K2	L	LABEL	SCALE

B. Cards for punching instructions.

1.	1-5	6-10		11-80	
	NØPT		LBLOUT		

where:

NØPT	-	Option number (input an 11 for this option).	(15)
LBLØUT	-	Option description.		(7A10)
NLIST	-	File where instructions will be written.		(15)
I	-	Punching instruction flag.		(15)
		I = 0 - Tabulating instruction.		
		I ≠ 0 - Punching instruction.		
K1	-	Number of columns for tabulated data (Maximum = 10).		(!5)
TITLE	-	Title for tabulated data.		(7A10)
NTAP	-	File where the instructions will reside.		(15)
K2	-	Data column to be tabulated or punched.		(15)
L	-	Column heading.		(A10)
LABEL	-	Variable description.		(5A10)
SCALE	-	Scale factor to be applied to the data (Default-1.0).		(E10.3)

NOTE:

- 1. K2 is the sequential number for the variable as ordered in option 7.
- For tabulating instructions, multiple sets of cards 3 and 4 may be input. The option is terminated when a blank card is input for K1.
- For punching instructions, a multiple set of card 3 may be input. The option is terminated wher a blank card for NTAP and K2 is input.
- 4. The file NLIST will be used in option 14 or 15.
- 5. See Paragraph A.5.3.10 for a sample input.

A.5.2.10 Option 12 - Store printer plot instructions on a file.

- 1. 1-5 6-10 11-80 NØPT LBLØUT
- 2. 1-5 NLIST
- 3. 1-5 K1

Input the following cards K1 times.

- 4. 1-80 TITLE
- 5. 1-80
- 6. 1-80 TITLE
- 7. 1-5 6-10 11-20 21-30 31-40 41-50 51-60 61-70 NCURVS XPLØT YPLØT DELX DELY STARTX STARTY
- 8. 1-40 41-80 FMTØ

Input the following cards NCURVS times.

9. 1-40 41-45 46-50 51-55 56-57 58 59-60 61-70 71-80
LABEL NDATA NCØLX NCØLY NSYM SCALEX SCALEY

where:

NØPT		Option number (input a 12 for this option).	(15)
LBLØUT	-	Option description.	(7A10)
NLIST	-	File where instructions will be written.	(15)
K1	-	Number of plots.	(15)
TITLE	-	Three card plot title.	(8A10)
NCURVS	•	Number of curves per plot.	(15)
XPLØT		Number of inches from left paper margin to the left end of the X axis.	(F10.3)
YPLØT		Number of inches from top of the paper to the bottom of the Y axis.	(F10.3)
DELX	-	Increment per inch on the X axis.	(F10.3)
DELY	-	Increment per inch on the Y axis.	(F10.3)
STARTX	-	X value at axis intersection.	(F10.3)
STARTY	•	Y value at axis intersection.	(F10.3)
FMTI	-	Label on X axis.	(AA10)
FMTØ		Label on Y axis.	(4A10)
LABEL	-	Legend associated with a curve.	(4A10)
NDATA	-	File where data for the curve is located.	(15)
NCØLX	•	Column number on the file where the X data is located.	(15)
NCØLY	•	Column number on the file where the Y data is located.	(15)
NSYM	-	Plotting symbol.	(A1)
SCALEX	-	Scale factor to be applied to the X data (Default = 1.0).	(F10.3)
SCALEY	-	Scale factor to be applied to the Y data (Default = 1.0).	(F10.3)

NOTE:

1. See Paragraph A.5.3.11 for a sample input.

A.5.2.11		13	-	Store	CalComp	plotting	instructions	on	a
	file								

1.	1-5	6-10		11-80	
	NØPT		LBLØUT		

Input the following cards K1 times.

Input the following four cards if bit zero of ISOPT is one.

11.	1-80
	TITLE
12.	1-80
	TITLE
13.	1-80
	TITLE
Input th	e following card if bit one of ISØPT is one.
14.	1-40
	LABELX
Input the	e following card if bit two of ISØPT is one.
15.	1-40
	LABELY
	Call the second of the second
Input the	e following card if bit three of ISØPT is one.
16.	1-40
	LEGEND
Input th	e next five cards if bit four of ISØPT is one.
17.	1-10 11-20
19663	X Y
18.	1-80
	TITLE
19.	1-80
	TITLE TERRETORS AND RESIDENCE THAT THE TERRETORS ASSESSED.
20.	1-80
	TITLE

21.	1-80	
	TITLE	
Input the fo	llowing cards NCURVS times.	
22.	2-80	
	\$CURVE NDATA=, NCØLX=, NCØLY=, NCX=	, 7
23.	1 2-80	
	NCY=, NCXY=, LINTYP=, DASH=,	21 552
24.	2-80	
	NSYM=, SCALEX=, SCALEY=, SCALXX=,	\neg
25.	1 2-80	
	SCALYY= \$END	
26.	1-6 7-10 11-50	
	K LABEL	
where:		
NØPT	- Option number (input a 13 for this option).	(15)
LBLØUT	- Option description.	(7A10)
PCØDE	- CalComp plot code.	(A10)
NTAP	- File produced by CalComp.	(A10)
NLIST	 File where plotting instructions will be written. 	(15)
K1	- Number of plots to be produced.	(15)
L	- Indicator for plotting on centimeter paper.	(A4)

- Number of curves per plot

NCURVS

ANGLE	-	Plot rotation angle in degrees (0 or 90 degrees).	
XPLØT	-	Distance in inches for which the origin of the plot is to be moved in the X direction.	
YPLØT	•	Distance in inches for which the origin of the plot is to be moved in the Y direction.	
XEXIT	-	Final pen movement in the X direction.	
YEXIT	-	Final pen movement in the Y direction.	
XLEGNI	0 -	X coordinate of the plot legend in inches.	
YLEGN) -	Y coordinate of the plot legend in inches.	
XØRG	•	X value at which axes intercept.	
YØRG		Y value at which axes intercept.	
LNGTH)	x -	Length of X axis in inches.	
LNGTHY		Length of Y axis in inches.	
START	x -	Initial value on the X axis.	
STARTY	· -	Initial value on the Y axis.	
DELX	-	Increment per inch on the X axis.	
DELY		Increment per inch on the Y axis.	
ISØPT		Bit array for read option. See Figure A.4.	
		BIT(0) = 1 - Read title to be centered over plot.	
		BIT(1) = 1 - Read X axis label.	
		BIT(2) = 1 - Read Y axis label.	
		BIT(3) = 1 - Read legend title.	
		BIT(4) = 1 - Read coordinates of the title and the title.	
TITLE	-	Four card title.	(8A10)
LABEL	x -	X axis label.	(4A10)
LABELY	· -	Y axis label.	(4A10)
LEGEN) -	Legend for the curve.	(4A10)

X	-	X coordinate for the title.	(F10.3)
Y	-	Y coordinate for the title.	(F10.3)
NDATA	-	File where data to be plotted is located.	
NCØLX	-	Column number on the file where the X data is located.	
NCØLY	-	Column number on the file where the Y data is located.	
NCX	-	Column number where the X elliptical axis data is located.	
NCY	-	Column number where the Y elliptical axis data is located.	
LINTYP	-	Line type for plot.	
		LINTYP = Zero, line only (no symbol)	
		LINTYP = Negative, symbol only (no line)	
		LINTYP = Positive, both line and symbol	
DASH	-	Length of plotting segments for dashed line in inches. See Table A.1.	
NSYM	-	CalComp symbol code (99 if ellipse).	
SCALEX	-	Scale factor for the X data (Default = 1.0).	
SCALEY	-	Scale factor for the Y data (Default = 1.0).	
SCALXX	·	Scale factor for the X elliptical axis (Default = SCALEX).	
SCALYY	-	Scale factor for the Y elliptical axis (Default = SCALEY).	
K	-	Line style. See Table A.1.	(06)
LABEL	-	Legend for line style.	(4A10)

NOTE:

- 1. See Paragraph A.5.3.12 for a sample input.
- 2. See Figure A.3 for a plot of ellipses of probability.
- 3. See Figure A.2 for a diagram of plotting variables.

Table A.1

LINE	LSTYLE	DASH
	177610	.01
	177610	.05
	177430	.01
	177430	.05
	177070	.01
	177070	.05
	177774	.01
	177774	.05
	177400	-01
	177400	.05
	177752	.01
	177752	.05
	177714	.01
	177714	.05
	125452	-01
	125452	.05
	170360	-01
	170360	-05
	177744	-01
	177744	-05
	177444	.01
	177444	-05
******************************	146314	-01
	146314	-05
	176314	-01
	176314	-05
	177777	ANY

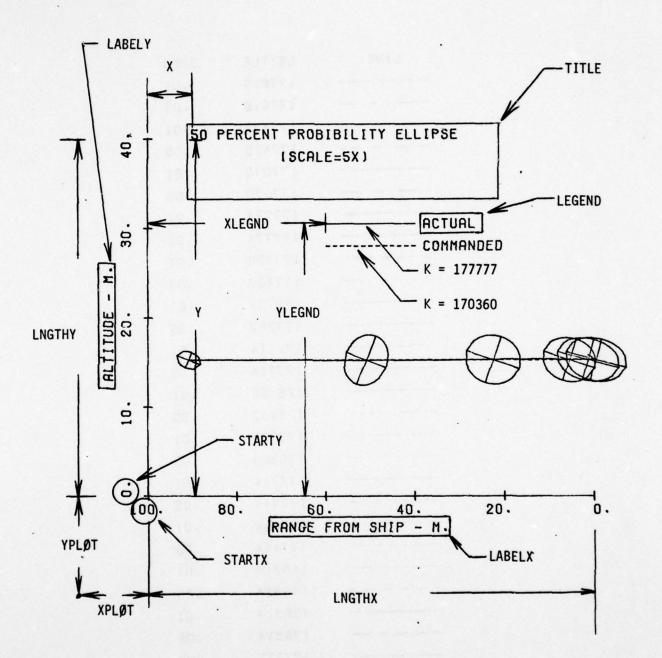


Figure A.2

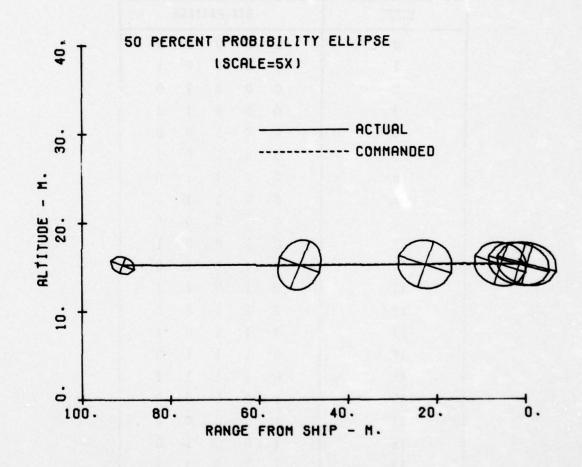


Figure A.3 Example of Probability Ellipses

60 BITS/WORD	
BITS 59 - 6	BITS 5 - 0

Seatonic Control

-

N

BIT #	4	3	2	1	0
VALUE	24	23	22	21	20

ISØPT		В	T PA	TTER	N	
0	0	0	0	0	0	O
1	0	0	0	0	1	
2	0	0	0	1	0	
3	0	0	0	1	1	
4	0	0	1	0	0	
5	0	0	1	0	1	
6	0	0	1	1	0	
7	0	0	1	1	1	
8	0	1	0	0	0	
9	0	1	0	0	1	
10	0	1	0	1	0	
11	0	1	0	1	1	
12	0	1	1	0	0	
13	0	1	1	0	1	
14	0	1	1	1	0	
15	0	1	1	1	1	
16	1	0	0	0	0	
17	1	0	0	0	1	
18	1	0	0	1	0	
19	1	0	0	1	1	
20	1	0	1	0	0	
21	1	0	1	0	1	
22	1	0	1	1	0	

Figure A.4

A.5.2.12 Option 14 - Print the time history in a tabular form

1.	1-5	6-10	11-80	
	NØPT		LBLØUT	

where:

NOTE:

- 1. File NLIST is generated by option 11.
- 2. See Paragraph A.5.3.13 for a sample input.

A.5.2.13 Option 15 - Punch the time history

1.	1-5	6-10	11-80	
	NØPT		LBLØUT	

2. 1-5 NLIST

where:

NOTE:

- 1. File NLIST is generated by Option 11.
- 2. See Paragraph A.5.3.14 for a sample input.

A.5.2.14 Option 17 - Produce a printer plot of the time history

Input the following cards if NLIST = 5.

3. 1-5 NPLØTS

Input the following cards NPLØTS times.

- 4. 1-80 TITLE
- 5. 1-80
 TITLE
- 6. 1-80
- 8. 1-40 41-80 LABELY

Input the following card NCURVS times.

9.	1-40	41-45	46-50	51-55	56-57	58	59-60	61-70	71-80
	LEGEND	NDATA	NCØLX	NCØLY		ISYM		SCALEX	SCALEY

where:

NØPT	-	Option number (input a 17 for this option).	(15)
LBLØUT	-	Option description.	(7A10)
NLIST	-	File where the plotting instructions are located.	(15)
NPRNT	-	Print option to display input.	(15)
		NPRNT = 0 - no print NPRNT = 1 - print	
NPLØTS	-	Number of plots to be produced.	(15)
TITLE	-	Three card plot title.	(8A10)
NCURVS	-	Number of curves per plot.	(15)
XØRG	-	Number of inches from the left paper margin to begin the X axis.	(E10.3)
YØRG	-	Number of inches from the top of the paper margin to begin the Y axis.	(E10.3)
DELX	-	Increment per inch on the X axis.	(E10.3)
DELY	-	Increment per inch on the Y axis.	(E10.3)
STARTX	-	First value on the X axis.	(E10.3)
STARTY	-	First value on the Y axis.	(E10.3)
LABELX	-	X axis label.	(4A10)
LABELY	-	Y axis label.	(4A10)
LEGEND	-	Legend for the curve.	(4A10)
NDATA	Ť	File where the X and Y data are located.	(15)

NCØLX		Column on located.	the	data	file	where	the	X	data	is	(15)
NCØLY	To s	Column on located.	the	data	file	where	the	Y	data	is	(15)

NOTE:

- 1. Cards 3 through 9 may be eliminated by using option 12.
 - 2. See Paragraph A.5.3.15 for a sample input.

A.5.2.15 Option 18 - Produce a CalComp plot of the time history

1.	1-5	6-10	11-80				
	NØPT		LELØUT	List to Court and the			

Input the following cards if NLIST = 5.

Input the following cards NPLØTS times.

6.	1 2-80
	XEXIT=, YEXIT=, XLEGND=, YLEGND=,
7.	2-80
	XØRG=, YØRG=, LNGTHX=, LNGTHY=, STARTX=,
8.	2-80
	STARTY=, DELX=, DELY=, ISØPT=\$END
Input the fol	lowing 4 cards if bit zero of ISØPT is one.
9.	1-80
	TITLE
10.	1-80
	TITLE
11.	1-80
	TITLE
12.	1-80
	TITLE
Input the fol	lowing card if bit one of ISMPT is one.
13.	1-40
	LABELX
Input the fol	lowing card if bit two cf ISØPT is one.
14.	1-40
	LABELY

Input the following card if bit three of ISOPT is one.

15. 1-40 LEGEND

Input the following 5 cards if bit four of ISØPT is one.

- 16. 1-10 11-20 X Y
- 17. 1-80 TITLE
- 18. 1-80 TITLE
- 19. 1-80 TITLE
- 20. 1-80 TITLE

Input the following cards NCURVS times.

24.	1-6	7-10

11-50

LABEL

where:

NØPT	Option number (input an 18 for this option). (I	5)
LBLØUT	Option description. (7	A10)
NLIST	File where the plot instructions are located. (I	5)
NPRNT	Print flag to display input (NPRNT=0, no print) (I	5)
K1	CalComp plot code. (A	10)
NTAP	File where CalComp writes its data. (A	10)
NPLØTS	Number of plots to be produced. (I	5)
I NCURVS	Centimeter plot indicator. (Add I = "C.M." pen movements are in centimeter. Number of curves per plot.	4)
ANGLE	Plot rotation angle in degrees.	
XPLØT	Distance in inches for which the origin of the plot is to be moved in the X direction.	
YPLØT	Distance in inches for which the origin of the plot is to be moved in the Y direction.	
XEXIT	Final pen movement in the X direction in inches.	
YEXIT	Final pen movement in the Y direction in inches.	
XLEGND	X coordinate of the plot legend in inches.	
YLEGND	Y coordinate of the plot legend in inches.	
XØRG	<pre>X value at which axes intercept (Default = 0.0).</pre>	
YØRG	Y value at which axes intercept (Default = 0.0).	
LNGTHX	Length of X axis in inches.	
LNGTHY	Length of Y axis in inches.	

STARTX	-	Initial value on the X axis.	
STARTY	-	Initial value on the Y axis.	
DELX	-	Increment per inch on the X axis.	
DELY	-	Increment per inch on the Y axis.	
ISØPT	-	Bit array for read option. See Figure A.4	
		BIT(0) = 1 - Read title to be centered over plot. BIT(1) = 1 - Pead X axis label. BIT(2) = 1 - Read Y axis label. BIT(3) = 1 - Read legend title. BIT(4) = 1 - Read coordinates of the point and the title.	
TITLE	-	Four card plot title.	(8A10)
LABELX	-	X axis label.	(4A10)
LABELY	-	Y axis label.	(4A10)
LEGEND	-	Legend for the curve.	(4A10)
X	-	X coordinate for plot title.	(F10.0)
Y	-	Y coordinate for plot title.	(F10.0)
NDAT/.	-	File where the plot data is located.	
NCØLX	Í	Column number on the data file where the X data is located.	
NCØLY		Column number on the data file where the Y data is located.	
NCX	-	Column number on the data file where the X elliptical axis data is located.	
NCY	-	Column number on the data file where the Y elliptical axis data is located.	
NCYY	-	Column number on the data file where the cross	

correlation data is located.

LINTYP - Type of line for the plot. LINTYP = zero, line only (no symbol) LINTYP = negative, symbol only (no line) LINTYP = positive, both line and symbol DASH Length of plotting segments for dashed lines in inches. See Table A.1. NSYM CalComp symbol code (99 if ellipse). SCALEX Scale factor to be supplied to the X data (Default = 1.0). Scale factor to be applied to the Y data SCALEY (Default = 1.0). SCALXX Scale factor to be applied to the X elliptical axis (Default = 1.0). SCALYY Scale factor to be applied to the Y elliptical axis (Default = 1.0). $(\emptyset6)$ LSTYLE Line style. See Table A.1. (4A10)LABEL Legend for line style.

NOTE:

- 1. Cards 3 through 24 may be input from file NLIST generated by option 13.
- Ellipses of probability may be plotted by specifying NSYM = 99, NCX, NCY, and NCXY. See Figure A.3 for an example of a plot with ellipses of probability.
- 3. See Paragraph A.5.3.16 for a sample input.
- 4. See Figure A.2 for a diagram of the plot variables.

A.5.2.16 Option 19 - Print the time history in a blocked form

1.	1-5	6-10		11-80				
	NØPT		LBLØUT					

2.	1-5					
	NTAP					1
where:						
NØPT	- Optio	n numbe	r (input	a 19 for	this option).	(15)
LBLØUT		n descr				(7A10
NTAP		to be p				(15)
NOTE:						
1. See	Paragraph	A.5.3.	17 for a	sample in	put.	
A.5.2.17 Opt	tion 21 -	Generat	e a time	history		
1.	1-5	6-10		1	1-80	-
	NØPT		LBLØUT			1
2.				1	-80]
	TITLE			11.0		7
3.				1	80	7
J.	TITLE					1
						7
4.	TITLE			1	80	-
	IIIee					'
5.				1	-80	-
	TITLE					1
6.	1-5	6-10	11-15	16-20	21-25]
	NLIST	NTAP	NDATA	INT	NPRNT	7

Input the following three cards as many times as needed if NLIST = 5.

7.	1-5	6-10	11-15	16-20	21-70	71-80
	I	J	K	L	LABEL	SCALE

Input the following card if I < 0.

8.	1-40	41-80	
	FMTI	FMTØ	

Input the following two cards as many times as needed if NTAP = 5.

10.	1-5	6-10	11-15	16-20	21-70	71-80
	I	J	К	L	LABEL	SCALE

Input the following card if I < 0.

where:

INT	- Integration option.	(15)
	<pre>INT = 1 - Fourth order Runge-Kutta.</pre>	
	<pre>INT = 2 - Third order Runge-Kutta.</pre>	
	<pre>INT = 3 - Second order Adams.</pre>	
NPRNT	- Print the time history as a block of data.	(15)
I	- Beginning segment number of the R array.	(15)
J	- Beginning element number of the R array.	(15)
K	- Ending segment number of the R array.	(15)
L	- Ending element number of the R array.	(15)
LABEL	 Variable names for the elements between I,J and K,L. 	(4A10)
SCALE	 Scale factor to be applied to R array data between I,J and K,L. 	(E10.3)
FMTI	 Variable input format for inputting data into the R array for card 9 above. 	(4A10)
FMTØ	 Variable output format for printing data from the R array. (Default = 7F14.5). 	(4A10)
R	- R array elements.	(F10.3)

NOTE:

- Cards 7, 8, and 9 are input through Option 4. The branch to Option 4 occurs within Option 21 and is invisible to the user. Any R array element may be input through this option. To terminate the read for cards 7, 8, and 9, a blank card for I,J,K,L must be input.
- If NLIST ≠ 5, cards 7 and 8 are input through file NLIST. Card 9 is input through file 5 (INPUT).

- Cards 10 and 11 are input through option 5. These cards print the results of trim and the call to Setup. Any R array elements may be printed at this time. To terminate the read for cards 10 and 11, input a blank card for I,J,K,L.
- If NTAP ≠ 5, input cards 10 and 11 through file NTAP.
- 5. See Paragraph A.5.3.18 for a sample input.

A.5.2.18 Option 28 - Store or retrieve R array data to or from a file (TAPE28)

1.	1-5	6-10	11-80		
	NØPT		LBLØUT		

2. 1-5 K1

3.	1-5	6-10	11-15	16-20	21-70	71-80
	I	J	K	L	LABEL	SCALE

where:

NØPT - Option number (input a 28 for this option). (I5)

LBLØUT - Option description. (7A10)

K1 - Data option flag. (I5)

K1 = 0 - Read data from a file (TAPE28).

 $K1 \neq 0$ - Write data to a file (TAPE28).

- Beginning segment number of the R array to be read/written from/to the file.
- J Beginning element number of the R array to be read/written from/to the file.
- K Ending segment number of the R array to be read/written from/to the file.
- L Ending element number of the R array to be read/written from/to the file. (I5)

LABEL	-	Variable names I,J to K,L.	appearing	between	seaments	(5A10)

SCALE - Scale factor to be applied to the R array. (E10.3)

NOTE:

- 1. Multiple sets of card 3 may be input.
- To terminate option 28, a blank card for I,J,K,L must be input.
- 3. See Paragraph A.5.3.19 for a sample input.

A.5.3 Sample Input for Each Program Option

The following examples are sample inputs for the initialization phase and the program options.

A.5.3.1 Sample of program initialization

SSEGMNT NSEGI=7, NSEGR=143, NPRNT=1, NI(1)=10,0,0,14,14,6, NR(1)=6,17,17,26,18,11,37,66,9,37, NR(13)-14,18,6,10,0,6,19,0,0,10, NR(21)=16,10,10,10,10,0,6,6,6,6,6, NR (31)=6,6,6,6,6,6,6,6,6,6,6,6,6, NR (41)=6,6,6,6,6,6,6,6,0,289, NR(51)-289,289,44,16,50,50,75,75,75,75, NR(61)=75,75,6,6,6,6,6,6,6,6,6,6, NR(71)=6,6,6,6,6,6,6,6,6,6,6,6, NF(81)=36,24,42,49,28,1,1,1,1,24, NF(91)=16,1,1,1,1,1,1,1,1,1,1, NR (101)=1,1,1,1,1,1,12,6,6,6,6 NR(111)=6,6,6,6,6,6,6,6,6,6,6,6,6, NR(121)=6,6,6,6,6,6,6,6,6,6,6,6, NR(131)=6,6,6,6,10,10,10,10,10,4, NR(141)=4,4,4, SEND

A.5.3.2 Sample of Option 1

```
STORE R ARRAY INSTRUCTIONS ON A FILE.
  6
                     WEIGHT, G, IX, IY, IZ, IXZ
  67
                     LM, WM, LTDM
                     TAUD
       9
             7
                 - 9
  7
      28
            7
                 29
                     DMEGAV, KV
  7
                     TAUA, K1, K2, KY, B1, B2
            7
      30
                 35
       1
                                                                           1.688
                            (V TABLE FOR AERO DATA)
13
           13
                     TABV1
                             (TIME TABLE FOR OPEN LOOP INPUTS)
                     TABV2
 14
            14
                 10
20
           20
                 10
                     TARTC
                             (OPEN LOOP THETA)
       1
       1
120
           120
                     TYV
                  6
                     TYP
121
          121
122
       1
          122
                  6
                     TYR
123
          123
                     TYDA
124
       1
          124
                  6
                     TYDR
                     TLV
125
           125
                  6
                    TLP
126
       1
          126
                  6
                    TLR
127
          127
                  6 TLDA
       1
128
          128
129
       1
          129
                    TNV
130
       1
           130
                  6
131
          131
                     TNP
       1
                  6
                    TNR
132
          132
                     THOA
          133
                  6
       1
133
       1
134
           134
                     TNDR
                     TABUB
135
       1
           135
                 10
136
       1
          136
                 10
                     TARWR
                     TXAPP
137
       1
          137
                 10
          138
                 10
                     TZAPP
138
       1
           139
139
                 10
                     TXSP
140
       1
          140
                     TDAIN
                     TDAGUT
141
          141
142
          142
                     TORIN
       1
143
           143
                      TOROUT
                      BLANK CARD FOR READ R
```

A.5.3.3 Sample of Option 2

```
2 READ INTO I ARRAY
5 5 0
1 3 1 6 NSTATES, NPA, NOM, NGM
11 17 4 11
1 7 1 10 NPE, NPX, NOAW, NOINIT
1 1 0 1
BLANK CARD FOR READ I
```

A.5.3.4 Sample of Option 3

PRINT DATA FROM THE I ARRAY

NOT THE I A

A.5.3.5 Sample of Option 4

4		READ	R	(CASE-PARTICULAR INPUT)	
5	5	0			
8	14	8	14	VAMB	1.688
20.					
8	15	8	-15	PSIAMB .	.01745329
150.					
8	10	8	10	V5 (SHIP SPEED)	1.688
20.					*******
8	11	8	11	PSI5 ((SHIP HEADING)	.01745329
30.					
8	3	8	5		
74.71		-7.012		10.495	017/5330
3	15		16	PHI, PSI	.01745329
-1.		0.			
5	10	200	12	SUMFYO, SUMLO, SUMNO	
290.41		0.		0.	
5	17	2	17	YSP	
0.					
5	14	2	14	YAPP	
0.		_			
7	36		37	TL1, TL2	
10.		2.			
16	5	-	6	GAINDA, GAINDR	
1.		1.		BLANK CARD TO TERMINATE OPTION 4	

A.5.3.6 Sample of Option 5

5 PRINT DATA FROM THE R ARRAY
5
2 1 2 5 UDOT, WDOT, QDOT, TDOT, XAPPDOT
-8 1 8 6 ALT, VAIR, UBAS, VBAS, WBAS, ALPHA
(6E20-10)
BLANK CARD TO TERMINATE OPTION 5

A.5.3.7 Sample of Option 6

6 4 2 12		SET	UP DI	FFERENTIAL EQUATIONS
4	1			
2	11	2	17	VOOT, POOT, ROOT, YAPPOOT, PHIDOT, PSIDOT, YSPOOT
12	15	12	18	DA1D,DA2D,DP1D,DR2D
				BLANK CARD TO TERMINATE DERIVATIVES
5	1			
3	11	3	17	VB, PB, RB, YAPP, PHI, PSI, YSP
12	11	12	14	DA1, DA2, DR1, DR2
				BLANK CARD TO TERMINATE STATES
6	1			
52	1	51	1	POOT, P
				BLANK CARD
6	3			
100	1	99	1	PED. PE
			Ī	BLANK CARD
6	5			
104	1	103	1	PXHATD, PXHAT
				BLANK CARD, END OF OPTION 6

A.5.3.8 Sample of Option 7

7		DES	IGNAT	E OUTPUT VARIABLES
1	1	1		TIME
8	1	8	2	ALT, VAIR
3	5	3	6	XAPP, ZAPP
3	14	3	-14	YAPP
3	17	3		YSP
3	15	3		PHI, PSI
12	7	12	8	DA, DR
16	3	16	4	SIGDA, SIGDR
-	11		11	VB
3 8	1	3 8	2	UB, WB
8	27	8	29	XM, YM, ZM
. 8	30	9	32	PSIA, THETAA, PHIA
8	33	8		SIGMAVX, SIGMAVY, SIGMAVZ
8	39	8	42	UWIND, UMEAN, UR, UAW
8	43	8	46	VWIND, VMEAN, VR, VAW
8	47	8	5C	WWIND, WHEAN, WR, WAW
55	1	55		SIGMAS OF THE STATES
11	9	11	9	ERY
16	1	16	2	SIGDAP, SIGDRP
				BLANK CARD TO TERMINATE OPTION 7

A.5.3.9 Sample of Option 10

10	CREATE	A FILE	COMPATIBLE	FOR OPTION	18		
5	8 0						
1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0
1.1	2.1 .	3.1	4.1	5.1	6.1	7.1	8.1
1.2	2.2	3.2	4.2	5.2	6.2	7.2	8.2
1.3	2.3	3.3	4.3	5.3	6.3	7.3	. 8.3
1.4	2.4	3.4	. 4.4	5.4	6.4	7.4	8.4
1.5	2.5	3.5	4.5	5.5	6.5	7.5	8.5

A.5.3.10 Sample of Option 11

			ADDING THETOIR	TTONE			
11	0	SIUKE !	ABBING INSTRUC				
9	•						
10	1	TIME					
10	2	ALT .					
10	3	VA-KTS					.5924
10	8	PHI					57.3
10	9	PSI					57.3
10	4	XAPP					
10	6	YAPP					
10	7	YSP					
10	55	ERY					
10							
10	1	TIME					
10	14	VB					
10	30	AMIND					
10	31	VPEAN					
10	33	WAV					
10	24	SIGMAVY					
10	10	DA					
10	11	DR					
10	12	SIGDA					
10	13	SIGOR					
10	1	TIME					
10	38	SIGV					
10	39	SIGP-DEG					57.3
10	40	SIGP-DEG					57.3
10	41	SIGPHI					57.3
10	42	SIGPSI					57.3
10	43	SIGY					
10	20	PSIA					57.3
10	21	THETAA					57.3
10	22	PHIA					57.3
•							
10	1	TIME					
10	56	SIGDAP					
10	57	SIGDRP					
10	12	SIGDA					
10	13	SIGOR					

A Deposit

Total Control

BLANK CARD TO TERMINATE OPTION 11

A.5.3.11 Sample of Option 12

STORE PRINTER PLOTTER INSTRUCTIONS ON A FILE. 12 VOLAR CHECKOUT - 16 FEB 78 EFFECT OF AIRWAKE ON SIMPLE MODEL UAW VS TIME VOLAR CHECKOUT - 16 FEB 78
EFFECT OF AIRWAKE ON SIMPLE MODEL
WAW VS TIME
3.0 1.0 0.0 7.0 TIME - SEC. UAW IN FEET PER SECOND. VOLAR CHECKOUT - 16 FEB 78

FFECT OF AIRWAKE ON STADE 0.0 TIME - SEC. WAW IN FEET PEP SECOND. EFFECT OF AIRWAKE ON SIMPLE MODEL 7.0 3.0 1.0 0.0 7.0 TIME - SEC. VAW FT/SEC. 44 V 1.0 1.0 VAW IN FEET PER SECOND. 10

```
13
            STORE CALCOMP PLOTTER INSTRUCTIONS ON A FILE.
CAL34
          PLOT
SPLOTD NCURVS-1, XPLOT-2.0, YPLOT-0.5, ANGLE-0.0, LNGTHX-5.0, STARTX-500.0,
        DELX=-100.0,XDRG=500.0,LNGTHY=4.0,STARTY=0.0,DELY=2.0,YDRG=0.0,
        ISOPT-22, SEND
          RANGE FROM SHIP - FT.
          SIGMA APP. PATH - FT.
5.0
          9.75
    VOLAR CHECKOUT
      14 FEB 78
  EFFECT OF AIRWAKE
   ON SIMPLE MODEL
SCURVE NDATA-10, NCDLX-21, NCCLY-31, LINTYP-0, DASH-0.01, SCALEX-1.0,
        SCALEY-1.0, SEND
177777
SPLOTO NCURVS=2, XPLOT=0.0, YPLOT=5.5, XLEGND=0.25, YLEGND=1.00,
        DELY-5C.O, ISOPT-12, SEND
              ALTITUDE - FT.
50 PERCENT PROB. ELLIPSE X 5
SCURVE NCOLY=2,NSYM=99,LINTYP=10,NCX=23,NCY=24,NCXY=53,
        SCALXX=5.0, SCALYY=5.0, SEND
177777
          ACTUAL
SCUPVE NCDLY=16,LINTYP=0,SCALEY=-1.0,SEND
170360
          COMMANDED
SPLOTO NCURVS=1, XPLOT=7.5, YPLOT=0.0, DELY=2.0, ISOPT=4, SENO
             SIGMA XAP - FT.
SCURVE NCTLY=23, SCALEY=1.0, SEND
177777
 SPLOTD NCURVS=1, XPLOT=0.0, YPLOT=-5.5, DELY=2.0, SEND
            SIGMA ZAP - FT.
SCURVE NCOLY=24, SEND
177777
 SPLOTO
          XPLOT=9.5, YPLOT=C., DELY=2.
                                          SEND
             SIGMA THETA - DEG.
 SCUPVE
          NCOLY -22, SCALEY-57.3
                                    SEND
177777
 SPLCTD XPLCT=C.O, YPLOT=5.5, STARTY=-8.G, DELY=4.0, SEND
                THETA - DEG.
 SCURVE
          NCOLY-4
                   SEND
177777
 SPLOTO
         . XPLOT=7.5, YPLOT=C., STARTY=-.2, DELY=.1
                                                    SEND
             DE - UNITS
SCURVE
          NCCLY=7, SCALEY=1. SEND
177777
 SPLOTO
          XPL PT=0., YPLOT=-5.5, STARTY=G., DELY=.05 SEND
           SIGMA DE - UNITS
 SCURVE
          NCOLY-28 SEND
177777
          XPLDT-9.5, YPLOT-C., DELY-10.0 SEND
 SPLOTO
             SIGMA RPM - RPM
          NCULY-25 SEND
 SCURVE
177777
```

A.5.3.13 Sample of Option 14

14 TAB THE DUTPUT 2 TAB INSTRUCTIONS STORED ON FILE 2

A.5.3.14 Sample of Option 15

15 PUNCH TIME HISTORY

A.5.3.15 Sample of Option 17

17 PRODUCE PRINTER PLOTS
5 1
3

VOLAR CHECKOUT - 16 FEB 78
EFFECT OF AIRWAKE ON SIMPLE MODEL

UAW VS TIME
1 0.0 7.0 3.0 1.0

TIME - SEC.

UAW IN FEET PER SECOND. 10 1 4C U 1.0 1.0

VOLAR CHECKOUT - 16 FEB 78
EFFECT OF AIRWAKE ON SIMPLE MODEL

WAW VS TIME
1 0.0 0.0 3.0 1.0

TIME - SEC.

WAW IN FEET PER SECOND. 10 1 48 W 1.0 1.0

VOLAR CHECKOUT - 16 FEB 78
EFFECT OF AIRWAKE ON SIMPLE MODEL

VAW VS TIME
1 0.0 7.0 3.0 1.0

TIME - SEC.

VAW FT/SEC.

VAW FT/SEC.

VAW FT/SEC.

```
A.5.3.16 Sample of Option 18
   18
            PRODUCE CALCOMP PLOTS
          1
CAL34
           PLOT
 SPLOTD NCURVS=2,XPLOT=.75,YPLOT=0.0,ANGLE=0.0,LNGTHX=4.0,STARTX=0.0,
         DELX=5.0, XDRG=0.0, LNGTHY=4.0, STARTY=00.0, DELY=40.0, YDRG=0.0,
         ISDPT=6 ,XLEGND=2.0,YLEGND=1.0 SEND
                TIME - SEC.
              LATERAL POS. - M.
 $CURVE DASH=.01, NDATA=10, NCDLX=1, NCDLY=6, LINTYP=0, SCALEX=1.0, SCALEY=.3048 SEND
177777
 SCURVE DASH=.01, NDATA=10, NCDLY=7, SEND
170360
           COMMANDED
 SPLOTD NCURVS=1,XPLDT=0.0,YPLDT=5.0,LNGTHY=4.0,STARTY=0.0,DELY= 1.0,YDRG=0.0,
         ISOPT=4, XLEGND=2.0, YLEGND=4.5, SEND
           SIGMA LAT. POS. - M.
 SCURVE DASH-.01, NDATA=10, NCDLY=43, SCALEX=1.0, SCALEY=.3048 SEND
177777
 $PLOTD NCURVS=1, XPLOT=5.5, YPLOT=-5.0, LNGTHY=4.0, STARTY=-4.0, DELY=2.0, YORG=0.0,
         ISOPT=4, XLEGND=2.0, YLEGND=3.5 SEND
              BANK ANGLE - DEG.
 SCURVE DASH=.01, NDATA=10, NCDLY=8, SCALEX=1.0, SCALEY=57.3 SEND
177777
 $PLATD NCURVS=1,XPLDT=0.0,YPLDT=5.0,LNGTHY=4.0,STARTY=0.0,DELY= 2.0,YDRG=0.0,
         ISOPT=4, XLEGND=2.0, YLEGND=4.5, SEND
              SIGMA PHI - DEG.
 $CURVE DASH=.01,NDATA=10,NCDLY=41,SCALEX=1.0,SCALEY=57.3 $END
177777
 SPLOTD NCURVS=1, XPLOT=5.5, YPLOT=-5.0, LNGTHY=4.0, STARTY=-0.2, DELY=0.1, YORG=0.0,
         ISOPT-4, SEND
           ROLL CONTROL - UNITS
 SCURVE DASH=.01, NDATA=10, NCDLY=10, SCALEX=1.0, SCALEY=1.0, SEND
177777
 SPLOTD NCURVS=1,XPLOT=0.0,YPLOT=5.0,LNGTHY=4.0,STARTY=0.0,DELY=.20,YORG=0.0,
         ISOPT=4, XLEGND=2.0, YLEGND=4.5, SEND
        SIGMA ROLL CONTROL - UNITS
 SCURVE DASH=.01, NDATA=10, NCOLY=56, SCALEX=1.0, SCALEY=1.0, SEND
177777
 SPLATD NCURVS=1,XPLDT=6.0,YPLDT=-5.0,LNGTHY=4.0,STARTY= -.02,DELY=.01,
         YORG-O.O, ISOPT-4, SEND
           YAW CONTROL - UNITS
 SCURVE DASH=.01,NDATA=10,NCDLY=11,SCALEX=1.0,SCALEY=1.0,SEND
177777
 SPLOTD NCURVS=1,XPLOT=0.0,YPLOT=5.0,LNGTHY=4.0,STARTY=0.0,DELY= .01,YORG=0.0,
         ISCPT=4, XLEGND=2.0, YLEGND=4.5, SEND
        SIGMA YAW CONTROL - UNITS
 SCURVE PASH-.01, NDATA-10, NCDLY-57, SCALEX-1.0, SCALEY-1.0, SEND
177777
 SPLOTO NCURVS=1, XPLOT=5.5, YPLOT=-5.0, LNGTHY=4.0, STARTY= -2.0, DELY=1.0,
         YORG-O.O, ISOPT-4, SEND
           LAT. POS. ERROR - M.
 $CURVE DASH=.01,NDATA=10,NCDLY=55,SCALEX=1.0,SCALEY=.3048,$END
177777
 SPLOTD NCURVS-1,XPLOT-0.0,YPLOT-5.0,LNGTHY-4.0,STARTY-0.0,DELY-1.0,YORG-0.0,
```

ISOPT=4, XLEGND=2.0, YLEGND=4.5, SEND

SCURVE DASH-.C1,NDATA-10,NCDLY-33,SCALEX-1.0,SCALEY-.3048,SEND

VAW - MISEC.

A.5.3.17 Sample of Option 19

19 PRINT A FILE IN BLOCKED FORM.

A.5.3.18 Sample of Option 21

A.5.3.19 Sample of Option 28

A.5.4 Program Output

The program's output is divided into four categories: disk storage, printed output, plotted output and punched output. Before the time history output can be printed, plotted, or punched, it has to be stored on a file.

A.5.4.1 Disk storage

Disk storage is divided into two sections: instructions and time history.

A.5.4.1.1 Instruction storage

Option 1 stores I or R array instructions on a file. Options 2 and 4 have the capability of storing I and R array instructions with the data on a file by specifying the NPF parameter. Options 11, 12, and 13 store tabulating and plotting instructions on a file. Option 28 stores only the R array values on a file.

A.5.4.1.2 Time history storage

Option 21 stores the time history output (specified by Option 7) on a file. Option 10 reads input and creates a file of the same structure as the time history file. This file is thus compatible with the program's output features.

A.5.4.2 Printer output

The time history output can be printed in two forms: tabular and blocked.

A.5.4.2.1 Tabular output

Once the time history has been generated and stored on a file (A.5.4.1.2), a tabular print of the output can be produced by using Options 11 and 14. Option 11 designates which elements from the stored file (A.5.4.1.2) are to be printed along with page title and column headings. Option 14 produces the tabular print. See paragraphs A.5.3.10 and A.5.3.13 for examples of Options 11 and 14 respectively.

A.5.4.2.2 Blocked output

The contents of a file can be printed in a blocked form by using Option 19. The output elements are not titled but appear in the same order as they appear on the file being dumped. Option 21 has the capability to print the time history in a blocked form by specifying NPRNT \neq 0. This is to be used for debugging because the print is generated every DTØUT seconds until job

termination. When using Option 14 to tab the output, the job must have executed normally. See paragraphs A.5.3.17 and A.5.3.19 for examples of Options 19 and 21 respectively.

A.5.4.3 Plot output

The time history output can be plotted in two forms: CalComp plots and printer plots.

A.5.4.3.1 CalComp plots

After the time history has been placed on a file (A.5.4.1.2), a CalComp plot can be produced by using Option 18. See the text for examples of the plots. See paragraph A.5.3.16 for an example of Option 18.

A.5.4.3.2 Printer plots

After the time history has been placed on a file (A.5.4.1.2), a printer plot can be produced by Option 17. The plots consist of a 7 by 7 inch grid with one plot per page. See paragraph A.5.3.15 for an example of Option 17. See Figure A.5.4.3.2 for a sample printer plot.

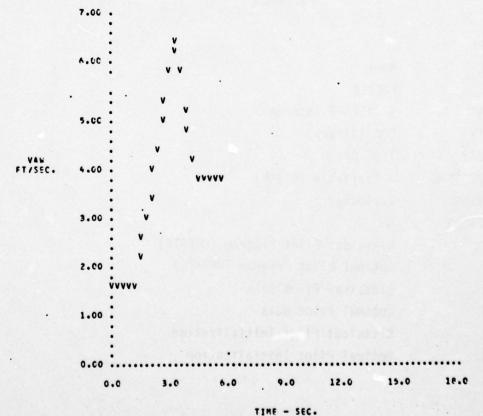


Figure A.5.4.3.2

A.5.4.4 Punched output

After the time history has been placed on a file (A.5.4.1.2), punched cards can be produced by using Options 11 and 15. Option 11 designates which elements from the stored file are to be punched. Option 15 produces the punched cards. See paragraphs A.5.4.10 and A.5.4.14 for examples of Options 11 and 15 respectively.

A.6 Program Flow

An overall picture of program flow is illustrated in Figure A.5.

A.7 Discussion of Control Cards

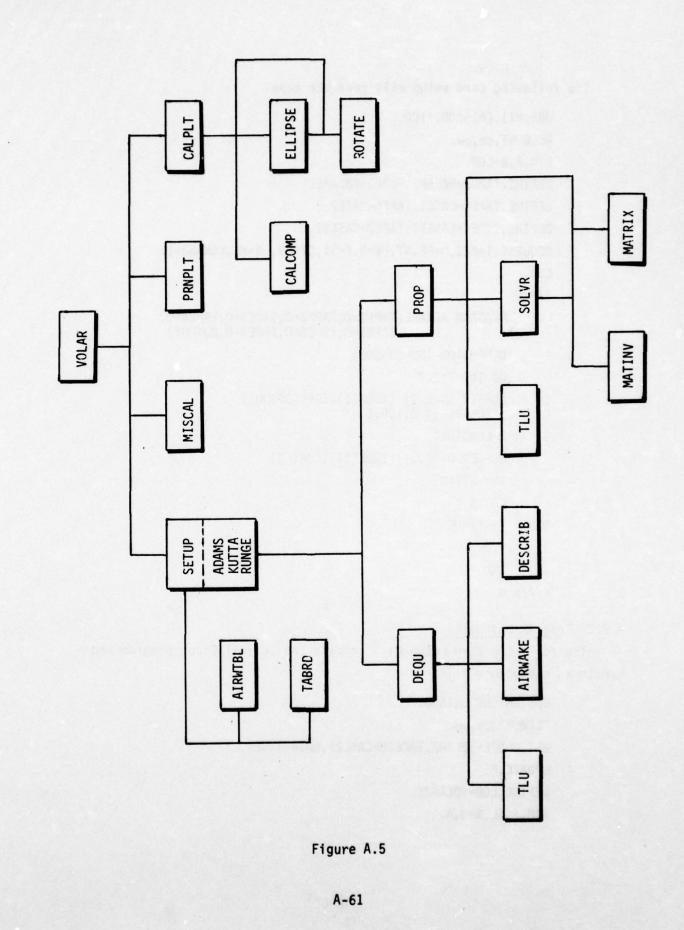
The following discussion of control cards is sufficient to place the VOLAR program online and execute its sample problems.

A.7.1 Transferring the Data from Magnetic Tape to Disk

Table A.2 is a description of how the tape was created.

Table A.2

TRACK	9
LABEL	None
CODE	EBCDIC
FORMAT	SI (SCOPE Internal)
PARITY	ODD (Binary)
DENSITY	1600 BPI
RECORD TYPE	S (Variable length)
BLOCKING	Unblocked
NO. FILES	6
1	Classical Pilot Program (UPDATE)
2	Optimal Pilot Program (UPDATE)
3	Classical Pilot Data
4	Optimal Pilot Data
5	Classical Pilot Initialization
6	Optimal Pilot Initialization



processed and the same of the

```
The following card setup will read the tape:
     JØB,NT1,CM15000,T100.
     ACCOUNT, cn, pw.
     FTN, A, B=LGØ.
     DEFINE, TAPE2=VØLAR1, TAPE3=VØLAR2.
     DEFINE, TAPE4=CASE1, TAPE5=CASE2.
     DEFINE, TAPE6=CASE1I, TAPE7=CASE2I.
     REQUEST, TAPE1, D=PE, NT, PØ=R, F=SI, CV=EB, LB=KL, VSN=5251.
     LGØ.
     7/8/9
           PRØGRAM RDTAPE(TAPE1=0, TAPE2=0, TAPE3=0, TAPE4=0,
                            TAPE5=0, TAPE6=0, TAPE7=0, ØUTPUT)
           DIMENSION IBUF(30000)
           DØ 100 J=2,7
           BUFFER IN(1,1) (IBUF(1), IBUF(30000))
           IF(UNIT(1)) 5,100,5
     5
           L=LENGTH(1)
           BUFFER ØUT(J,1)(IBUF(1), IBUF(L))
            IN=UNIT(J)
           GØ TØ 1
     100
           CØNTINUE
           STØP
            END
     6/7/8/9
```

A.7.2 Program Execution

The following card setup will compile the Optimal Pilot program and create an executable file:

JØB, CM150000, T500.

ACCOUNT, cn, pw.

GET, ØLDPL=VØLAR2, TAPE28=CASE2I, DATA=CASE2.

UPDATE, F.

DEFINE, LGØ=VØLAR2E.

FTN, I, SL, R=3, A.

MAP, FULL.
LDSET, PRESET=ZERØ, LIB=CALCØMP.
LGØ, DATA.
7/8/9
6/7/8/9

A.7.3 Program Modification

The following card setup will modify one of the routines in the Optimal Pilot program and execute the program.

JØB,CM150000,T500.

ACCOUNT, cn, pw

GET, ØLDPL=VØLAR2, ØLD=VØLAR2E.

UPDATE.

FTN, I, SL, R=3, A.

CØPYL.

MAP, FULL.

LDSET, PRESET=ZERØ, LIB=CALCØMP.

NEW.

7/8/9

UPDATE CHANGE CARDS GØ HERE.

7/8/9

INPUT DATA CARDS GØ HERE.

6/7/8/9

A.8 Discussion of Input Deck for the Classical Pilot Model Simulation

The purpose of this section is to lead the prospective user of VOLAR through a sample input deck. The discussion here will focus on the necessary flow of options to generate a time history and point out any special input requirements that might not be obvious to the new user. This input deck is identical to the one which generated the AV-8A classical pilot model simulation and plots for the case with control limiting. After studying this section the user should run this case on his computer.

A schematic of the job setup to run this case is presented in Figure A.6. Figure A.7 is a listing of the input deck. The circled numbers provide a cross reference to this test; i.e., the cards following 4 are discussed below in Section A.8.4.

Throughout the discussion of this input deck, it may be beneficial to the reader to refer to the description in Section A.5 of the main program and its options.

A.8.1 Namelist Input

The first step is to provide the main program with the information required to bookkeep the I and R arrays. The namelist SEGMNT establishes the number of segments in each array and the number of elements in each segment. The format for NAMELIST inputs can be found in the CDC FORTRAN manual.

The namelist SEGMNT is the one and only mandatory input. All other inputs are either user selected options or input required by the chosen option.

For this case the I array is seven segments long, and the R array is composed of 143 segments. The NPRNT = 1 causes the I and R array segmentation information to be output. The lengths of the segments are consistent with the I and R arrays presented in Appendix E.

A.8.2 Option 2

Integer values that define system size and control the selection of certain calculations are input here. These parameters are defined in Appendix E.

Although NPE and NPX are dimensions of matrices used only in the optimal pilot case, they are given a value of one (1) here. The reason is the

integration subroutines expect to integrate a set of means and three matrices. By giving NPE and NPX a small value, a negligible increase in run time is traded for the simplicity of having only one set of integration subroutines. This keeps the number of problem dependent subroutines to an absolute minimum.

This run will include the ship airwake (NOAW = 0) and is not an initialization run (NOINIT = 1).

A.8.3 Option 4

Required values of the R array are input next. At Vought fixed geometric and aerodynamic properties are input here. Case-dependent information is input later in the deck. At the beginning of job execution, the 'LDSET, PRESET = ZERO' control card initializes core to zero. Therefore, parameters not initialized through Option 4 begin with a value of zero.

Note that the inertias are input here as 1 (obviously not the true value). However, they are not required to generate accelerations (Vought used dimensional derivatives) but inertias do appear in SETUP in a denominator. This is all related to the calculation of forces and moments in DEQU, where the total forces and moments that drive the mean equations must be obtained from a reference condition and the perturbation forces and moments.

Tables defining the independent variable arrays, open loop inputs, aerodynamic data and nonlinear elements are also input here.

The weight and aerodynamic derivatives are from Reference 15. The ship geometry inputs represent a DD-963. Feedback gains and time constants are for the classical pilot model discussed in Section 6. The values of TABUB, TABWB, TXAPP, TZAPP, and TXSP were derived from the task description. These tables provide the reference longitudinal values required by the lateral/directional equations. The final four tables define the nonlinear functions (control limiters) discussed in Section 4.

A.8.4 Option 6

Here the user specifies the variables that are to be integrated and the variables that contain the integrated values. This option allows one to use any variable in blank COMMON as an integrand or integrated value.

Note that the setup includes the matrices PED, PE, PXHATD, and PXHAT. These are associated with the optimal pilot model and not required by the classical model. In Section A.8.2 it was noted that these are specified as 1 by 1 matrices (NPE and NPX) and included in this setup to avoid the need for two sets of integration subroutines.

A.8.5 Option 7

The variables specified here appear on the output file. Their selection is totally up to the user. All of the output features (tabbing, plotting, etc.) access the file containing the Option 7 specified variables.

A.8.6 Option 11

The variables to be tabbed are user defined. Here it was attempted to tabulate all the key parameters for interpreting the performance of a given task.

A.8.7 Option 4

The case-particular input goes here. The order is not important.

The first two terms in this input are ambient wind magnitude and direction. The ambient wind gets into the calculation of airspeed and wind over deck.

The ship's speed and heading are also input. The ambient wind and ship conditions were selected to give 35 knots wind over deck comming at 30 degrees to port. This value is a 'breakpoint' in the ship airwake model data tables.

The initial body axis components of airspeed are necessary to initialize the airplane inertial speed. Aside from this exception, airspeeds are calculated in DEQU from inertial speeds. This particular representation was chosen because it was felt that most often the airplane flight conditions would be specified by stating an airspeed, angle-of-attack, and sideslip. If this is undesirable, the user can modify DEQU to meet his needs. The mean components of the airwake, that enter into the calculation of airspeed, may be obtained by requesting a zero second time history after specifying the airplane and ship positions in space.

The initial aircraft bank angle is -1 degree, and the aircraft's heading is zero degrees. The bank angle is required to balance out the initial side force on the airplane. The initial side force is due to the non-zero value of sideslip (VAS \neq 0).

The value of SUMFYO was obtained from Y_{v} . The initial values of SUMLO and SUMNO are zero. It is assumed that the roll and yaw controls would trim out the moments due to N_{v}' and L_{v}' so that the total moments on the airplane are zero. SUMFYO, SUMLO, and SUMNO are total force and moments on the airplane and are required in subroutine SETUP to initialize YO, LO, and NO.

The initial displacements of the ship and airplane along the y earth axis are input as zero. The x-axis displacements of the ship and airplane, and the z axis displacement of the airplane were previously input in table form.

A.8.8 Option 28

This option reads data stored from a previous run. It is used here to initialize the P matrix.

In the previous run, NOINIT was set to -1 (all other input discussed to this point remains unchanged). This froze the means and integrated only the covariance matrix. When NOINIT = -1, Option 28 should follow Option 21. Refer to Section A.5 for using Option 28 in a BUFFER IN or BUFFER OUT mode.

This initialization is necessary to start the P matrix at realistic values. Because the airplane did not suddenly appear at a point 16 seconds away from the ship, beginning with P=0 is unrealistic. The airplane flew through the atmosphere (and its disturbances) to get to the point in the trajectory where the VOLAR simulation picks it up. The question then becomes one of determining what is a realistic method to use for initializing the covariance matrix.

Subroutine SOLVR provides a method for initializing P. SOLVR calculates the steady-state (i.e. $t \to \infty$) value of P. This solution would provide an upperbound on the uncertainties (i.e. the value of P). However, SOLVR will not work for the optimal pilot cases because there are three inter-related covariance matrices, and it is programmed to solve only one. Also, one might argue that $t \to \infty$ statistics may not be realistic either. Note that if the system is unstable, $P \to \infty$ as $t \to \infty$.

The approach selected here was to integrate the P matrix for some period of time. Five seconds was selected. For a stable system, the P matrix will approach its steady state value fairly rapidly. This is something the user

must evaluate on a case by case basis. For the runs presented here, 5 seconds was quite adequate. One more comment is in order. When making initialization runs, it is often necessary to use a lower integration increment and/or a higher order integration scheme than in the simulation runs. The reason is the elements of the P matrix often undergo wild perturbations, before settling out, when all the elements are initialized to zero.

A.8.9 Option 21

This option generates time histories of the means and covariances. The example presented here asks for a 20 second time history using Adams integration. The covariance matrix will be printed out at the initial time point (t = 0) and every 20 seconds. The output file is TAPE10.

After the call to SETUP, before the integration process begins, the elements of segment eight will be output. This was done to check on the parameters associated with the airwake calculations. It is not necessary to output anything here. But often, the user desires to know some parameter values but does not want to take up space on the output file. This is a convenient place to look at the values of such parameters.

For a given stepsize, Adams integration is three times faster than the third order Runge-Kutta and four times faster than the fourth order. However, the Adams integration stepsize will normally have to be lower than the Runge-Kutta stepsizes to obtain the same degree of accuracy. We have found the stepsize change does not offset the speed advantage; and for production running, Adams integration is preferable. As the user modifies these routines and/or treats new problems, he should spot check his integration to confirm the accuracy of the simulation. Integration problems normally manifest themselves as time history divergence, indefinite parameter values, or infinite parameter values.

A.8.10 Option 14

This option causes the output file to be tabbed according to the instructions stored by Option 11.

A.8.11 Option 18

For some runs, the user may desire CalComp plots as well as tabbed output. The final option in this setup directs the plotting of 15 parameters from the output file. Normally one does not plot in the same run that generates the output file. It is difficult to know a priori good scales for the plots. The scales presenting these data were selected after having seen a tab output of the desired parameters.

A good description of the input required by the plot package has already been presented in Section A.5.2. The best approach to setting up plot instructions is to lay out the desired axes on regular graph paper, and use the grids to develop the distances for pen movement, etc.

A.9 Discussion of an Input Deck for the Optimal Pilot Model Simulation

The purpose of this section is to lead the prospective user of VOLAR through a sample input deck for the optimal pilot model simulation. The user should be familiar with Section A.5 which discusses the main program and its options. The discussion here will focus on the necessary flow of options to generate a time history and point out any special inputs that might not be obvious to the new user. This input deck is identical to the one which generated the 20 second sea state 5 time histories appearing in Figure 26.

A schematic of the job setup to run this case is presented in Figure A.8. Figure A.9 is a listing of the input deck. The circled numbers were added to provide a cross reference to this text; i.e. the cards following 4 are discussed below in Section A.9.4.

After studying this example, the user should run this case on his computer.

A.9.1 Namelist Input

The first step is to provide the main program with the information required to bookkeep the I and R arrays. The namelist SEGMNT establishes the number of segments in each array and the number of elements in each segment.

The namelist SEGMNT is the one and only mandatory input. All other inputs are either user selected options or input required by the chosen option.

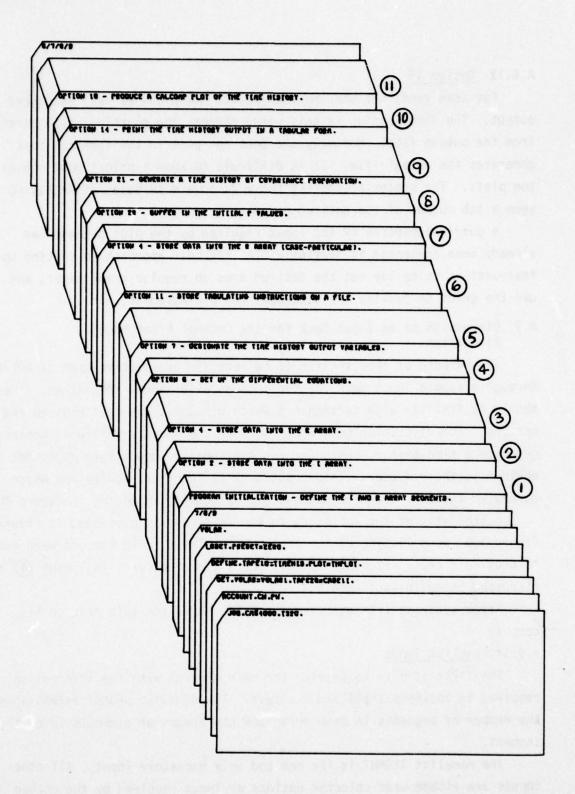


Figure A.6

```
(1) SSEGMNT NSEGI=7, NSEGR=143, NPRNT=1,
             NI(1)=10,0,0,14,14,6,
             NR(1)-6,17,17,26,18,11,37,66,9,37,
             NR(111-14,18,6,10,0,6,19,0,0,10,
             NR(21)=10,10,10,10,10,0,6,6,6,6,6,
             NR(31)=6,6,6,6,6,6,6,6,6,6,6,6,
             NR (41)=6,6,6,6,6,6,6,6,0,289,
             NR(51)=289,289,44,16,50,50,75,75,75,75,
NR(61)=75,75,6,6,6,6,6,6,6,6,6,
             NR(71)=6,6,6,6,6,6,6,6,6,6,6,6,
             NR(81)=36,24,42,49,28,1,1,1,1,24,
             NR(91)=16,1,1,1,1,1,1,1,1,1,1,
             NR(101)=1,1,1,1,1,1,12,6,6,6,6,
              NR(111)-6,6,6,6,6,6,6,6,6,6,6,6,
              NR(121)=6,6,6,6,6,6,6,6,6,6,6,6,
             NR(131)=6,6,6,6,10,10,10,10,10,4,
             NR(141)=4,4,4,
     SEND
2
                 READ INTO I ARRAY
                           NSTATES, NPA, NOM, NGM
       11
                           NPE, NPX, NOAW, NOINIT
                       10
             1
                   0
        1
                            BLANK CARD FOR READ I
3
                READ R
                   0
                         6 WEIGHT, G, IX, IY, 12, IX7
              1
                   6
                                                            0.
     16300.
               32.174
                        9 LM, WM, LTDM
     438.
                46.75
                          348.
                           TAUD
     0.2
                       29 DMEGAV, KV
        7
                   7
            28
               3.
                       35 TAUA, K1, K2, KY, B1, B2
        7
                   7
            30
                       2.83
37 TL1, TL2
                                                            2.
     0.1
               1.12
                                     .010
                                                1.
        7
            36
                   7
     10.
               2.
                           TABV1 (V TABLE FOR AERO DATA)
       13
             1
                  13
                        6
                                                                                  1.688
    0.14
               30.
                                                80.
                                                            105.
                                      65.
                  14
                       10
                           TABV2
                                   (TIME TABLE FOR OPEN LOOP INPUTS)
                                                            10.
     0.
                                                 8.
                                     6.
                           20.
     14.
               16.
                           GAINDA, GAINDR
             5
      16
                 16
               1.
       20
             1
                 20
                       10
                          TABTC
                                   (OPEN LOOP THETA)
                                                 .13964
                                                            .13964
                                                                       .13964
     .13964
                .13964
                           .13964
                                      .13964
     .13964
                .13964
                           .13964
      120
             1 120
                          TYV
                           -.088
                                      -.104
                                                 -.120
                                                            -.138
     -.034
                -.063
                          TYP
      121
                121
               0.
                                                 0.
                          0.
                                      0.
                                                            0.
      0.
             1 122
                         6 TYR
      122
                        6 TYDA
                -.240
                                      -. 235
                                                 -.235
                                                            -.215
     -.225
      123
              1 123
                -.006
                           -.015
                                      -.026
                                                 -.039
                                                            -.065
      124
             1 124
                         6 TYDR
                        6 TLV
     -.68
                -.67
                                      -.75
                                                 -.80
                                                            -.90
              1 125
     125
             1 126
                        -.0197
6 TLP
     -.002
                                                 -.0184
                                      -.0204
                                                            -.0104
     126
                                      -.79
                                                 -1.0
                                                            -1.38
     -.13
                -.42
                           --62
```

Figure A.7

```
1 128
                           .24
                                                              .49
     .015
                                       .31
                                                  .375
                         6 TLDA
      128
                                                              . 5
                                       . 5
                                                   . 5
     . 5
      129
                129
                            TLDR
     -.06
                -.065
                           -.075
                                       -.08
                                                  -.095
                                                             -.13
                           TNV
      130
              1 130
     -.0036
                -.0021
                           -.0010
                                       0.
                                                  .6014
                                                              .0047
      131
                           THP
              1 131
                            -.053
                                       -. 072
     -.005
                -.032
                                                  -.091
                                                              -.126
     132
              1 132
                           THR
     -.042
                                       -. 142
                                                             -.203
                 -.088
                            -.12
                                                  -.164
                133
                           TNDA
      133
                .03
                            .031
TNDR
                                       .033
     .03
                                                  .035
                                                              .040
      134
                134
                .235
                           .243
TABUB
     .225
                                       .248
                                                  .255
                                                              .265
      135
                        10
     65.869
                61.254
                            56.640
                                       52.025
                                                  47.410
                                                             42.796
                                                                        38.181
                28.952
     33.566
                           28.952
TABWB
                        10
     9.257
                8.608
                            7.96
                                       7.311
                                                             6.014
                                                                         5.366
                                                  6.663
                           4.069
                4.069
      137
                 137
                        10
                            TXAPP
                128.372
                           247.425
                                       357.157
                                                  457.57
                                                             548.662
                                                                         630.434
     702.887
                766.02
                            882.964
      138
              1 138
                        10 TZAPP
     -50.
                -50.
                           -50.
                                       -50.
                                                  -50.
                                                             -50.
                                                                         -50.
     -50.
                -50.
                           -50.
                        10 TXSP
                 139
      139
     298.24
                356.712
                           415.185
                                       473.657
                                                  532.13
                                                             590.602
                                                                         649.07
                            882.964
     707.547
                766.02
      140
              1 140
                         4 TOAIN
     -5.
                -.9
      141
              1 141
                            TDADUT
     -.9
                 -.9
                                       .9
              1 142
      142
                           TORIN
     -5.
143
                                       5.
                            .532
              1 143
                            TORDUT
     -.532
                -.532
                            .532
                                       .532
                             BLANK CARD FOR READ R
4
                   SETUP DIFFERENTIAL EQUATIONS
        2
             11
                             VDOT, PDOT, ROOT, YAPPDOT, PHIDOT, PSIDOT, YSPOOT
                            DAID, DAZO, DRID, DR 20
BLANK CARD TO TERMINATE DERIVATIVES
        12
             15
                   12
                        18
         5
             11
                        17
                             VB, PB, RB, YAPP, PHI, PSI, YSP
         3
                    3
        12
             11
                   12
                             DA1, DA2, DR1, DR2
                             BLANK CARD TO TERMINATE STATES
        52
              1
                   51
                             PDOT, P
                             BLANK CARD
      100
              1
                   99
                             PED, PE
                             BLANK CARD
      104
                             PXHATD, PXHAT
BLANK CARD, END OF OPTION 6
                  103
(5)
                   DESIGNATE OUTPUT VARIABLES
                             TIME
                             ALT, VAIR
                             XAPP, ZAPP
                             YAPP
             14
                        14
                    3
                             YSP
             17
                    3
                        17
             15
                    3
                        16
                             PHI, PSI
                             DA. DR.
```

1 127

127

6 TLR

Figure A.7 (cont'd)

```
SIGDA, SIGDR
                    1 f
3
      16
                           11
             11
                                 UB, WR
XM, YM, ZM
             27
                           29
                                 PSIA, THETAA, PHIA
SIGMAVY, SIGMAVY
UWIND, UMEAN, UR, UAW
VWIND, VMEAN, VR, VAW
             30
                           37
             33
                      8
                           35
             39
                           42
             43
                                 WWIND, WHEAN, WR, WAW
SIGMAS OF THE STATES
      55
11
              1
                    55
                           17
                                 FRY
                    11
                                 SIGDAP, SIGDRP
              1
                            2
      16
                    16
                                 PR, PR
SIGPR, SIGRB
BLANK CARD TO TERMINATE OPTION 7
       3
             12
                     3
                           13
               2
                    55
     11
2
9
                    STORE TABBING INSTRUCTIONS
               0
      10
                    TIME
                    ALT
VA-KTS
      10
               2
                                                                                                      .5924
57.3
57.3
      10
               3
      10
               8
                    PHI
      10
               9
                    PSI
      10
                     XAPP
               6
      10
                    YAPP
      10
10
10
                     YSP
             55
                    ERY
                    TIME
                    VB
VWIND
      10
             14
      10
             30
      10
             31
                     VMEAN
      10
10
10
10
             33
                     WAV
             24 SIGHAVY
             10
                    DA
                    DR
                   SIGDA
             12
      10
             13
                   SIGDR
      10
      10
                    TIME
                  SIGV
             38
      10
10
10
             39 SIGP-DEG
                                                                                                       57.3
                                                                                                       57.3
57.3
             40 SIGR-DEG
             41
                  SIGPHI
SIGPSI
      10
             43
                   SIGY
                                                                                                       57.3
             20
                   PSIA
                                                                                                       57.3
       10
             21
                   THETAA
       10
             22
                   PHIA
      10 10 10
               1
                     TIME
             56
57
12
13
                   SIGOAP
                     SIGDRP
                     SIGDA
                     SIGDR
       10
      10
                     PB
RB
              58
             59
      10
             60
                     SIGPB
                     SIGRB
                                BLANK CARD TO TERMINATE OPTION 11 (CASE-PARTICULAR INPUT)
0
                   PEAD R
               5
             14
                                                                                                       1.688
                                 VAMB
        8
                           14
    20.
                                                                                                       .01745329
              15
                      8
                           15
                                 PSIAMB
    150.
```

Figure A.7 (Cont'd)

```
8
          10
                8
                     16 VS (SHIP SPEED)
                                                                              1.t88
   20.
                        PSIS ((SHIP HEADING)
          11
                     11
      8
                8
                                                                              .01745329
   30.
           3
                B
                      5 UAS, VAS, WAS
             -7.012
                        10.495
                     16 PHI, PSI
          15
                                                                              .01745329
                3
             0.
   -1.
          10
                     12 SUMFYO, SUMLG, SUMNO
   290.41
             0.
                        0.
                     17 YSP
          17
                2
      2
  0.
                     14 YAPP
      2
          14
                2
  0.
                         BLANK CARD TO TERMINATE OPTION 4
(8)
    28
               BUFFER IN INITIAL P VALUES
      0
     51
               51 289
                        BLANK CARD
     21
               COVARIANCE PROPAGATION
       *********************
                 AV-8A
       ..
            35 KT WOD, LAT/DIR
       ..
       ******************
           5 10
                           0
           3
                1
                      6 DTIME, DTOUT, DTOUT2, TMAX
  0.0125
            0.2
                       20.0
                                 20.0
                        BLANK CARD FOR READ P
                     66 PRINT SEGMENT 8
BLANK CARD FOR WRITE R
      8
                8
    14
            TAB THE DUTPUT
            TAR INSTRUCTIONS STORED ON FILE 2
             PRODUCE CALCOMP PLOTS
    18
  CAL 34
            PLOT
   SPLOTO NCURVS=2, XPLOT=.75, YPLOT=0.0, ANGLE=0.0, LNGTHX=4.0, STARTX=0.0,
          DELX-5.0, XORG-0.0, LNGTHY-4.0, STARTY-00.0, DELY-40.0, YORG-0.0,
          ISOPT-6 , XLEGND-2.0, YLEGND-1.0 SEND
                 TIME - SEC.
               LATERAL POS. - M.
   SCURVE DASH -. 01, NDATA-10, NCOLX-1, NCOLY-6, LINTYP-0, SCALEX-1.0, SCALEY-. 3048 SEND
  177777
   SCURVE DASH .. 01, NDATA = 10, NCOLY = 7, SEND
            COMMANDED
  170360
   SPLOTD NCURVS-1, XPLOT-0.0, YPLOT-5.0, LNGTHY-4.0, STARTY-0.0, DELY- 1.0, YORG-0.0,
          ISOPT-4, XLEGND-2.0, YLEGND-4.5, SEND
            SIGMA LAT. POS. - M.
  SCURVE DASH-.01, NDATA-10, NCOLY-43, SCALEX-1.0, SCALEY-.3048 SEND
   SPLOTD NCURVS=1,XPLOT=5.5,YPLOT=-5.0,LNGTHY=4.0,STARTY=-4.0,DELY=2.0,YDRG=0.0,
          ISOPT-4, XLEGNO-2.0, YLEGNO-3.5 SEND
               BANK ANGLE - DEG.
   SCURVE DASH-. 01, NDATA-10, NCOLY-8, SCALEX-1.0, SCALEY-57.3 SEND
  177777
   SPLOTO NCURVS-1, XPLOT-0.0, YPLOT-5.0, LNGTHY-4.0, STARTY-0.0, DELY- 2.0, YORG-0.0,
          ISOPT-4, XLEGND-2.0, YLEGND-4.5, SEND
               SIGMA PHI - DEG.
   SCURVE DASH-.01, NDATA-10, NCOLY-41, SCALEX-1.0, SCALEY-57.3 SEND
  177777
   SPLOTD NCURYS-1, XPLOT-5.5, YPLOT--5.0, LNGTHY-4.0, STARTY--0.2, DELY-0.1, YORG-0.0,
          ISOPT-4, SEND
            ROLL CONTROL - UNITS
   SCURVE DASHO.01, NDATA-10, NCOLY-10, SCALEX-1.0, SCALEY-1.0, SEND
  $PLOTO *CUPYS-14 TELOT-0.0. YPLOT-5.0. LNGTHY-4.0. STARTY-0.0. DFLY-. 20. YORG-0.0.
```

Figure A.7 (Cont'd)

```
ISOPT-4, XLEGND-2.0, YLEGND-4.5, SEND
       SIGMA PULL CONTROL - UNITS
SCURVE DASH-.01, NDATA-10, NCOLY-56, SCALEX-1.0, SCALEY-1.0, SEND
177777
 SPLOTO NCURVS=1, XPLOT=6.0, YPLOT=-5.0, LNGTHY=4.0, STARTY= -.02, DELY=.01,
        YOKG-0.0, ISOPT-4, SEND
           YAW CONTROL - UNITS
SCURVE DASH-.01, NDATA-10, NCOLY-11, SCALEX-1.3, SCALEY-1.0, SEND
177777
SPLOTO NCURVS=1, XPLOT=0.0, YPLOT=5.0, LNGTHY=4.0, STARTY=0.0, DELY= .01, YDRG=0.0,
        I SOPT-4, YLEGNO-2.0, YLEGNO-4.5, SEND
       SIGNA YAW CONTROL - UNITS
 SCURVE DASH-.01, NDATA-10, NCOLY-57, SCALEX-1.0, SCALEY-1.0, SEND
177777
SPLOTD NCURVS=1, XPLOT=5.5, YPLOT=-5.C, LNGTHY=4.0, STARTY= -2.0, DELY=1.0,
        YORG-O.O, ISOPT-4, SEND
          LAT. POS. ERROR - M.
 SCURVE DASH-.01, NDATA-10, NCOLY-55, SCALEX-1.0, SCALEY-. 3048, SEND
177777
SPLOTD NCURVS-1, XPLOT-0.0, YPLOT-5.0, LNGTHY-4.0, STARTY-0.0, DELY-1.0, YDRG-0.0,
        ISOPT-4, XLEGND-2.0, YLEGND-4.5, SEND
              VAW - MISEC.
SCURVE DASH-.01, NDATA-10, NCOLY-33, SCALEX-1.0, SCALEY-.3048, SEND
177777
SPLOTD NCURVS=1, XPLOT=5.5, YPLOT=-5.0, LNGTHY=4.0, STARTY=-.8, DELY=.4, YDRG=0.0,
        ISOPT-4, KLEGNO-2.0, YLEGNO-4.5 $
          ROLL RATE - DEG/SEC.
SCURVE DASH-.01, NDATA-10, NCDLY-58, SCALEX-1.0, SCALEY-57.3 $
177777
SPLOTD NCURVS-1, XPLOT-0.0, YPLOT-5.0, LNGTHY-4.0, STARTY-0.0, DELY-2.0, YDRG-0.0,
        ISOPT-4, XLEGNO-2.0, YLEGNO-4.5 $
       SIGMA ROLL PATE - DEG/SEC.
 SCURVE DASH-.01, NDATA-10, MCOLY-60, SCALEX-1.0, SCALEY-57.3 $
177777
SPLOTD NCURVS-1, XPLOT-5.5, YPLOT--5.0, LNGTHY-4.0, STARTY--.04, DELY-.02, YDRG-0.0,
        ISOPT-4, XLEGNO-2.0, YLEGNO-4.5 $
          YAW PATE - DEG/SEC.
SCURVE DASH-. 01, NDATA-10, NCOLY-59, SCALEX-1.0, SCALEY-57.3 $
177777
SPLOTO NCURVS-1, XPLOT-0.0, YPLOT-5.0, LNGTHY-4.0, STARTY--.4, DELY-.2, YORG-0.0,
        ISOPT-4, XLEGNO-2.0, YLEGNO-4.5 $
       SIGMA YAW RATE - DEG/SEC.
 SCURVE DASH-.01, NDATA-10, NCOLY-61, SCALEX-1.0, SCALEY-57.3 $
177777
SPLOTO NCURVS=1, XPLOT=5.5, YPLOT=-5.0, LNGTHY=4.0, STARTY=0.0, DELY=1.0, YORG=0.0,
        ISOPT-20, XEXIT-17.0, YEXIT-0.0 SEND
            SIGHAVY - M/SEC.
1.0
AV-BA APPROACHES A DD-963
     LAT./DIR. CASE
SCURVE DASH-.O1, NOATA-10, NCOLY-24, SCALEX-1.0, SCALEY-. 3048 SEND
```

Figure A.7 (Cont'd)

Here the I array is seven segments long and the R array is composed of 119 segments. The R array is shorter than the previous example because at Vought we actually ran the longitudinal example first then later expanded the R array to include the additional lateral/directional terms. The new parameters were mostly added to the end of current segments or new segments generated for them. The expanded R array will work for this case provided the segment length information is adjusted to the correct values here. The lengths which need to change are those which define matrix sizes. These have the word 'varies' under the column 'element' in Section E.2. Note that in the previous listing, segment 51 (the P matrix) was 289 long and here it is 1521 long. This is because P went from a 17 by 17 matrix in the classical pilot example to a 39 by 39 matrix in the optimal pilot example.

One should compare blank COMMON for the two listings in Appendices B and C. Note that they are essentially the same except for the new segments and the added terms on the end of segments; then, verify the segment lengths.

Remember that the main program uses the information input by SEGMNT to establish a one to one relationship with the elements of blank COMMON. If the segment lengths are incorrectly specified, the program will self destruct; or at best, not run.

A.9.2 Option 2

Integer values that define system size and control the selection of certain calculations are input here. The elements of the I array are defined in Appendix E.

There are 11 mean equations to be integrated. The three covariance matrices, P, PE, and PXHAT are n by n matrices where n is 39, 18, and 18 respectively. QM is a 15 by 15 matrix (NQM = 15) and GM is 32 (NGM = 32) by 15 (NQM). This run will include the ship airwake calculations (N \emptyset AW = 0) and is not an initialization run (N \emptyset INIT = 1).

A.9.3 Option 4

Required values of the R array are input next. At Vought, we normally input fixed geometric and aerodynamic properties here; inputting case dependent information later in the deck. At the beginning of job execution, the control card 'LDSET, PRESET = ZERØ.' initializes core to zero; therefore parameters not initialized through an Option 4 begin with a value of zero.

Note that the value of IY is 1; obviously not a realistic inertia. The 1 is used because the inertias are not needed to generate accelerations (because of dimensional derivatives) but inertia does appear as a denominator in SETUP. The numerator term is zero so anything in the denominator will work. This is all related to the calculation of forces and moments in DEQU, where the total forces and moments that drive the mean equations must be obtained from a reference condition and perturbation forces and moments.

All the tables that define the open loop inputs, dimensional derivatives, and optimal pilot feedback gains are input here. They are consistent with the independent variable arrays TABV1 and TABV2.

The ship geometry terms are for a DD-963 and the aerodynamic derivatives are from Reference 15. The optimal pilot feedback gains were determined consistent with the derivation in Section 7.

Note the breakpoints in TABV1 (segment 13, elements 1 - 6). The only two 'legitimate' points are 35. and 56.6 knots. The data tables that are a function of airspeed are input with the same value at 0 as 35 knots and the same values for 60., 61., and 62. knots as 56.6 knots. This was done to fill up the tables, and in the case of 0 knots, to keep the computer from extrapolating to speeds lower than 35 knots. Here the simulation uses 35 knots data for any airspeed that drops below 35 knots. Thirty-five knots is the lowest airspeed the airplane should have (35 is WOD speed) and the 56.6 knots was a value initially selected for the beginning of the time history. The pilot feedback gains and the dimensional derivatives are assumed to vary linearly between these speeds. To cut down on run time, the airplane was moved closer to the ship, to start the simulation, and the initial airspeed became 44.7 knots. There was no requirement to change the data tables because the table look-up routine will give values for 44.7 knots just as it will for all airspeeds between 35 knots and 56.6 knots.

A.9.4 Option 6

The user next specifies the variables that are to be integrated and the locations which contain the integrated values. There is no restriction on the number of variables one desires to integrate as long as the fourth and fifth I array segments are long enough to keep all the R array indices.

Also note that the number of mean equations should equal NSTATES (I array segment 1, element 3). The integration subroutines will only integrate the first NSTATES derivatives specified in the first part of Option 6. When setting up matrices to be integrated it is only necessary to define the R array location of the first element. The number of matrix elements integrated is determined internally from the matrix size information read in previously (Option 2).

Option 6 expects location information for all three pairs of matrices (PDOT and P, etc.) whether the user intends to integrate these or not. A good example of this is the classical pilot model. Refer to Sections A.8.2 and A.8.4 for additional comments on this matter.

A.9.5 Option 7

The variables specified here appear on the output file. Their selection is totally up to the user. All of the output features (tabbing, plotting, etc.) access the file containing the Option 7 specified variables.

A.9.6 Option 11

The variables to be tabbed are user defined. Here we have attempted to tabulate all the key parameters for interpreting the performance of a given task.

A.9.7 Option 4

The case-particular input goes here; i.e., the things necessary to define the environment (wind speed, etc.) and the initial conditions of the airplane and ship.

The initial components of airspeed (segment 8, elements 3 - 5) and initial forces and moment (segment 5, elements 1 - 3) are required. The airspeed requirement could be relaxed, if desired, according to the discussion of Section A.8.7. If the equations describing the means in DEQU were perturbation equations or it was not desired to integrate the means then the initial forces and moment requirement would not longer be valid.

The ship motion inputs KZS, ZETAZS, and WNZS were obtained from Section 9 of this report. The value of KZS is the value of KZ from the table multiplied by ω_n squared. ZETAZS and WNZS are the damping, ζ , and natural frequency, ω_n , presented in Table 9 of Section 9.

A.9.8 Option 28

This option reads data stored from a previous run. It is used here to initialize the matrices P, PE, PXHAT, VU, and VY. A good discussion of the reason for this initialization appears in Section A.8.8 and will not be repeated here.

The important thing is that this setup expects a TAPE28 to be ATTACH'ed (GET'ed) to this job; and for this file to contain numerical values for all the elements of the above mentioned matrices.

To generate the TAPE28 file for initialization the user makes the following changes to the run deck. In Option 2 the value of NSTATES is reduced by one and the value of NØINIT is set to -1. The cards setting RCD as an integrand and RC as the integrator's output should be removed from Option 6. In one of the Option 4's, input RCD (segment 11, element 2) with the value -37.28 (its t = 0 value). Run a 5 second time history using third or fourth order Runge-Kutta integration. An integration stepsize of .025 is adequate. Following the time history (Option 21) call Option 28 and store the desired matrices; remembering to include the necessary control cards to catalog this file for future use.

A.9.9 Option 21

This option generates time histories of the means and covariances. The example presented here asks for a 20 second time history using Adams integration. The output of MISCAL will be printed at the initial time (t=0) and every 20 seconds. The output file is TAPE10.

After the initial call to setup, before the integration process begins the elements of segment eight will be output. This was done to check on the parameters associated with the airwake calculations. It is not necessary to output anything here. But often, the user desires to know some parameter values but does not want to take up space on the output file. This is a convenient place to look at the values of such parameters.

A.9.10 Option 14

This option causes the output file to be tabbed according to the instructions stored by Option 11.

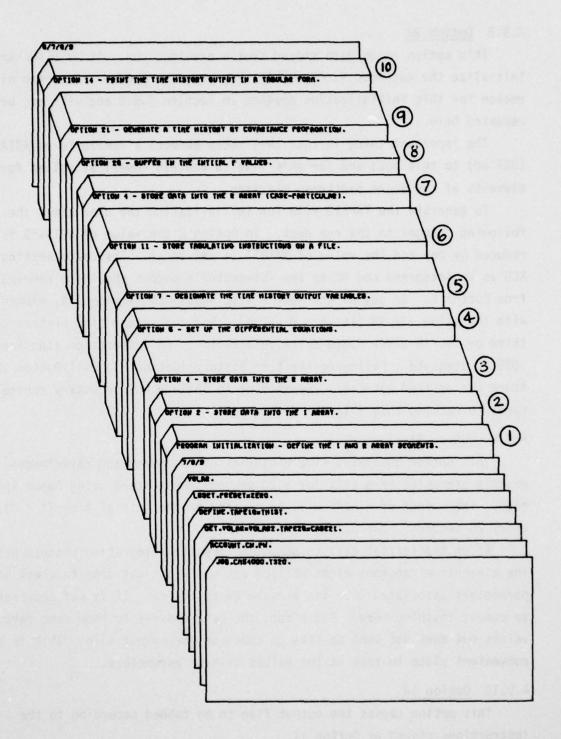


Figure A.8

```
SSEGMNT NSEGI-7, NSEGR-119, NPRNT-1,
              NI(1)=10,0,0,14,14,6,
              NR(11-6,16,10,16,9,11,27,66,7,22,
              NR(111-8,6,6,10,7,7,15,0,0,10,
              NR(21)-10,10,10,10,10,0,0,6,6,6,6,6,
              NR (311-6,6,6,6,6,6,6,6,6,6,6,6,6,6,
              NR(41)=+,6,6,6,6,6,6,6,6,0,1521,
              NF(511-1521,1521,460,225,50,50,75,75,75,75,
              NR(411=75,75,6,6,6,6,6,6,6,6)6,
              NR (71) = 6, 6, 6, 6, 6, 6, 6, 6, 6, 6, 6,
              NR(81)-49,21,56,64,40,36,42,36,42,45,
              NR(911-9,25,9,36,30, 9,324,324,324,324,
              NR(101)-1GE, 324, 324, 324, 324, 9, 12, 6, 6, 6,
              NR(111)=6,6,6,6,6,6,6,6,6,6,6,
     SEND
2
                 READ INTO I ARRAY
              5
                   0
                             NSTATES, NPA, NOM, NGM
                   1
       11
             39
                  15
                        32
                             NPE, NPX, NOAW, NOINIT
       18
             18
                   0
                            BLANK CARD FOR READ I
3
                 PEAD INTO THE R ARRAY
        5
                   0
                            WEIGHT, G, IX, IY, IZ, IXZ
        6
              1
                           O. 1.
LM, WM,LTDM
                32.174
                                                             0.
     16300.
                         Q
        .0
               46.75
                          348.0
                         6 DMEGAU, DMEGAW, KU, KW, KFRPM, KCDN
              1
                2.
     2.
                           3.
                         9 TAUENG, TAUCON, TAUD
                .1
     . 2
                           TABLE FOR AERO DATA)
                 13
                                                                                   1.688
       13
               35.0
                          56.6
                                                61.0
    0.0
                                     60.0
                                                           62.0
       14
                  14
                        10 TABV2 (T TABLE FOR OPEN LOOP CNTRLS)
                2.
     0.
                                      6.
                                                  8.
                                                             10.
                                                                        12.
     14.
                           20.
                16.
                         7 TABEZP
     -1GOCC.
                -1000.
                           -100.
                                      0.
                                                  100.
                                                             1000.
                                                                        10000.
                  16
                         7 TABEZ
       16
                           -100.
     -100co.
                -1000.
                                      0.
                                                  100.
                                                             1600.
                                                                        10000.
                        10
                           TABTC
       20
                  20
                                       .13963
                .13963
                           .13963
                                                  .13963
                                                             .13963
                                                                        .13963
                                                                                     THETAC
     .13963
     .13963
                .13963
                            .13963
                                                                                     THETAC
       21
              1
                  21
                        10
                            TRPMOL
     0.
                0.
                           0.
                                      0.
                                                 0.
                                                             0.
                                                                        0.
                                                                                      RPM 1
     C.
                                                                                      RPH 2
       22
                  25
                        10
                            TCONOL
              1
                0.
     0.
                           0.
                                      0.
                                                 0.
                                                             0.
                                                                       0.
                                                                                      CON 1
                                                                                      CDN 2
     0.
                0.
       23
                  23
                            TOEOL
              1
                        10
                0.
                           C.
     0.
                                      0.
                                                 0.
                                                            0.
                                                                        C.
                                                                                      0E 1
     0.
                0.
                           0.
                                                                                      DE 2
                  24
                        10
                            TABR
       24
              1
    0.0
               0.0
                          0.0
                                     0.0
                                                0.0
                                                           0.0
                                                                      0.0
    0.0
               0.0
                          0.0
       25
              1
                  25
                        10 TABRD
                                                                                  1.69
               0.0
                          0.0
    0.0
                                     0.0
                                                           0.0
                                                                      0.0
                                                0.0
    0.0
               0.0
                          0.0
              -.044
                         t TXU
      27
     -.044
                         6 TYL
                                      -. 044
                                                 -.044
                                                            -.044
                                                                                     XU
       28
              1 28
     .0009
                . 000.9
                           .00+36
                                       .00636
                                                  AFA00.
                                                             45400.
                                                                                     **
```

Figure A.9

29	1 24	6 TXQ					
.035	.035	6 1XQ	.0509	.0509	.0509		XO
30	1 30	6 TXRPP			.0307	THE REPORT OF	1
.2905	.2905	.2457	.2457	.2457	.2457	1917	XRPM
31	1 31	6 TXCON					
0.	0.	0.	0.	0.	0.		XCDN
32	1 32	6 TXPIGV					
0.	0.	0.	0.	o.	0.		XPDIGV
33	1 33	6 TXDE	1414	14.04			
1495	1 34	1424 6 TZU	1424	1424	1424		XDE
0307	0307	0663	0663	0663	0663		20
35	1 35	e TZW					
1425	1425	2148	2148	2148	2148		ZW
36	1 36	6 129		10000000			
3175	3175	4368	4308	4308	4308		20
37	1 37	6 TZRPM					
-2.4375	-2.437		-2.322	-2.322	-2.322		ZRPM
38	1 38	6 TZCON					
0.	. 0.	0.	0.	0.	0.		ZCDN
	1 39	6 TZPIGV	0	•	•		VOLUME
0.	1 40	6 TIDE	0.	0.	0.		ZPDIGV
3388	3388	3328	3328	3328	3328		ZDE
41	1 41	6 TMU					
0012	0012	00226	00226	00226	00226		MU
42	1 42	6 THW					
.00453	.00453	.00316	.00316	.00316	.00316		MW
43	1 43	6 THWD					
0.	0.	0.	0.	0.	0.		MMD
44	1 44	6 140					
1285	1 45	1736	1736	1736	1736		MQ
036	036	6 THRPM	036	036	036		
46	1 46	6 THCON		030	030		HRPH
0.	0.	0.	0.	0.	0.		HCON
47	1 47	6 THPIGV					
0.	0.	0.	0.	0.	0.		MPDIGV
48	1 48	6 THDE					
.2355	.2355	.2383	.2383	.2383	.2383		MDE
63	1 63	6 TKDEU					
-9.064	-9.064	-9.027	-9.027	-9.027	-9.027		
-1.729	1 64	6 TKDEW	. 499				
65	1 65	-1.677 6 TKDEO	-1.677	-1.677	-1.677		
214.67	214.67	6 TKDE0 213.16	213.16	213.16	213.16		
66	1 66	6 TKDET	213.10	213.10	213.10		
368.23	368.23	387.05	387.05	387.05	387.05		
67	1 67	6 TKDEX					
-4.289	-4.289	-4.29	-4.29	-4.29	-4.29		
£8	1 68	6 TKDEZ					
-1.444	-1.444	-1.447	-1.447	-1.447	-1.447		
69	1 69	6 TKDEN					
6123	6123	5986	5986	5986	5986		
9.9987	1 70 9.9987	6 TROFOE	10.	10	10		
71	1 71	6 TKDEDT		10.	10.		
2425	2425	2366	2366	2366	2366		
72	1 72	6 TKOTU		300	12300		
33.44	33.44	36.17	36.17	36.17	36.17		
73	1 73	6 TKDTW					
-19.524	-19.524		-20.189	-20.189	-20.189		
74	1 74	6 TKDTQ					
-655.11	-655.11		-693.91	-693.91	-693.91		
75	1 75	6 TKDTT	*** **				
-409.81	-409.A1	513.66	513.8A	513.PA	513.AF		

Figure A.9 (Cont'd)

```
TKPTY
                  76
       76
              1
                         +
                                       14.05
                                                  14.35
                                                             14.65
      13.34
                 13.34
                            14.05
        77
                   77
                             TKOTZ
      -39.627
                 -39.627
                            -41.653
                                       -41.653
                                                  -41.653
                                                             -41.653
       78
                   78
                             TKDTN
      10.503
                 10.563
                            10.524
                                       10.524
                                                  10.524
                                                             10.524
                             TKOTDE
                  79
       79
                                       -22.298
                                                  -22.298
                                                             -22.298
                 -20.697
      -20.697
                            -22.298
        80
                   80
                             TKDTDT
                                                             9.9985
                                       9.9985
                                                  9.9985
      10.00
                 10.0
                            9.9985
       108
                 108
                            TOEUR
      -.1684
                                       -.149
                                                  -.149
                                                             -.149
                 -.1684
      109
              1 109
                            TOFWR
                 -.1993
                                       -.1723
                                                  -.1723
                                                             -.1723
      -.1993
                            -.1723
                110
       110
              1
                            TDEVX
                 -.3552
                                                  -.3428
                                                             -. 3428
                                       -.3428
      -.3552
                            -.3428
              1 111
      111
                            TDEVXD
      -.2248
                 -.2248
                             .2372
                                       -.2372
                                                  -.2372
                                                             -.2372
      112
                 112
                             TDEVZ
      -.263
                 -.263
                            -.2329
                                       -.2329
                                                  -.2329
                                                             -.2329
              1 113
                            TDEVZO
      113
                                       -.0432
                                                  -.0432
                                                             -.0432
      -.04412
                 -.04412
                            -.0432
                114
                            TOTUR
       114
      . 3245
                 .3245
                                       .06174
                                                  .06174
                                                             .06174
                            .06174
       115
                 115
                             TOTWR
      -.19145
                  .19146
                             .6403
                                       -.6403
                                                  -.6403
                                                             -.6403
       116
                116
                            TDTVX
                 .8613
                            . 5995
      .8613
                                       .5995
                                                  .5995
                                                             .5995
       117
               1
                 117
                             TOTVXD
              1 118
      .68496
                                       .7478
                            .7478
                                                  .7478
                                                             .7478
     118
                            TOTVZ
                          t
                                       -. 9717
                 -.3777
                                                  -. 9717
                                                             -.9717
                            -.9717
              1 119
      119
                            TOTVZD
      -.0884
                 -.0884
                            -.1678
                                                  -.1678
                                                             -.1678
                             BLANK CARD FOR READ R
4
                  SETUP DIFFERENTIAL FOUATIONS
         6
                             UDDT, WDOT, ODDT, TDOT, XAPPOOT, ZAPPOOT
         2
                    2
                             DERPHO
                             XSPDOT
         2
        12
                   12
                          5
                             DED, DTD
        11
               2
                   11
                          2
                             RCD
                             BLANK CARD TO TERMINATE DERIVATIVES
                             UB, WB, QB, THETA, XAPP, ZAPP
                             DFRPM
                             XSP
               1
                   12
                             DE, DT
        12
                   11
        11
                          1
                             RC
                             BLANK CARD TO TERMINATE STATES
        52
               1
                   51
                          1
                             POOT, P
               1
                   99
       100
                          1
                             PEO, PE
                             PXHATD, PXHAT
BLANK CARD TO TERMINATE OPTION 6
       104
               1
                  103
(5)
                            OUTPUT VARIABLES
                 DESIGNATE
                            TIME
                             ALT, VAIR
                             THETA
                          6
                             XAPP, ZAPP
        12
                             DE, DT
                   12
                   12
```

Figure A.9 (Cont'd)

```
UR, WR, GB
ALPHA
ZGS
                                  3
                65
                                 65
                                       THE TAC, FRPNOL, CONOL, DEUL
                                       ACTUAL PANGE
        55
55
55
55
3
55
9
8
                                       SIG THETA, SIG XAP, SIG ZAP
                                       STG FRPM
                         55
55
3
                                       SIG DE
                17
16
7
40
7
27
                                 16
                                       DFRPM
                         55
                                 41
                                       SIG EGS, SIG TO
                                 29
                                       XM, YM, ZM
PSIA
                          8
                30
33
39
          8
                          8
                                 30
                                 35
                                       SICMAVX, SIGMAVY, SIGMAVZ
                                       IMIND, UMEAN, UR, UAW
VWIND, VMEAN, VR, VAW
WWIND, WMEAN, WP, WAW
SIGMA XZ
                43 47 6 1 4 7
        56
11
56
56
                                  6
                         56
                         11
                                       RC, RCD
                        56
56
        56
56
3
                16
                         56
                                 17
                         56
                                 38
                                       XSP
                       STORE TABRING INSTRUCTIONS
6
        11 2 9
                  0
                          NTAP, IPUNCH
        10
                         TIME
                         ALT
        10
                         VA
                                                                                                                       .592417
                         THETA
                                                                                                                      57.29578
        10
10
10
10
10
                         XAP
                         ZGS
                                                                                                                        -1.
-1.
                         ZAP
                50
                         PC
                         XSP
        10
                         TIME
                          DE
        10
        10
                  8
                16
        10
                         RPHOL
        10
                         CONOL
                18 19 26 9
                          DEOL
        10
10
10
9
                          PANGE
                         DFRPM
                         DCDN
                1 TIME
20 SIG THETA
21 SIG XAP
22 SIG ZAP
        10
                                                                                                                         57.3
        10
                23 SIG FRPM
24 SIG DT
25 SIG DE
        10
10
10
10
10
10
10
10
                49
                      SIG XZ
                         TIME
                30
31
32
33
37
                        YM
YM
ZM
PSIA
                                                                                                                        57.3
.5917
                         UWIND
                40
                         YAP .
```

Figure A.9 (Cont'd)

```
.5917
           45
48
41
      10
                UNIND
      10
                WAW
                                                                               .5917
                VWIND
                                                                               .5917
                         BLANK CARD
7
               READ INTO THE R ARRAY (CASE PARTICULAR)
            5
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Figure A.9 (Cont'd)

A.10 A Discussion of the Programmed Equations in Subroutines DEQU and PROP.

DEQU and PROP are the primary subroutines whereby the user defines his problem for analysis. Their importance warrants a more detailed explanation than previously presented in Section A.3.

This discussion addresses the "classical pilot model" example. Once the user is familiar with this example, transition to the more complex "optimal pilot model" example will be simple. Sub-section titles appearing below in quotation marks are the same "Titles" preceding a group of calculations in the subroutines. This provides the user with a one-to-one correspondence between this section and the listings of Appendix B.

DEQU

Subroutine DEQU provides the main program with the differential equations for the mean values of all state and control variables. It also provides the zero subscripted (reference) values of these variables which define the conditions about which the motions are linearized.

"Look-Up Values of Required Longitudinal Parameters"

Recall that the classical pilot model example (Volume I, p. 41) employs lateral/directional airplane dynamics. Nevertheless, the associated equations require some longitudinal parameters. As an example, consider the equation for rate of change of roll attitude:

$$\Phi = P + Q \sin(\Phi) \tan(\Theta) + R \cos(\Phi) \tan(\Theta)$$

Q and Θ are longitudinal parameters. Required to generate Φ .

This section of coding provides the necessary longitudinal parameters as a function of time. Values of the longitudinal parameters for the reference trajectory are stored in the appropriate tables; at the desired time instant, values are determined by table-look-up. When performing an initialization run the table-look-ups are made only once.

"Miscellaneous Calculations"

Calculations performed here include:

(a) $\Theta = \Theta_c$. This sets airplane pitch attitude equal to the pitch attitude from the table-look-up of the previous section.

- (b) Ship vertical position is set to zero (ZSP = 0).
- (c) Perturbation values for roll rate and yaw rate are evaluated; for example, $p = P P_0$, where p is the perturbation, P is the total roll rate and P_0 is the reference value. The reference values are updated at the end of each integration increment as part of the quasilinearization process.
- (d) The remaining calculations are performed to minimize the number of calls to the trigonometric functions used throughout the remainder of the subroutine.

"Altitude"

Due to the standard axis convention, altitude is "minus z".

"Airplane With-Respect-To Ship, Earth Axis"

Both the ship and the airplane are referenced to a fixed earth axis system. These equations calculate the x, y, and z components distance between the aircraft c.g. and the ship c.g. in that earth axis system.

"Airplane With-Respect-To Ship, Ship Wind Axis"

The airwake model requires the coordinates of the airplane relative to the ship to be in ship wind axes. These equations transform the earth axis distances to ship wind axes. The parameters DXM145, etc. were calculated in subroutine SETUP.

"Euler Angles for Airwake Model"

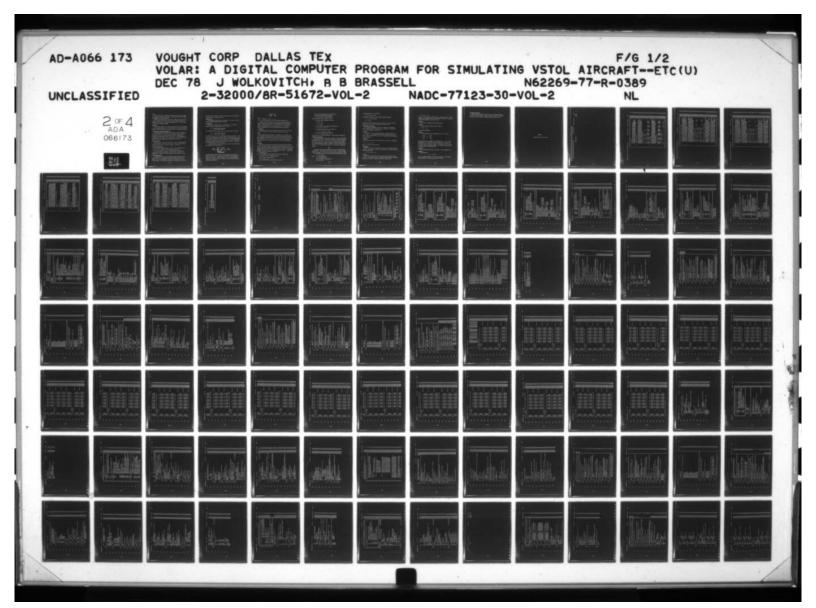
These are Euler angles of the airplane with respect to the ship wind axes and are necessary inputs to the airwake model equations. They are simplified greatly because the airwake model used does not pitch and roll with the ship.

"Ship Airwake"

If ship airwake is desired (NOAW = 0) subroutine AIRWAKE is called. Following the call to AIRWAKE, the airwake related parameters are available in COMMON.

"Airplane Body Axis Components of Ambient Wind"

These equations transform the ambient wind velocity, which is given in earth axes, to the aircraft body axes. Wind velocities are defined consistent with the earth axis reference, i.e. a positive x-axis wind is oriented in the positive earth axis direction.





"Wind"

Total wind velocity is composed of the ambient wind and the non-random disturbances introduced by the airwake. This section defines the non-random wind components in aircraft body axes.

VOLAR is currently set-up to initialize on airspeeds instead of inertial speeds. Equations for initializing total inertial velocity components are contained in this section. They are calculated once only. This calculation is controlled by the ICEES parameter.

"Airspeed"

Wind velocity components are subtracted from inertial velocity components to yield airspeed components in the aircraft body axis system. Angle-of-attack, sideslip, and total airspeed are calculated according to standard conventions.

"Look Up Aero. and Open Loop Parameters"

Aerodynamic stability and control derivatives are stored in tables as a function of airspeed. This section of the program performs a table-look-up of these derivatives at the current value of airspeed. Subroutine TLU evaluates several dependent variables with one call. Fifteen parameters, YV through NDR (R array, segment 10), are determined by the single call to TLU. Open loop aileron and rudder control deflections are set to zero.

"Range From Ship"

Range from ship is arbitrarily defined here as the distance between the x earth axis positions of the ship and airplane. "Range", as defined here, provides some measure of how close the airplane is to the ship.

"Lateral Position Error"

The aircraft's commanded lateral position is the lateral position of the ship. Error in position is the difference between the two.

This section begins the build-up of parameters associated with the calculation of pilot control inputs. Figure 8 (Volume I, page 40) is a schematic of the classical pilot model employed for the AV-8A at low speed.

"Roll Attitude Error"

Commanded bank angle is a gain multiplied by lateral position error.

Bank angle error is the difference between the commanded and actual bank angles. This error is modified by a bias term to account for the initial trim bank angle. A non-zero initial bank angle is necessary to trim out the

side forces on the airplane. These side forces result from the steady side velocity required for tracking the ship.

"Heading Error"

The commanded aircraft heading is zero degrees. Heading error is the difference between commanded and actual heading.

"Roll Control"

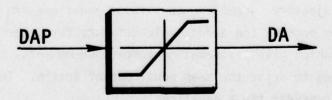
The pilot's roll control input is calculated here. From Figure 8 (Volume I, page 40) the appropriate transfer function is:

$$^{\gamma}P_{\phi} = \frac{-112.0 (s + 0.1) (s - 10.0)}{(s + 10.0) (s + 10.0)}$$

This transfer function was obtained from the following transfer function.

The quantity K_1 (τ_{L1} s + 1) is the compensation applied by the pilot. A lag, (τ_a s + 1), is introduced to represent actuator and neuromuscular lags. The final numerator and denominator factors provide a first order Pade approximation to a pure time delay. This delay represents the time it takes the pilot to generate an output strategy following sensing of the error. Time delays are a standard feature in most pilot models.

As presented in block diagram form below, the pilots' output, DAP, must pass through a control system limiter.



Subroutine DESCRIB calculates the non-linear describing function which represents the limiter. A necessary input to DESCRIB is the standard deviation of the signal DAP. A general equation for calculating the standard deviation of a parameter which is a function of the state variables but not a state variable itself is:

$$y = \sqrt{\left(\frac{\partial y}{\partial x}\right)^T P \left(\frac{\partial y}{\partial x}\right)}$$

where $y = f(x_1, x_2, ..., x_n)$

and P is the Covariance matrix associated with the state vector $\underline{\mathbf{x}}$.

Normally the standard deviation of the control would be evaluated by describing functions and the mean would be determined by applying the true limiter. This was not done here. For this application, the difference in results was insignificant and so the modified mean (i.e. its describing function representation) was used to reduce the number of calculations.

"Yaw Control"

This section is so similar in layout to the previous one it will not be discussed. The output is, of course, the yaw control from the pilot.

"Ship"

Only the mean lateral ship motion is considered for this example. The ship is steaming with velocity V5 in a direction PSI5 with respect to north. When integrated, the differential equation in this section yeilds the y earth-axis position of the ship. The x and z earth-axis positions were defined in previous sections of this subroutine; one by table look-up and the other by equation.

"Airframe"

This section of coding defines the differential equations which describe the aircraft's mean trajectory. Complete non-linear equations are used. This creates a small problem because the aerodynamic data are furnished as dimensional stability derivatives which give perturbation forces and moments. Total forces and moments are required to drive the mean equations of motion. To demonstrate how this is overcome, consider the V equation.

Some definitions:

Let Yo be the total side force divided by mass at some reference time.

 δ_{A} and δ_{R} are the pilot commanded positions

δAOL and δROI are open loop inputs

vas is the perturbation airspeed along the y body axis

p and r are the perturbation roll and yaw rates.

P and R are the total roll and yaw rates

U. V. and W are total airspeed components

Based on these definitions proceed as follows:

1. the total control deflection is given as:

$$\delta_4 = \delta_A + \delta_{AOL}$$

$$\delta_5 = \delta_R + \delta_{ROL}$$

2. the incremental or perturbation force-over-mass is:

$$\Delta Y = Y_v v_{as} + Y_p p + Y_r r$$

3. the total force-over-mass on the airplane is:

$$Y = Y_0 + \Delta Y + Y_{\delta_A} \delta_4 + Y_{\delta_R} \delta_5$$

4. the rate of change of side velocity is:

$$\dot{V} = Y + g \cos(\Theta) \sin(\phi) - R U + P W$$

Thus the total y-axis velocity component, V, can be found by integrating V.

"Update Sub Zero Values"

The zero subscripted values define the reference trajectory about which quasilinearisation occurs. Perturbation quantities are found by subtracting the reference value from the total value. The reference values are updated prior to each integration increment and remain fixed during the increment. Zero subscripted terms also appear as elements, or parts of elements, in the F matrix. (F is the system matrix appearing in the covariance propagation equation.)

PROP

Subroutine PROP has only one purpose; to furnish the integration subroutine with P. The prospective user should keep this in mind when reading through the subroutine. Familiarity with state variable notation is helpful.

As an overview, consider the system governed by the differential equation.

z = F z + GM W

where

z is the state vector,

F is the system matrix

G_M is a control or coupling matrix

w is white noise

The covariance matrix, P, is defined by:

$$P \stackrel{\triangle}{=} E \{ (\underline{z} - \overline{z}) (\underline{z} - \overline{z}) \}$$

and obtained by integrating the following differential equation.

$$\dot{P} = F P + PF^{T} + G_{M} Q_{M} G_{M}^{T}$$

$$Q_{m} = E \{ \underline{w} \underline{w} \}$$

Each of the titles preceding a group of calculations in subroutine PROP is explained below, with the titles repeated in quotation marks.

"Miscellaneous Calculations"

This group of calculations provides some frequently used parameters. They are grouped here for "one time per call" calculation. This minimizes calls to the trigonometric functions, etc.

"F1 Matrix"

The F1 matrix is the aircraft system matrix. Aircraft states are v, p, r, ϕ , ψ , and y. F1 is developed from the standard linearized equations of motion. Refer to Section 2.0 in Volume I for a description of the linearized aircraft equations.

"G1 Matrix"

G1 is the control matrix for the airplane. The airplane is represented by:

$$\frac{\dot{x}}{\dot{x}} = F_1 \underline{x} + G_1 \underline{u}$$

where <u>u</u> is a vector of control inputs.

"Gamma Matrix"

Gamma is the matrix for coupling the colored noise disturbances with the airplane. If \underline{w} ' represents a vector of colored noises, the equations describing the airplane motion are.

$$\underline{x} = F_1 \underline{x} + G_1 \underline{u} + \Gamma \underline{w}'$$

"A Matrix"

The A matrix and the B matrix (next section) define the noise coloring processes. In this example, noise is composed of Dryden atmospheric turbulence, plus the ship's airwake. Equations for the noise take the form:

$$\dot{\underline{w}}' = A\underline{w}' + B\underline{w}$$

where \underline{w}' is the colored noise (output) and \underline{w} is white noise (input). Dryden turbulence is represented by a first order filter (in each axis). Each axis of ship airwake requires a second order filter.

"B Matrix"

The B matrix is explaned in the preceeding section.

"C Matrix"

C and R_L are used to define the control input, \underline{u} .

$$\underline{u} = C\underline{x} + R_{\perp}\underline{u}$$

 \underline{x} and \underline{u} are explained above.

"F Matrix"

F is the system matrix for the augmented vector $\underline{z}^T = (\underline{x}, \underline{w}', \underline{u})$:

$$F = \begin{bmatrix} F_1 & \Gamma & G_1 \\ 0 & A & 0 \\ C & 0 & R_L \end{bmatrix}$$

The subroutine LAYIN is designed to store submatrices $(F_1, \Gamma, \text{ etc.})$ into a larger matrix (F). By building F from its submatrices; (1) the user has more visibility of the pieces, (2) there is less chance of an error in row or column placement of individual elements, (3) elemental model additions or size changes can be incorporated quickly.

"GM Matrix"

 G_M is the multiplier of white noise inputs. For this example $G_{;;i} \equiv B$.

"QM Matrix"

 Q_M is defined by:

$$Q_{M} = E \{ \underline{w} \ \underline{w}^{T} \}$$

The (1, 1) element corresponds to the Dryden turbulence and the remaining diagonal elements are associated with the ship's airwake.

"Propagate Covariances"

These operations develop \dot{P} from F, G_M , and Q_M . Matrix operations are identified in subroutine MATRIX. MATRIX is written in COMPASS; but FORTRAN equivalent subroutines appear as comments preceding each ENTRY point.

APPENDIX B

LISTING FOR CLASSICAL PILOT MODEL

VOUGHT LAUNCH AND RECOVERY PROGRAMKING NOTES.

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	IV. I AND	PROPLI	GROUP	LENGT	SPECI	2 1	I AND	REOUT	AND R	CCCUR	LOCATION	ANA	*COMDECK	AIRWAK	*COPD	ADAMS	*COMDECK	ADAMS	330403+	NEAPL	WITHI	VAPIA	A CHA	SINCE	TIME	CHANG	LCCAT	12.
PRUCRAMING NOTES	2	• • •	••	••		• •	• •			••			••	••	••								• • •	••	••		• •	• •

COMPASS 3.3-428.

THE INITIAL INPUT TO THE PROGRAM IS A NAMELIST, SEGMNT,

VOTES	JTE	DIE	DIE	OTE	1	5	JIE	OTE	DIE	OTE	DIE	OTE	DIE	OTE	OTE	OTE	CTE	OTE	OTE	OTE	OTE	OTE	DIE	OTE	OTE	DTE	OTE	CTE	OTE	TE		36	OTE	OTE	016												
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WHICH DEFINES THE NUMBER OF SEGMENTS AND THE LENGTH OF EACEGRENT CONTAINED IN THE I AND R ARRAYS. THIS INFORMATION IS STORFD IN & LARFILLED COMMON BLOCK, /SEGMENT/, CONTAINED IN *CCMDECK* SEGMENT, ADDING OR DELFTING VARIABLES FROM AN

FXISTING SEGMENT REQUIRES A CHANGE TO THE ASSOCIATED INPUT FCR THAT SEGMENT, ADDING SEGMENTS TO THE TAIL END OF THE I OR R ARRAY RECUIRES AN ADDITIONAL INPUT FOR EACH ADDITION/ SEGMENT AND A POSSIBLE INCREASE IN THE ARRAY DIMENSION FOR THE ASSOCIATED I OR R ARRAY DESCRIPTOR IN *COMDECK* SEGMEN

COPDECK SEGMENT IS CALLED FROM *DECK*S :

CCPDECK INTEG VI.

WHICH IS USED TO HOLD TWO SINGLE-DIMENSIONED ARRAYS OF LENGTH MEDU WHERE NEOL IS THE SUM OF THE NUMBER OF STATE VARIABLES AND THE SOUARE OF THE NUMBER OF ROWS IN THE COVARIANCE MAIRIX. THESE ARRAYS ARE USED TO HOLD TEMPORARINTEGRATION VALUES. IT SHOULD BE NOTED THAT THESE ARRAYS ALS USED AS SCRATCH MATRICIES IN ROUTINE SOLVE WHICH PREVENTS SOLVE FROM BEING CALLED FROM WITHIN THE INTEGRAT LOOP (SEE SCLVR NOTES). AN INCREASE IN THE NUMBER OF STAT VARJARLES OR NUMBER OF ROWS IN THE COVARIANCE MATRIX REQU THIS *COMDECK* CUNTAINS A LABELLED COMMON BLOCK, /INTEG/,

COMDECK INTEG IS CALLED FROM *DECK*S

A CHANGE IN THE ARRAY DIMENSIONS.

RUNGE PROP KUTTA ADAMS

VII. *COMDECK* GDF

THIS *COMDECK* CONTAINS THE LABELLED COMMON BLOCK, /GDF/*WHICH IS USED TO HOLD THE NUMBER OF DESCRIBING FUNCTION, FUNCTIONS THEYSELVES AND INDEXES FOR THE FUNCTIONS. IF TNUKBER OF DESCRIBING FUNCTION INCREASE, THE DIMENSION ON FUNCTION VALUES (TABLE) MAY NEED TO BE INCREASED.

COMDECK GOF IS CALLED FROM *DECK*S :

TABRD DE SCR 18 The same of

VUILL CENTRAL MEMORY RECUREFERIS AND EXCUIDENT TIPE VIII. CENTRAL MEMORY RECUREFERIS AND EXCUIDENT TIPE SEVERAL SITES SERVER TAKEN TO RECURE FERENA AND THE SIEPS REQUIRED NOTES THE ALABASE MODIL WAS PRICEDS SIEPS WERE TAKEN AND THE SIEPS REQUIRED NOTES THE ALABASE MODIL - **OECT'S AIRWAYE AND AINWISE TO NOTES THE ALABASE MODIL - **OECT'S AIRWAYE AND THE SIEPS REQUIRED NOTES THE ALABASE MODIL - **OECT'S AIRWAYE AND AINWISE TO NOTES THE ALABASE MODIL - **OECT'S AIRWAYE AND SIGHA VY AND SIG	PAGE	ESS	SSSS	E S	222	SES	E E E	2222	22:	SES	ES	SES	ESS	ES	ESSE	ESS	ES	ESS
N		NON		N	O O O	NON	N N N	2000	22	222	20 Z	222	222	2 2 2	222	222	252	ZZZ
9	15.13.15		F AND CENTR DESIGNED T		COKUPS TO A VZ BASED UPON	HIP. EACH TABLE TO THE R ARRAY GUNT OF CODING	X TABLES ARE S PERFORMED ON EQUIRES THE	HE R ARKAY IN TED BY BLE LOOKUPS IN		ARPAY OF THE	AY TO BE USED ORAGE REQUIRED	NS OF THE E STORED INTO IN FACH MATRIX	. ELLIPSE AND	E PLOTS ON AN	E. SHOULD THE E ASSOCIATED INFS SHOULD BE		PLOT GN A	ARE ABY 3
	.85	ECUTION	E EXECUTION T © DISCUSSION TAKEN AND THE	-	A VY AND SICH	LAKE TO THE S 15 PLACED IN REDUCE THE AM	OKUPS, ALL SI THE LOOKUP I TABLE. THIS R	OCATIONS OF TAN BE PLIVIA ORMING THE TA	A AND ADAMS	WITHIN THE PATENT AND THE	NTO THE 1 AFR AMBUNT OF ST	EMENT LOCATIO IVE PATRIX AR OF ELEMENTS	AXIS, DASPLT	SEO TO PRODUC	LCOMP SCFTWAR UTINES AND TH KE THESE ROUT		7 8Y 7 INCH	SPACE THE 61 HTS CAN BE PE ARPAY RATHER
	3.3-4	FNTS AND	THE FOLLOWING	S AIRWAKE AL	CRPS A SERI	ENTRIES AND ORDER. TO	HE TABLE LO SE TABLE AND THE LARGER	NSECUTIVE LIGER. THIS C. OF CODE PERFI	RUNGE, KUTT	TE LUCATIONS	HEN STORED I	THE FIRST EL THE DERIVAT	K#S CALPLT,	SECK+S ARE U	SUCIATED CA	IAF.	TO PRODUCE A	IND TO SAVE
9	ະ	RECU	OUIPEMENTS WHERE THE	30+ - 7300	AKE MUDEL PERF	SEVENTY-FIVE POVE PENTICNED	T TO PERFUPM TED AS CHE LARGER SECTION OF	E PLACED IN CO E MENTIONEC OF THE SECTION C	DRS - +DECK+S	RIABLES, THE	CATIONS APE TH	GE MATRIX AND RAY BLONG WITH	PLOTTEP - *DEC	E MENTIONED +C	LITY OF THE AND NOT BE AVAILA	FROM THE PROGR PLOTTER - +DE(TINE IS USED 1	NTO AN ARRAY PER INTO T 60-1
0	w	ATRAL	E K	. AIRW	THE AIRE	CONTAINS IN THE A	CONSIDER THE PROP	TABLES B THE APOV ALTERING ROUTINES	B. INTEGRAT	THE USER	THESE LO	BY THE I COVARIAN THE I AF		THE ABOV	AVAILABI SOFTWARF INPUT OP		THIS ROU	COMPRESS STORING
CH AND RECOVERY PRO	AHFING			••	• • •	• • •	•••	••••	•••		••	• • •	•••	• • •	•••	•••	•••	••••
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NOTES NOTES NOTES NOTES NOTES NOTES INTEGRATORS. IT IS ALSO USED TO HACK NON-TIME VARING NUMBERS. AS AN EXAMPLE, THE AIPLAKE MODEL REQUIRES THE WIND-OVER-DECK AND SHIP HEADING WHICH, ONCE SET, NEVER VARY. IN KEEP THESE HACKS OUT OF THE INTEGRATION LOND, THEY ARE PERFORMED IN THIS POUTINF IS CALLED PRIOR TO INTITATING THE INTEGRATION LEOP. IT IS USED TO HACK THE INITIAL VALUES USED BY THE E. INTEGRATION INITIATION - *DECK* SETUP

F. TARLE LOOKUP KOUTINE - *DECK* TLU

THIS KOUTINE IS USED TO LOOK UP A SERIES OF VALUES BASED UPON A SEPIES OF TABLES AND A SINGLE INDEPENDENT VARIABLE. THIS RECUIRES THAT ALL DEPENDENT VARIABLE TABLES TO RE LOCKED UP BY A SINGLE CALL MUST HAVE THE SAME NUMBER OF ITEMS IN THE TABLE AND BE LOCATED IN CONSECUTIVE AREAS OF COME. THE DEPENDENT VARIABLE VALUES WILL RE PLACED IN A CONTIGUOUS AREA OF CORE IN THE SAME ORDER AS, THEIR TABLES ARE ARRANGED.

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COVAPIANCE MATRIX INITIALIZATION - *DECK* SOLVR

THIS RCUTINE SOLVES FOR P IN THE PICCATI FOLATION

P + F TRANSPOSE + F + P + G + O + G TRANSPOSE . O

AND THE TWO SCRATCH INTEGRATION MATRICIES ARE USED FOR THIS PURPOSE. THIS PREVENTS CALLING SOLVP INSIDE THE INTEGRATION LOOP TO FIND THE STEADY-STATE P MATRIX. THIS CAN BE ACHIEVED BY ADDING 3 ADDITIONAL N BY N MATRICIES TO ROUTINE PROP AND PLACING THESE MATRICIES INTO THE CALL TO SOLVR. TO INITIALIZE THE COVARIANCE MATRIX. THE ROLTINE NEEDS 3 N BY N SCRATCH MATRICIES (N. NUMBER OF ROWS IN COVARIANCE MATRIX P). TO SAVE SPACE, THE COVARIANCE DERIVATIVE MATRIX

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MATRIX MANIPULATION - *DECK* MATRIX ÷

DCCUR IN GENERATING THE COVARIANCE PATPIX. SINCE THE TIME REQUIRED TO PULTIPLY TWO MATRICIES RISES EXPONENTIALLY WITH THE SIZE OF THE MATRIX, THESE ROUTINES HAVE BEEN COLLECTED INTO An ASSEMELY LANGUAGE ROUTINE. THIS ROUTINE IS DESIGNED IN SIDE THE COUNTY THE SIZE OF THE COUNTY THE GOOD, THEREBY REDUCING THE EXECUTION TIME SIGN FICANTLY. WE REALIZE THIS MAKES DEBUGGING AND MOUSFICATION OF THE MATRICIES INVOLVED AND THE NUMBER OF TIMES THE RATRICIES INVOLVED AND THE NUMBER OF TIMES THE ROUTINES ARE CALLED, WE FEEL IT IS ADVANTAGEOUS TO USE THE ROUTINE IN ITS PRESENT FORP, THE FORTHAN EQUIVALENT OF THESE ROUTINES HAVE BEEN GENERATED AND ARE AVAILABLE FOR USE SHOULD THIS ROUTINE BE UNDESTRABLE. SEVERAL MATRIX MANIPULATIONS (ADD, MULTIPLY AND TRANSPOSE)

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	COMPASS 3.3-428.	•			~		TIUN ROUTE	S APE SGUA	IMENSIONIN	THAT THE			*********
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	VOUGHT LAUNCH AND RECOVERY PROGRAMMING NOTES.		•		. 17.	•		•		•	•	•	********
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	(IN(I),I"K1,K2)	VOLAR	166
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	NT.FG.23 CALL		203
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506	INUE	VOLAR	803
		VOLAR	804
	C see PRINT RESULTS FOR THIS INTEPVAL.	VOLAR	895
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	1111 N1 • N1 + 1	VCLAP	268
010	0	VOLAR	808
	IF (DTDUT 2.6T.C.O.AND.NI.6E.NZ) I . 1	VOLAP	800
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23011	11 FCF41(5x,10f12.5) 22 FCF441(f410) 33 FCF441(15,5x,6410)	VOLAR	958 959
24004	FERFA	VCLAR	961
24008		VELAR	696
24011	444	VCLAR	666
980 25002	FURNATUTHIS SY,	VELAP	968
250	FULFATI	VCLAR	969
25007	F CR MATC	VCLAR	971
985	CHFILEW 12/1	VOLAP	973
25052	FERMATO	VCLAP	975
26002	02 FORMAT(FAIO)	VOLAR	976
20022	FURMA		976
0.00	LING AT SEGMENTS 12,8 H FLFMENTS 12,1H.		979
50072	T SEG		980
27004			982
995	11NG AT SEGRETI12,8H ELEMENT,12,1H.)	VOLAP	983
	AT SEGRENTIZION ELEMENTIZITE.		985
270	27006 FRAMIST, 69HPXDDI AND PX INDICES ARE STOPED INTO THE I ARRAY BEGI		986
1000	31001 FCRMAT(1615)	VOLAR	988
31002	FORMA	VCLAR	686
31004	1 4HENGIF(1) /)	VCLAR	990
	FOPMAT(///5x, 1615)	VCLAR	266
31008	08 FRMAT(415,5410, E10.3)	VOLAR	663
31013	FURNAL (VILAR	999
	1 6PFILEWs, 12/)	VOLAR	900
31025		VCLAR	466
1010	1 SYNDET CO. 12/5×2HCOLNCHO.12/1	VOLAP	866
320		VOLAB	1000
32003	7	VOLAR	1001
	60	VOLAR	1002
32006	-	VOLAP	1003
32002	2 5	VCLAR	1004
766	-	VELAR	1006
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1020		VCLAR	1008
		VOLAR	1000
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		VCLAR	1012

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	av 101	•	•	1001 FFF	1002 FUR	OO3 FOR	.005 FUR	FOR FOR	1012 FCF	013 FCP	FND
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CCPPON F1(6,4), G1(6,4), 1	I , , , , , , , , , , , , , , , , , , ,							+0	
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	•	EGFENTS 81-106	«	163

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		26.60	10.88	.54		37.00	34.62	-	24.78			VSS - 35		,	37.00	25.18	3.43	34.75	32.14		37.00	19.8	46.36		6.33	37.00		59.29	6.6	57.34	6.34	VSS . 35			37.00		48.77	2.67	2	10.41	37.00	
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			,								ATRUTRI		
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			00.0	•	•	00.0	152.0	250.0	8417	\$1- ·	ALKWIDE		
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	0.0		65.99	32.F1	• •	6.43	30.50	36.76			AIRWIRL	205	

Estimate Sections

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24-18 27-88 AIRWIBL 208 21-71 40-96 AIRWIBL 209 AIRWIBL 209	2WT9L	.34 , 57.35 , AIRWIBL	18VT8L	4-48 / AIRWIRL	G. AIRWTBL	IRVTBL IRVTBL	IRVIBL IRVIBL	AIRWTBL	IRVT8L	RETBL	IRVTBL	RVTBL	1RWTBL	IRWIRL	RVTBL	IRWTBL	IRVTBL	IRWIEL	RVT8L	IRWTBL	IRWTBL IRWTBL	RUTRL	IRWTBL	IRM TRL	IRVTBL	RVTBL	IPUTPL	101181	IRWTBL	RVTBL
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24-18 + 27-88 + 21-71 + 40-96 +	25.0 250.0 2TAB44	.34 , 57.35 ,	43.69	1 85.4	•		AB14				•	4825				•	**				4 4	•				14				
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of their dation	54.0 63.90 · 35.23 · 2 104.0 37.50 · 24.73 · 1	104.0 63.90 · 35.23 · 2 C Y X • 0.00 37.00 9	63.90 · 35.23 · 37.50 · 24.73 · X • 0.00 37.00 · 75.57 · 82.79 · · 78.50 · 75.15 · · · · · · · · · · · · · · · · · · ·	54.0 63.90 35.23 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.73 7.50 24.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 27.75 7.50 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106.00 106.00 106.00 106.00 106.00 106.00 106.00 106.00 106.00 106.00 106.00 106.00 106.00	104.0	104.0	104.0	104.0	104.0	16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 16.75 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7.	TABLE 11C. VY AT VSS - 33 TO 90.00 125.0 250.0 27AB14 TABLE 11C. VY AT VSS - 35 KT AND SIS - 9.05 7.05 7.05 7.05 7.05 7.05 7.05 7.05 7	0.0			1		8 8 9	4.50			ATRATE	
	1.60 0.75 3.75 5.71 1.65 1.60 0.75 3.75 5.71 1.65 1.60 0.00 37.00 90.00 125.0 250.0 1.60 1.30 0.05 0.05 0.05 1.60 1.30 0.05 0.05 0.05 1.60 1.30 0.05 0.05 0.05 1.60 1.30 0.05 0.05 0.05 1.60 1.30 0.05 0.05 0.05 1.60 1.30 0.05 0.05 0.05 1.60 1.30 0.05 0.05 0.05 1.60 1.60 0.00 125.0 250.0 1.60 1.60 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 125.0 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 1.60 0.00 0.00 0.00 1.60 0.00 0.00 0.00 1	18.75		35	1	-0	30	3.39			ATPLIAL	
7.		54.0		. RO			17.	1.65			ATPETRE	
75	77	104.0		.33	. 4	3	. 79	-2.29			AIRWIRL	
75	7.	3									AIRVTEL	
TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DEG. DATA TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DEG. TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DEG. DATA TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DEG. V	0.17	٠. ٠			-	.06	25	50	2748	**	AIRVTBL	
TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. DATA TABLE	75	J									AIRNTBL	
TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. DATA TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. DATA TABLIC/	TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. DATA TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. DATA TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. V	-18.75		64.	•	3.34	2.25	4.80			AIRWTBL	
75	2.66	٥.٠		.69	0	0.05	-0.53	50.2			AIRWTBE	
TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. DATA TABLIC/ X = 0.00 37.00 90.00 125.0 250.0 Y	TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. DATA TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. TABLE IIC. VY AT VSS = 35 KT AND SIS = 30 DFG. V	18.75		.66	-	0.52	-0-10	-0.69			AIRNTBL	
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7.	7	24.0		.45	-0-3	i	90	-2.13			AIRLTRL	
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2.74 p -4.45 p -3.97 p 1.31 p 2.38 -9.64 p-10.33 p -7.00 p -0.16 p -0.55 0.93 p -4.11 p -1.64 p 5.05 p -2.81 6.03 p 10.44 p 3.57 p 0.99 p -6.71 x = 0.00 37.00 90.00 125.0 250.0	7.74 p -4.495 p -3.97 p 1.31 p 2.38 p -9.64 p-16.33 p -7.00 p -0.16 p -0.55 p 6.03 p 10.44 p 3.57 p 6.99 p -6.71 p x = 0.00 37.00 90.00 125.0 250.0 77AB = -25 0.67 p -2.99 p 0.70 p 3.88 p 7.51 p	-18.75		•	:	, -3.73	5.00	3.41			AJRNTBL	
-5.64 ,-16.33 , -7.00 , -0.16 , -0.55 C.93 , -4.11 , -1.64 , 5.05 , -2.81 6.03 , 16.44 , 3.57 , 6.99 , -6.71 X = 0.00 37.00 90.00 125.0 250.0	7.64 y-16.33 y-7.00 y-0.16 y-0.55 y C.93 y-4.11 y-1.64 y 5.05 y-2.81 y 6.03 y 10.44 y 3.57 y 6.99 y-6.71 y x = 0.00 37.00 90.00 125.0 250.0 71AB s-25 0.67 y -2.99 y 0.70 y 3.86 y 7.51 y	2.5		•		3.07	1.31	2.38			AIRWIBL	
6.03 p 1C.44 p 3.57 p 6.99 p -6.71 x = 0.00 37.00 90.00 125.0 250.0	C.93 p -4.11 p -1.64 p 5.05 p -2.81 p 6.03 p 1C.44 p 3.57 p 6.99 p -6.71 p x = 0.00 37.00 90.00 125.0 250.0 7TAB p -25 0.67 p -2.99 p 0.70 p 3.88 p 7.51 p	16.75		•	;	00.7- 1	-0.16	-0.55			AIRVIBL	
6.03 , 1C.44 , 3.57 , G.99 , -6.71 x = 0.00 37.00 90.00 125.0 256.0	x = 0.00 37.00 90.00 125.0 250.0 77AB = -25 0.67 p -2.99 p 0.70 p 3.88 p 7:51 s	54.6		•	;	, -1.64	5005	-2.81			AIRWTRL	
0.00 37.00 90.00 125.0 250.	0.00 37.00 90.00 125.C 250.0 71AB = -25 0.67 p -2.99 p 0.70 p 3.88 p 7:51 s	104.0			:	3.57	60.0	-6.71			AIRWTBL	
0.00 37.00 90.00 125.0 250.	0.00 37.00 90.00 125.C 250.0 71AB25 0.67 p -2.99 p 0.70 p 3.88 p 7:51 s	u									AIRWTBL	
	.87 p -2.99 p 0.70 , 3.88 ; 7:51 ;				-		5	20.	1	-2		
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15.13.13	321 322 323 324	326	328	331	333	336 336	33.8	340	341	343	345	347	348	350	351	353	355	356	358	359	360	362	364	365	367	368	370	371	373	375
2/08/78 1	AIRWTBL AIRWTBL AIRWTBL	PET	IPWT	1861	777	RET	IRWI	IRVI	2 2	IRE	IRV	2 3	REL	IRET	IRWI		IPWT	IREL	154	INT	IRW	IRE	FEE	IRV	RE	IRVI	IRET	IRVI	FET	IRMI
-		TAB44					ZTAB14				36 - 2	7 4				74846								21.0 - 11.	- 0				2TAB25	
FTN 4.64428	4.98 , 2.20 , 4.05 ,	2 0.03	222		F.G.		20.06	1.19	3.27	2.67 ,			**	2.42 ,	.24	200		.17	0.03	6.45 ,	1.66	E6.		0		48	.83		20.0	
•	1.56 ; 3.35 ; 9.36 ; 3.22 ; -	125.0 2	66 .	1 1 1	15 - 30 D		125.0 2	5.98 ,	71 , -	- , 79.0		0.00	.13 ,	7.09	.15 ,	6 00.5		9 9	9.7	14.82 ,	7	118 - 50 0		125.0	2.5	-2.89	09	8.	125.0 2	
	14.56 14.46 14.95 14.95	00.06	~~,	6.58	KT AND S		00.06	-12.87	. 2	1.86	• •		2.52	4.28	8.80	60.00	•	15.06	21.	, 19.13 ,	x	S KT AND S		00		-0.07	-4.P1		00.06	
	-1.48	37.00	2:1	.31	r vss - 45		37.00	-1.94	2.36	-1.21	07.	:	11.91	2.27	• 50			2.5	2.94	15.27	040	T VSS . 4		27 00		20	-15.71	8.26	37.00	
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14/14		*			TABLE II	DATA TABILE!	*				•											TABLE II	DATA TABILF/	,					*	
TE ALKWIN	18.75 24.6 164.6	۶ ا	0.0	24.0	.:	•	٠.	-18.75	18.75	54.0	,		-18.75	18.75	54.0			-18.75	18.75	24.0	104.0	:.		>		-18.75 0.0	18.75	104.0	٠ د د	J
SUBROUTINE AIRNTBL		920		525					. \$38			940				6		250				988			996			565		

	SUBPOUTINE AIRWTBL	11RWTBL	14/14	0PT-1					FTN 4	.6+42		12/08/	1 82	5.13.13	PAGE
		;							•				-		
		10.01		1.50	97.1- 1	-	. 00.	75.6	01.6				181	378	
		2000		-0-1	3.1			20.	1:1			AIN	181	379	
		3.501		10.01	13.5	•		• 33	-2.5			AIKE	181	380	
	•											AJEN	181	361	
575	3		• ×	00.0	37.00	96	00.	125.0	250.0		ZTAB .	HAIN 55-	181	382	
	·											AIRM	TBL	383	
	7	-18.75		1.60	5	9	. 50	00.	, 14.94			AIRW	TRL	364	
		0.0		-6.24	2.1	7 .		10.	8.6			ATRI	TRI	385	
		18.75		8 10	1117			**	2			7014	101	286	
								0					701	000	
280		2000		57.5			. 0.	10.13	1.60			AIKA	121	387	
		104.6		6.36	10.5	, 14	86	.28	6.2			AIKE	181	388	
		DATA	TABILIA/									AIRW	181	369	
	J											AIRM	181	390	
	9	*	• ×	00.0	37.00	06	00.	125.0	250.0		ZIAB .	-14 AIRW	TBL	391	
585													181	392	
		18.75		7.7	-3.1			3.85	7.0			ATP	TRI	303	
					. 4		. 46					7014	101	200	
		300		•	0.00	•	. 07	2.00	1:1			# X 7 4	101	****	
		20.61		•	:	-	4 04	51.	5.7			AIKW	181	395	
		24.6		15.2-	, -1.35	, 2	. 50 ,	3.83	69.6	•		AIKE	Tel	396	
240		194.0		•	6.3	•	. 00	24.	3.2			AIRM	181	397	
	v											AIPW	181	398	
	•		• ×	00.0	37.00	05	00.	125.0	250.0		ZTAB .	-25 AIRW	TBL	399	
	3	Į.											181	400	
	7	18.75		4	~	5		5.46	0			AIRV	TRI	401	
595		0.0		-3.76	3.17		57 .	-1.32	2.34			ATA	TRI	405	
		18.75		1	0		23 .	2 27	1 1			ATOLA	101	703	
		0.75			,				- 4				101	103	
		104.0		200	::		> •		•				101	***	
		10101		:	77	2	-	*0.	•			****	191	505	
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000		-		00.00	31.00	90	000	125.0	250.0		ZIAB .	-44 AIRM	181	404	
	•				,				9			AIRK	TRL	408	
	7	18.75			6.7	1-1	29 .	04.	-2.3			AIRM	181	604	
		J.0		-7.52	-3.84	4- 4		3.06	-0.19	•		AIRM	191	410	
		18.75		77		0 .	20	92.	10.7			AIRM	TAL	411	
609		24.0		•	-2.3	9	20 .	.81	3.5			AIBN	181	412	
		104.0		3.61	2		11	040	1.5			AIEN	TBL	413	
	u											AIRW	181	414	
	•	- ***	ABLE III	P. VZ	AT VSS .	20 K	T AND	S18 .	50 DEG.			AIRW	TRL	415	
		•										AIRW	TEL	416	
610		DATA	TAEIIIR/									AIRM	181	417	
	•											AIRW	TBL	418	
	3		• ×	0.00	37.00	05	00.	125.0	250.0		2148 .	-14 AIRW	TBL	419	
	·											AIRM	181	420	
		-18.75		-7.99	1	0	81 ,	3.09	-0-1			AIRM	146	451	
. 615		0.0		-3.48	, -2.17	1 -5	13 ,	4.28	1.7			MAIN	181	422	
		18.75		-1.60	1 -2.40	-3	31 ,	04.	2.1			AIRM	TRL	423	
		54.0		C. 34	1 -3.24	3	.12 ,	0.13	1 2.37	•		AIRE	TEL	454	
		104.0		-5.56	1-2.26	,	41 ,	220	4.1			AIRN	181	425	
													TRL	426	
95(0		. *	00.00	37.00	00	00.	125.0	250.0		ZTAB .	-25 AIRW	TBL	427	
	J			,								AJRWTRL	TRL	428	
	•	-18.75		-7.08	1	1 -2	. 40	3.62	0			AIRW	TBL	459	
		0.0		-7.44	•	3	•	.25	•	•		AIRE	TBL	430	
		18.75		-0.00	-2-	7	25	2.22	2.			AIRM	TAL	431	
629		24.0		-1.11	-	-1	41 ,	94.	*			AIRM	T81	432	
		104.0		-6.56	ė		. 54	.93					TBL	433	
	•	-					2 14					AIR'	TBL	434	

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5.13.13	435	437	438	430	055	747	443	***	445	447	855	674	450	452	453	454	456	457	428	094	191	204	191	465	100	468	694	470	472	473	475	476	477	478	480	461	482	483	485	486	488	489	
1 87/80/	AIRWTBL	AIRLIBL	PIRNTRE	AIPHTBL	ATOUTE	ATRUTAL	AIRWIGL	AIRWTBL	AIRWTRL	AIRWIBL	AIRWTBL	AJRWTBL	AIRVIE	AIRWTBL	AIRWTEL	ATPUTEL	AIRWTPL	AIRLTBL	AIRVIEL	AIRWTRL	AIRVTBL	AIRVIBL	AJRVTBL	AIRWTBL	ATRUTEL	AIRWIRL	AIRWTBL	AIRWTBL	AIRWTEL	AIRWTRL	AIRWIBL	AIRWTBL	AIRWIBL	AJKWIRL	AIRVIBL	AIRWTEL	AIPUTBL	AIRWIRL	A IRWT81	AIRKTAL	AIRNTAL	AIPVTBL	
21	*B44									A814						AR25						AB44									AB14							48 · -25					
4.6+428	C 2T									17 0			• •			11		3 .				77 0									17 0							17 0			3 .		
2 2	250.	1.9	0.1	, 8.3			30 DFG			250.		6.0	4.4 8.4	, 12.5	1.1	250-		, -0.3	11.2	, 12.0	1.9	250.		2- 1			. 8	50 DFG			250.				5.71	, 111.	3	250.	0	9.5	7.7	, 14.0	
	125.0	-3.6	-0-	, 4.35	5.0	:	ND 515 .			125.0		2.8.	1.52	10.4	15.6	125.0		8 4		8.7	-:	125.0		,-10.5	3.3	3.25	1 9.7	AND STS .			125.0		1 -3.4	1 -0.2	-1.96	6.8		125.0	, -3.6	-3.2		, 10.8	
	00.00	-4.2	2.3	09.0-	1.3	•	35 KT AN			90.00		19.5	28-1-6	4.5	50.6	00-00		,-11.50	3.0	6.1		90.00		-14	: 6	9	•	35 KT A			90.00		10.6	16.1	5.82	3.4		00.06	-5.		4.71		
	37.00	-7.1	.5		. 4		1 VSS .			37.00		-6.9	-4.32	0-	15.0	37.00		-19	0	0.3		37.00		-12.4		•	1.6	- SSA T			37.00		4.5	10.0	-4.43	4.8	,	37.00	-6-3	2.0	-2.64	2.1	
1-140	00.00	~	.5	-4.10		•	1C. VZ A		,	00.0		50	7.73	3.3		00-0		-14.69			-	00.0		00	9	-8.24		ID. VZ A			00 00		4.0	200	-0.10	2.3		0.00	4.7	16.3	-2.44	2.9	
74/74	*						TABLE 11		DATA TABILLE	*												*						TABLE II		DATA TABIIID	*							•					
AIRVTBL	-	-18.75	1.0	18.75	0.401		:			-		-18.75	18.75	54.0	_		•	-16.75	18.75	24.0	_			-18.75	16.75	54.0	104.0	. :			-		-18.75	18.75	54.0	104.0		-		15.75	54.6	164.0	
SUBROUTINE AIRWTBL	U	, ,				•		u			3	•						•														٥	•				٠,						
208		630				618	;			049				649				920				622			099				699			•	029				675			480			

		9 41	, , ,	1	,		=		5	AIRWTBL	267
0.0		-16.61	,-12.92	3.69	, -2.26		66			AIRVIBL	404
18.75		-13.05	-4.3			-	.16			IRMIB	565
24.0		-11.49	7.6		-		.05			IRMIB	964
•		-10.52	\sim	•			.19			AIRWTBL	497
:	TABLE 1116	44	AT VCC -	AS KT AN	313	20 0	2			ATOUTAL	700
		:	?			2				RUTE	200
DATA	A TABILLE									IRVIB	501
										8	205
*	• ×	00.0	37.00	00.06	125.	0 25	0.06	2148	-14	RUT	503
										RWIB	504
-18.75		-31.11			,-12.0		.70			ENT.	505
٥.٥		-7.25	•	Ţ	, -7.0		-			IPNTE	906
18.75		7.48	, -3.06		1.5		.27			B	202
24.0		-7.99	•	•	12.7	1 . 3	~			AIRWTBL	
104.0		18.29	~		, 23.4		2.			AIPVTBL	
										AIRWTBL	
	• ×	0.00	37.00	00.06 . 0	125.0	2	20.0	ZTAB .	25	AIRWTRL	
										AIRWTBL	
-18.75		0	4.7		,-14.		.02			AIRWTBL	
0.0		9.9	-7.0	7.	7.					AIRVIBL	
18.75		-0.62					.70			ATPETRE	
277			-1.							ATOLTOL	
104.0		10.67	7 86	,	3,6		3			ATOCA	
			0000	1007	•	•				ATOUTO	
,	*	00.0	37.00	00.00	125.0	^	20.0	TAR .	77-	ATRETRE	
						,				ATRUTAL	
-18.75			,-16.	18.	,-13.5		.32			AIRVIBL	
0.0			-111-	11.	9-7-	•	. 39			AIRWTBL	
8.75			4.		, 3.7	,	66			AIRVIBL	
24.0			4.	.0	, 4.1	,	.18			AIRWTBL	
104.0		12.07			12.1					ATRUTBL	
						9				AIRWTBL	
:	TABLE IIIF	. 12	AT VSS .	. 45 KT A	NO SIS	3 36 .	DEG.			AIRWTBL	
										ATPUTAL	
DATA	A TABILLE									AIRWTBL	
										AIRWTBL	530
-	*	00.00	37.00	00.00	125.	2 2	90.0	ZTAB .	\$1	LIRWTBL	531
										AIPWTBL	532
-18.75		-24.54	, -1.09		1 -2.2		. 77.0			AIRVIBL	
0.0		-10.45	1.2		1-6-1		.19			ATRETRE	
18.75		-4.25	-5.2		1-4-1					ATRUTRE	
54.0		-0-23	-6-1		3.3		91.			ATDUTAL	
104.0		-12.05	-2.81		. 6.7		. 87			ATOUTO	
•		00	C	00 00	126	36	•		•	TO LA LOCA	220
		•	:	•		•	•		-63	1	239
76		-		•	•	9	9			THE	046
2007		23 00	12.51	1 -3.64	1000		. 60.7			AIRWIBL	156
200		44.77-					11			AIRWIRL	245
1.13		-2.65	9	4	-		.13			AIRLTBL	543
24.0		-3.77	-		0		.51			AJPUTBL	544
0.00		-13.57	7	. 5.	•		.29			AIRWIBL	545
										ATRUTAL	975
*											
		00.0	37.00	00-00	125.	2	90.0	TAR .	77-	A TOLTET	47.7

Course of the last

.13.13 PAGE	549 550 551 552	2 4 B	57 58	660	61	63	65	99	. 89	69	11	7.2	73	75	7.2	28	2 6	81	62	586	882	98	88	69	06	100	93	75	96	26	86	000	25	
13.1																																		
12/08/78	AIRWTRL AIRWTBL AIRWTBL	AIRWTBL AIRWTBL	A IPW TBL	AIRWTBL AIRWTBL	AIRWTBL	AIPUTBL	AIKWTBL	AIRWTBL	AIRWTBL	AIRWTBL	AIPWTBL	AIPUTAL	AIRWTBL	AJRWTBL	AIRWIEL	AIRWTRL	ATPUTAL	AIRLTBL	AIRWTRL	AIFUTBL	AIPWTRL	AIRWT8L	AIRWIBL	AIRWTAL	AIRWIBL	AIREIGE	AIRWTBL			AIRWTBL	AIRWIBL	AIKEIBL	AIRVTBL	
7				-14				-25						-44									-						-52					
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S - 35 KT AND STS - 30 DFG. ATKWTBL	AIRWIAL	JPWTBL Tevin	IPVTBL	24 , 6.89 , 6.89	6.89 c 7.69 c AIRWIRL	9.74 , 5.91 , AIRWIBL	.14 , 4.88 , AIRWIBL	25.0 250.0 21AB25 AIFWIBL	AIRWTBL	P. 94 . AIRWIBL	10.03 , AIPWTBL	4.58 P AIRWIRL	AIPWIBL	IRVTBL	2.68 . AIPWIBL	AIRVIBL	43 . ATRUTAL	AIRWTBL	VT8L	IPVT8L	NT9L	AIRVTBL	IRVIBL	NTBL	IRWTBL	AIREIR	IFWTRL	AIRWTBL	AIRVIBL	AIRWIRL	AIRVIBL	IPUTAL	IRWTBL	TOLTRI	NTBL.	VIBL.	LTR!
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IF (F. EG. C) GL 10 140	11 (10.20.20.40.50.1)		ALPLT
	24105404405		CALPLT
:	READ AND PRODUCE A CENTERED PLOT TITLE.		ALPLT
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NC . 80		•	ALPLT
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	0.5+LNGTHX - 4.0		ALPLT
10 110	0.11		11414
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C *** READ X-A	READ X-AXIS LABEL.		71014
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20 RFADINLIST, 1010) LABELX	010) LABELX		CALPLT
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CCPPON UDO	UDDIT, WDDIT, CDDIT, TCDIT, XAPPDDIT, ZAFFDUIT, DFRPMC, XSPDCIT, P ZSFOCI, TSPDOIT, VDDIT, PBDOIT, R8DDIT, YAPPDGIT, PHICCI, PSIDDIT, YSPDOIT
*** R ARPA	RPAY SEGMENT 3 - STATE VARIABLES.
CCMMON US,	UB, WR, OB, THETA, XAPP, ZAFP, DFRPM, XSP, ZSP, THETAS, PV VB, PE, RB, YAPP, PHI, PSI, YSP
*** R ARRA	ARRAY SEGMENT 4 - REF. VALUES FUR LOCAL LINEARIZATION.
CCFFON UOS	UO, WO, CO, THE TAO, XAPPO, ZAPPO, XO, PO, UPASO, WBESO, WASDO, R THETABC, PSIAO, PHIAO, RCDO, VO, PO, PO, YAPPC, PHIO, PSIO, YOLO, R NC, VPASO MO, LOSNO
*** R ARRA	ARRAY SEGMENT 5 - INPUT FORCES AND MOMENTS.
COMMON SUM	SUMFXO, SUMFZO, SUMMO, SUMFX, DFX, SUMFZ, DFZ, SUMM, DM, SUMFYO, SUMPLO, SUMMO, SUMFY, DFY, SUMPL, DL, SUMP, DN
*** R AKRA	ARRAY SFGMENT 6 - GEOPETRY.
COMMON WEI	WEIGHT, G. IV, IV, IZ, IXZ, LM, WM, LTCM, LS, LTDS G. IX, IV, IZ, IXZ, LM, LTDM, LS, LTCS
*** R ARRA	ARRAY SIGMENT 7 - CONSTANTS.
CCMPON 1 2 3 0 9 FAI KEI	COMEGAL, CHEGAL, KU, KW, KFRPM, KCCN, TAUENG, TAUCON, TAUD, KDEU, KDEW, KDEW, KDET, KDET, KDEZ, KDEN, KDEDE, KDEDT, KDTU, FDTW, KDTO, FDTT, KDTX, KDTZ, KDTN, KDTDE, KDTDT, RDTW, KYV, TAUDA, KT, KZ, KY, B1, BZ, TL1, TL2 RDTM, KTOPM, KTOM,
	ET, KOEX, KOEZ, KOEN, KOEDE, KOEDT, TT, KOTX, KOTZ, KOTN, KOTOF, KOTOT,
*** R ARRAY	SEGMENT R - WIND, ALTITUDE, AIRSPEED AND AIRWAKE.
COPPON	ALT, VAIR, UPAS, VBAS, WBAS, ALPHA, BETA, DUMI, DUMZ, VS, PSIS, XIDWS, RYIDWS, VAMB, PSIAMP, XIDWA, YIDWA, YIDWA, VWDD, PSILOD, PSIADPSISP, RPSIS, DX45, DX45, DX45, XM, YM, ZM, PSIA, IHETAA, PHIA, SIGMAVX, SIGMAVX, VXAW, VYAW, VZAW, UWINC, UMFAN, UK, UAN, VWIND, R

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N 4.6+428 12/08/78	DYM245,265P,		VAIRC,		FRPM, ZCON, ZPOIGV, NR,		ETHETA,		0R1C, 0R2D	BLE LOOKUPS.	CPEN LOOP COMMAND TABLE L			NDR		S, WNTS, S, WNPS, TAUPRT	TABLES.		
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COPPON	TZU(6) TZV(6) TZC(6)	ac ac ac ac
COMMON	72CDN(6) 72PICV(6) 72DE(6) 7PU(6)	***
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Principle of the Parket

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DESCRIBING FUNCTION CALCULATION

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- TAPLE(J+1) + PIAS - TABLE(J+1) - BIAS

DC 70 I-1,K

20

IF(XXZ .LT. 0.0) PII - 0.0 IF(XXZ .LT. 0.0) PIZ - C.C IF(SIGMA .EC. 0.0) GD TD 65

- XX1/SIGPA - XX2/SIGPA

INDEX(M) + INDEX(M+1)

.0*xx1 - SG

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DESCRIP

DESCRIB

				U -
SUBRC	SUBROUTINE DESCRIP 74/74 0PT-1	12/08/78	15.13.13	PAGE
	PII - C.5*(1.0 + FPF(0.7C7)0675*XXIII	DF SCR IR	46	
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02	SF - XX1 - 3F	DESCRIB	66	
	IFIBIAS.NE.O.O) BE - RE - Z.O*XXZ*TARLF(J+1)/PLAS + XXZ*SIGMA*(DESCRIB		
	Š	DESCRIP		
25	DDD COMPONENT CALCULATIONS.	DESCRIB	2.2	
	XXI - TABLE(II+I) + PATIG+(TABLE(II+2+K+I) - TARLE(II+I)) XX2 - SG - KKI	DESCE 18 DESCR 18		
•	E.0.01 80	DESCRIB		
08	70 CCN11NUE - RD + XX2+(P11 + P12)	DESCRIB DESCRIB		
	C *********** CALCULATE BUTPUT MEAN AND VARIANCE ************			
		DESCRIB	0.5	
2		DESCRIP		
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00		DESCRIB		

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C	-	SURRDUTINE ELLIPSE(XP, YP, DXP, CYF, DXYP, ANGLE, STARTY, CELX, STARTY,		LIPSE	~
Nouth 10 pice am		DELY, SCAL YX, SCAL YY	;	LLIPSE	m .
Nouth to place an elifes on a caccep plot.			: •	LIPSE	• •
C	•			LIPSE	•
C			•	LIFSE	1
C		INPUT APGUMENTS	•	LLIPSE	80
C		dx	•	LLIPSE	0
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CONTRACTOR OF THIPPER AND THE PROPERTY OF THE	10	×c	•	LLIPSE	=
December Control of Y Control		DXP	• (x	LLIPSE	12
C		DYP		LLIPSE	13
C		DXYP	•	LLIPSE	14
C		٥٨.	•	LLIPSE	15
C	15	ANGLE	•	LLIPSE	16
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C		* DELY	+ EL	LLIPSE	20
C. SCALYY SCALE FACTOR FOR Y ELLIPTICAL AYIS C. CALCULATE AAGLE OF FOTATION C. CALCULATION C. CALCULATE AAGLE OF FOTATION C. CALCULATE AAGLE OF FOTATION C. CALCULATE AAGLE OF FOTATION C. CALCULATE O	20	. SCALXX SCALE FACTOR FGR X FLLIPTICAL AXI	13 •	LIIPSE	2.1
C. C		SCALYY SCALE FACTOR FOR Y ELLIPTICAL AXI	• E.	LLIPSE	22
C C C C C C C C C C C C C C C C C C C			•	ILIPSE	23
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DYP2		•		LIPSE	30
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SINCA SINCA SINCACA SINCA SINC	04	CHATINOE		LIPSE	;
COSAZ - COSTANGINEZ - A124SINAZ + A224SINAZ B11 - A114COSAZ + A124SINAZ + A224COSAZ B11 - A114COSAZ + A124SINAZ + A224COSAZ B11 - A114SINAZ - A124SINZA + A224COSAZ ELLIPSE B12 - A114SINAZ - A124SINZA + A224COSAZ ELLIPSE B12 - SORT(1.3663/82) + SCALXX CALXX CAXX CA		• •	1	LLIPSE	25
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DX = SORT(1.3863/811)	57	•		1100	4
07 - SORT(1.3663/822) + SCALYY x	0.0	•	ī	ITPSE	47
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CALL ROTATE(X,Y,AMGLE,-1,XR,YR) ANG ANG FLIPSE ANG				LIPSE	64
CALL ROTATE(X,Y,AMGLE,-1,XR,YP) ANG			13	LLIPSE	20
ANG * ANG * 57.2957E X * X X X X X X X X X X X X X X X X X	90	ROT	13	LLIPSE	51
X = XF Y = YR CALL ROTATE(X,Y,ANG,O,XR,YR) ELLIPSE FILIPSE ANG = ANG + ANGLE CALL ROTATE(X,P,ANG,O,XR,YR)			F	LLIPSE	52
CALL ROTATE(x, Y, ANG, O, XR, YR) ELLIPSE ANG - ANGLE CALL ROTATE(X, Y, ANG, O, XR, YR)		***	14	LLIPSE	53
CALL ROTATE(X, Y, ANG, O, XR, YR) ELLIPSE ANG + ANGLE C. FLLIPSE C. FLLIPSE		æ -	13	LLIPSE	24
SCHIIPSE CHIIPSE CHIIP	,	CALL ROTATE(X, Y, ANG, O, XR, YR)	=	LLIPSE	25
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SUBROUTINE ELLIPSE 74/74 OPT-1

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FTK 4.6+428

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	61 10 70		444	66
			E6F	09
09			ERF	61
	C *** EVALUATE FRF FOR 0.4770 .LE. ABSCAN .LE. 4.0.		LR.F.	62
			FRF	63
	FFF . P1(7)*x + P1(8)		ERF	49
	Dilp . X + 01(7)		ERF	69
65	DC 30 I•1,6		ERF	99
	FRF = ERF*X + P1(1)		ERF	67
			EPF	89
	30 CONTINUE		ERF	69
	xpxSo		EPF	20
20	IF(XP .LT. XPAIN) XP . XPAIN		ERF	71
	ERF . SIGN+(1.0 - ERF+EXP(XP)/DUM)		EPF	72
	65 TD 70		ERF	73
	40 IF(X,GT,XLARGE) GO TO 60		FRF	14
	• •		FRF	75
75	C *** EVALUATE ERF FOR 4.0 .LT. APSIXX) .LF. 5.6875.	THE PERSON NAMED IN	ERF	92
			ERF	11
	x50 - 1.0/x50		FRF	18
	ERF - P2(4)*XSQ + P2(5)		ERF	42
	DUM - XSO + 02(4)		ERF	80
80	00 50 I-1,3		ERF	81
	EPF - FRF+XSO + P2(I)		EFF	82
	DUM - DUP*XSC + 02(I)		ERF	83
	50 CUNTINUE		ERF	84
	xp1.0/xS0		ERF	6.5
. 58	IF(XP .LT. XPMIN) YP . XPMIN		EFF	86
	ERF - SIGN+(1.0 - EXP(XP)+((SSOPI + XSO+ERF/DUM)/X))	(0)	ERF.	87
	60 10 70		EPF	88
			FRF	68
	C *** EVALLATE ERF FOR ABS(XX) .GT. 5.6875.		ERF	06
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			FRF	92
	70 RETURN		ERF	93
	FNO		ERF	*6

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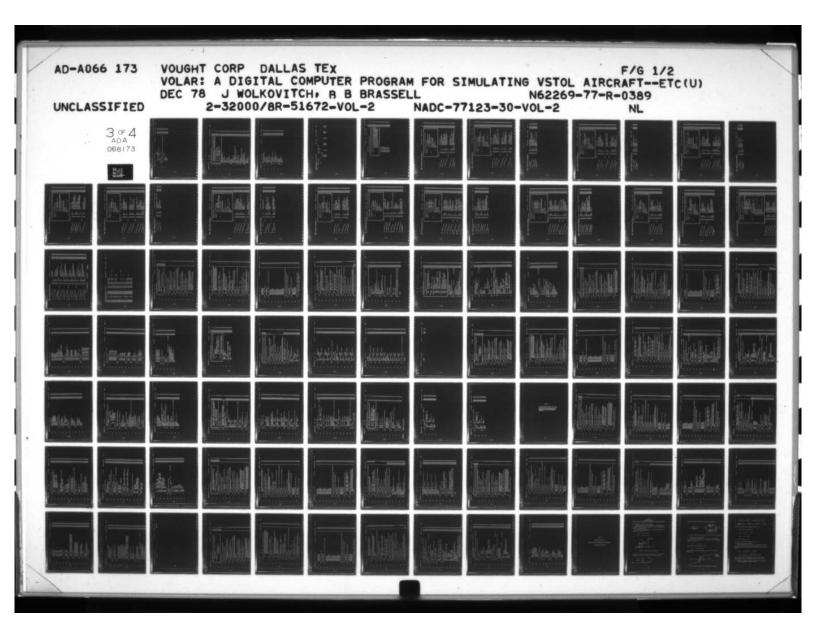
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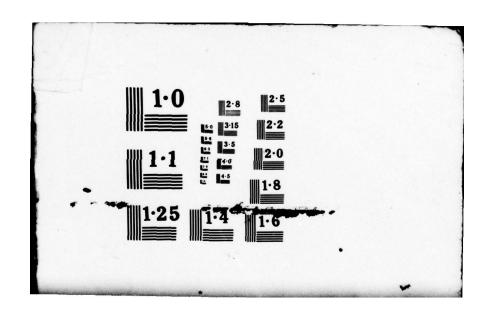
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SUBREUTINE KUTTA

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0		CULINE MATINY (IHP,N,DIT,NCIP) ************************************	MATRIX TO BE INVER NUMBER OF ROWS IN SINGULAR FLAG. DET = 0. SINGULAR POW DIPENSION OF T INVERTED MATRIX.	01h, 1) 4), ICOL (34)			F11E		MENTS IN CO	
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9			VATIAN	61	
	1*AY-1C0L(1)-N		ANTITA	62	
	DG 700 J-1,N		WATTAN	63	
	N+7-XX		WATINY	99	
	700 A(1MAX,NK)-A(1,1)		MATINY	69	
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	X+=7+X		PATINY	70	
20	75		PATINV	11	
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	848 NTFPP=ICOL(I)		PATINV	74	
			VALLAY	75	
75			PATIN	92	
		849,850	MATINV	11	
	849 ICOL(1) - ICOL(3)		VALTAM	78	
			PATINY	79	
	DET05T		NATIAN	08	
80			WATINY	61	
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	950 OF 256 I-1,N		WATINY	*8	
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COMPENT	MISCELLANEGUS	COMPENT MISCELLANEGUS MATRIX OPERATIONS.
••••••	***************************************	***************************************
ROUTINE	TO PERFORM ALL	ROUTINE TO PERFORM ALL REQUIRED MATRIX OPERATIONS IN THE STACK
NOTES :	1) AN CUIPUT	NOTES : 1) AN CUIPUT MATPIX CANNOT BE EQUIVALENT TO AN INPUT. WAIRIX IN ANY POUTINE WHICH INVOLVES MULTIPLICATION
	2) THESE POUT	OF TWO MATRICIES, IT IS ALLONED IN ALL OTHER ROUTIN
		DIMENSIONED N BY N. DVER DIMENSIONED IS ALLOWED IN
	AS A(J+(N-1)+1).	EQUIVALENT OF A(1,1) PAY BE ADDRESSED

MATRIX

MATRIX

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		::	ROUTIN	ROUTINE TO MULTIPLY AN N	7	N MATRIX BY A CONSTANT.	::
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		::			IN - NUMBER OF ROWS IN	IN MATRIX.	: :
		::	METE	Tans .	SOUTH FOLLY ENT POLITINE		::
		:					:
		:		SUBR	SUBROUTINE MULTNR (A,R,B,N)	(2)	:
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6110000001			Sel	-	RFG 81		
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2 53210			SAZ	7	GET CENTENTS OF +R+		
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53310				X			
42333	33		IX3	x3+x3	COMPUTE NUMBER OF ELEMENTS	FLEMENTS IN +8+	
	63433		SR4	R3+X3	SET PEG 84 TO LWA+1 OF		
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20170			NY 3	22	NORMALITE SI SHENT		
66221	2.1		CR2	R2+R1	CEMPITE NEXT ELEMENT ADDRESS IN	NT ADDRESS IN *A*	
	40623		F X 6	X2*X3	MULTIPLY BY +R+		
•			SA6	83	STORE IN NEXT ELEMENT OF +8+	ENT OF +8+	
66331			583	83+81		NT ADDRESS IN *B	•
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+ 00000000000			9	FULTER	RETURN		

NOTE

ARGUMENTS

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10 6110000001		581	1	SET REG 81 TO 1	MATRIX
54211		SA2	A1+81	SET PEG X2 TO FWA OF +8+	MATRIX
54321		SA3	A2+81	SET PEG X3 TO FWA OF +C+	MATRIX
63230		SAS	x3	MEVE FWA UF +C+ TO REG B2	MATRIX
54331		SA3	A3+81	SET REG X3 TO ADDRESS OF +N+	MATRIX
53330		SA3	x3	GET CONTENTS OF +N+	MATRIX
43000		OXW	0	CLEAP REG XO	MATRIX
42433		1×4	X3+K3	CALCULATE NUMBER OF ELEMENTS IN MATRIX	MATRIX
43700		FX7	0	CLEAR REG X7	MATRIX
63342		583	82+X4	SET REG 83 TO LWA+1 OF +C+	MATRIX
					FATRIX
	1000.2	955	0		PATRIX
13 42437		1 1 4	x3.4x7	CALCILLATE NACI-11	WATOTY
43600		WX6		CLEAR REG Xe	PATRIX
36442		1×4	X4+X2	CALCULATE ADDRESS OF +8(1, J)+	MATRIX
00094		J.		*C-0*	MATRIX
14 63440		SA4	5×	STORE ADDRESS IN REG 84	MATRIX
36401		1×4	x0+x1	CALCULATE ACORESS OF *A(I, 1)*	MATRIX
63534		585	84+X3	SET REG 85 TO ADDRESS OF *8(N. J) *	MATRIX
09969		SP6	, 5x	STORE ADDRESS IN REG 86	MATRIX
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	100P.3	RSS	0		MATRIX
14 54440		745	38	The standard to	MATRIX
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14499		*	18+48	GFT NEXT FLEMENT ADDRESS OF +8+	MATRIX
			Crabi	CLAPUTE A(1,0K)+B(K,0J)	MATRIX
16 63636		286	R6+X3	GET NEXT ELEMENT ADDRESS OF *A.	MATRIX

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A PERSONAL PROPERTY.

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•	142	143	144	145	146	147	148	149	150	151	152	153
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COMPASS	SUP INTO	NCRP4L12	CP.3 CCATINUE	STOPE SE	GET NEXT	INCREMEN	7			INCREMENT +J+	CP.2 CONTINUE	RETURN
	*****	7.6	R4,8851	8.2	P2+81	X0+81	x0-x3	x5, LCOF.2	•	x7+81	82,83,16	MUL THN
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SA3 A2+81 SET REG X3 TO FWA OF +C+ SA3 X3 SET REG X3 TO FWA SA3 X3 SET REG X3 TO FWA SA3 X3 SET REG X3 TO WA SA4 X3 SET REG X3 TO WA SA5 B0 CLEAR REG B5 CLEAR REG B5 CLEAR REG B5 CLEAR REG B6 MATRIX	54211		242	1+81	SET REG X2 TO FWA OF +R+	4	TRIX	184
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\$43 43+81 \$5ET REG X3 TO ADDRESS OF *N* \$43	230		\$82		PCVE FWA OF #C+ TO REG 82	Y.	TRIX	186
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LOCP.5 BSS 0 LOAD +A(I,K)+ SA4 X0 LOAD +A(I,K)+ SA5 X7 LOAD +B(J,K)+ IXO X0+X3 CALCULATE NEXT +A+ ADDRESS FATRIX FX4 Y4*5 CALCULATE NEXT +A+ ADDRESS MATRIX IXT Y7+X3 CALCULATE NEXT +B+ ADDRESS MATRIX FX6 86+81 IXT X7+X3 CALCULATE NEXT +B+ ADDRESS MATRIX FX6 X6+X4 SUF KESULT NX6 X6 NXFMALIZE RESULT HATRIX MATRIX	66600		586			4	TRIX	108
LOCP.5 BSS 0 LOAD +A(I,K)+ SA4 X0 LOAD +A(I,K)+ SA5 X7 LOAD +A(I,K)+ IXO X0+X3 CALCULATE NEXT +A+ ADDRESS FX4 Y4-X5 CALCULATE A(I,K)+B(I,K) RATRIX RATRIX SR6 B6+B1 INCREMENT K RATRIX FX6 X6+X4 SUPPLIE RESULT NX6 X6 NAMELIZE RESULT LT P6,B3,LCOP.5 LOOP UNTIL K **N* MATRIX M						W	TETX	100
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\$4 X0						4.4	TRIX	201
SA5 X7 LCAC +8(J,K) + IXO XO+X3 CALCULATE NEXT 4A4 ADDRESS MATRIX FX4 Y4-X5 CCMPUTE A(I,K)+8(J,K) SR6 E6-81 INCREMENT A IX7 X7-X3 CALCULATE NEXT +8+ ADDRESS PATRIX FX6 X6+X4 SUPPRISE PESULT NX6 X6 IT P6,93,1COP,5 LOOP UNTIL K ** +N+ NATRIX SA6 E2 STERE SUPPRITED INTO +C(I,J)+ HATRIX HATRIX	034		SA4		LOAD +A(I,K)+	7	TRIX	202
IXO XO+X3 CALCULATE NFXT \$4\$ ADDRESS PATRIX FX4 X4*Y5 CCMPUTE A(I,K)*B(J,K) SR6 E6+81 INCREMENT K IX7 X7*X3 CALCULATE NEXT *B* ADDRESS PATRIX FX6 X6+X4 SUP RESULT NX6 X6 NCPMALIZE PESULT IT P6,93;[COP,5 LOOP UNTIL K ** *N* MATRIX SA6 E2 STERE SUPMATION INTO *C(I,J)* MATRIX	53570		SAS		LCAC *8(J,K)*	AH	TRIX	203
FX4 X4*Y5 CCMPUTE A(I,K)*B(I,K) SR6 86+B1 INCREMENT K IX7 X7*X3 CALCLATE NEXT *B* ADDRESS PATRIX FX6 X6+X4 SUF KESULT NX6 X6 NCPMALIZE PESULT LT P6,93,[COP.5 LOOP UNTIL K ** *N* MATRIX SA6 62 STERE SUPMATION INTO *C(I,J)* MATRIX	36003		0 × 1		CALCULATE NEXT *A* ADDRESS	A.	ITRIX	504
SRG BG+81 INCREMENT K IX7 X7+X3 CALCULATE NEXT +84 ADDRESS PATRIX FX6 X6+X4 SUF KESULT NX6 X6 NCFMALIZE RESULT LT P6,83,[COP.5 LOOP UNTIL K **N** SAG BZ STORE SUPMATION INTO +C(I,J)** MATRIX MATRIX	57507		F×4		COMPLITE ALL, KI +B(J,K)	4	TRIX	502
1X7 X7+X3 CALCULATE NEXT +8+ ADDRESS PATRIX FX6 X6+X4 SUP KESULT NX6 X6 NCPMALIZE RESULT LT P6,83,1COP,5 LOOP UNTIL K = +N+ SA6 B2 STORE SUPMATION INTO +C(1,1)+ MATRIX	661		SR6		INCREMENT K	AM	ITRIX	206
FX6 X6+X4 SUP RESULT NX6 X6 NCPMALIZE RESULT LT P6,83,1COP,5 LOOP UNTIL K # 4N4 SA6 B2 STERE SUPMATION INTO 4C(1,1)+ MATRIX	34773		1×7		CALCULATE NEXT +8+ ADDRESS	Y.A.	ITRIX	207
NX6 X6 NCFMALIZE RESULT LT P6,83,1COP.5 LOOP UNTIL K # 4N4 SA6 62 STERE SUPMATION INTO +C(1,1)+ MATRIX	30664		F 16		SUR RESULT	44	TRIX	206
LT P6,83,1COP.5 LOOP UNTIL K # +N+ SA6 62 STERE SUPMATION INTO +C(1,1)+ MATRIX	24606		9XN		NCPMALIZE RESULT	1	ITRIX	503
SA6 62 STERE SUPMATION INTO +C(1,J)+ MATRIX	£3000030 +		-	6, 83,1 COP.	L'OP UNTIL K . *N*	A.	TRIX	210
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		SP2	18+28	CALCULATE NEXT	ADDRESS OF +C+		MATRIX	277
	00299	587	85.84.1008.6	I CCP UNTIL I .	2.4		MATRIX	279
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CLAPASS 3.3-468.	***************************************	20		TRANNICA.B.N.		N BY N MATRIX.	DESTITANT MATERY	THE PARTY OF THE P	PUMBER OF KUMS	EDUINALENT ROUTINE		TRANKIA, B, N)	12.X)8.1X.X)4	2.	2.	A(1,1)				************************		ENTRY/EXIT POINT		REG B1	REG X2	REG 83 TO ADDRESS OF	CONTEN	REG 82 TO *N*	REG 83 TO +N+ -	AR REG. 84				1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CALCOLATE 14N	***********	F TO BEG XA	3		PEG 87 TO +(1,				DFFSET FOR +(J	CFF SET FOR +(I	*(I fr) v.	*A(1,1)*	E FEG X4 TO X6	** OT *(L,1) **	E PEG X5 TO REG	*8 (1, 1) * TO *A	PERENT ?		NCREPENT I	D CNTIL I - NA
		and agona at the section	356.354.41.01	SEG ! CALL TRAN		N - 1		3	-	 S FURTRAN E		SUBFOUT IN	DIMENSION	10 10 10	1-1 00	10 8(Jel) - A(1,J)	RETURN	END.		*********		ENT		SET	+81	+81			2-81 SET				,	3000	7447					R6 SET						¥1+86 GET			+87		2+R6	5+81	5,82,LCOP.	18+	4. R 3. LUIP. 7
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SA6 X2+82	

A	DEDUINE TG ADD AN P BY P HATRIX TO THE LOVER RICHT HAND CORN OF AN N BY N FATRIX. CALLING SEG : CALL ADDWN (A.B.C.P.P.) ARGUMENTS : A - IN - N BY N MATPRIX. C - DUT - RESULTANT N BY N PATRIX. C - DUT - RESULTANT N BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY N PATRIX. N - IN - N NY BY	DULINE IC ADD AN P BY P HATRIX TO THE LOWER RIGHT HAND CORN CALLING SEC : CALL ADDMH(A,B,C,M,P) ARGUMENTS : A - IN - N BY N NATBIX. C - DUT - RESULTANT N BY N NATBIX. C - DUT - RESULTANT N BY N NATBIX. NOTE : FORTRAN FOLTVALENT ROUTINE SUBROUTIVE ADDNH(A,B,C,N,M) C - DUT - RESULTANT N BY N NATBIX. NOTE : FORTRAN FOLTVALENT ROUTINE SUBROUTIVE ADDNH(A,B,C,N,M) C - DUT - RESULTANT N BY N NATBIX. NOTE : FORTRAN FOLTVALENT ROUTINE SUBROUTIVE ADDNH(A,B,C,N,M) C - DUT - RESULTANT N BY N NATBIX. I - IN - NUMBER OF RUANN C - DUT - RESULTANT END - A - IN - N BY N NATBIX. SET REG 83 IC FA DF - RES SET REG 84 IC IN REG 86 C - LEAR - IN REG 86 C - LEAR - IN REG 86 SES SET REG 84 IN REG 86 C - LEAR - IN REG 86 C - LOW - IN REG 86 C
	RDUIINE TG AP OF AN M BY A A ARGUMENTS 8 10 10 10 10 10 10 10 10 10 10 10 10 10	ABGUMENTS : CALLING SEO : ARGUMENTS : ARG

ADONA	MATRIX - MISCELLAMEGUS MATRIX (PEPATIONS. ADDNM - ADD M RY M MATRIX TO N BY N MATRIX.	CPEPATIONS N BY N MAT	PIX.		CCMPASS 3.3-428. 12/08/78	12/08/78 15.15.17.	PAGE	2
	53420		545	12	GET NEXT ELEMENT OF +B+		HATRIX	461
	73221		SX2	X2+R1	INCREMENT INDEX INTO +8+		MATRIX	462
							MATRIX	463
104		JAP.1	855	0			MATRIX	494
							MATRIX	465
104	104 66441		584	P4+81	INCREMENT +I+		MATRIX	466
	30645		Fx6	X4+X5	COMPUTE +A(1, J) + B(1-N+M, J-N+F)+	+1)*	MATRIX	467
	24606		NX6	46	NORMALIZE PESULT		MATPIX	468
	73111		Sx1	x1+81	GET NEXT ELEMENT ADDRESS IN .A.	**	PATRIX	695
105	105 0747000106 +		-	84,87,JMP.2	JUMP IF +I+ LT +N+		MATRIX	470
	00499		584	80	CLEAP +I+		MATRIX	471
	66551		585	85+81	INCREMENT +1+		MATRIX	472
							MATRIX	473
106		JPP.2	855	0			MATRIX	474
							MATRIX	475
106	106 56620		SA6	8.2	STORE SUM INTO NEXT ELEMENT O	*3* J	PATRIX	476
	66221		582	82+81	GET NEXT ELEMENT ADDRESS IN +C+	•	MATRIX	477
	0723000102 +		11	82,83,LCOP.9	82,83, LCOP.9 LODP UNTIL +C(N,N)+ FCUND		MATRIX	478
107	107 0400000075 +		60	ADDAM	RETURN		MATRIX	410

	- 17 Company							
ADDING TO THE N N PARRICLES. CALLING SEO : CALL ADDINGAPE.C.N.) REGIFFERS A - IN - N RY N MATRIX. C - GUT - RESULTANT NATRIX. C - GUT - RESULTANT NATRIX. NOTE : FCRTEAN FOUTUAGE DE NONS IN N BY N MATRIX. 10 C(1.3) - A(1.3) - A(1.3) + B(1.3) RETION 10 C(1.3) - A(1.3) - A(1.3) - B(1.3) RETION ADDNN BSS 1 ENTRY/EXIT POINT SSS 2 A1+R1 SET REG B1 TO TO REG B2 SSS 3 A1+R1 SET REG B1 TO TO REG B2 SSS 3 A1+R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 A1-R1 SET REG B1 TO LAN OF 98- SSS 3 SSS 3 SST REG B1 MEXT ELEFENT ADDRESS IN 88- SSS 3 SSS 3 SST REG B1 MEXT ELEFENT ADDRESS OF 98- SSS 3 S	The sale and the sale of the s		:	*******				
AGGIPENTS : A - IN - N BY N MATRIX. - GUI - RESULTANT MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N MATRIX. - GUI - LANGER DE ROUS IN N BY N		:	PCUTI	NE TO ADD 1	WE N BY N MATRICIFS.		:	FATRIX
ADDNN BSS 1 ENTRY/EXIT POINT SAZ AZ-B1 SFF EG X3 OF FLEENTS IN SCALE ADDNN BSS 1 ENTRY/EXIT POINT SAZ AZ-B1 SFF EG X3 OF SAG SAZ AZ-B1 SFF		:					•	977
ADDNN BSS 1 ENTRY/EXIT POINT SB1 1 SET REG B1 TO 14 SEP SB2 X3 A3+B1 SET REG B1 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP LDDP.10 BSS 0 SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB3 X3 X3 SET REG B3 TO 14 SEP SB4 X3 SET REG B3 TO 14 SEP SB5 SEP SB5 SEP SB5 SEP SB6 SEP SEG TO 14 SEP SB7 SE		:	CALLI	NG SEO 1 CT	ILL ADDNR (A, P, C, N)		:	
ADDIN BSS 1 SET REG BJ TO 1 SET REG BS 10 S S S S S S S S S S S S S S S S S S		:					•	
ADDN BSS 1 ENTRANT PAIR AND NOTE SUBPLUTINE STATEMENT PAIR NOTE SUBPLUTINE ADDNIALENT POLITINE SUBPLUTINE ADDNIALENT POLITINE SUBPLUTINE SUBPLU		::	ARGIL	-	1			
ADDNN BSS 1 ENTRY/EXIT POINT SA2 A1+R1 SET REG B1 TO FWA FOR SENS IN BY N NATRIX. ADDNN BSS 1 ENTRY/EXIT POINT SA3 A2+B1 SET REG B1 TO FWA OF CC. SA3 A2+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA3 A3+B1 SET REG B1 TO FWA OF CC. SA4 A5-B1 SET REG B1 TO FWA OF CC. SA5 A3+B1 SET REG B1 TO FWA OF CC. SA5 A3+B1 SET REG B1 TO FWA OF CC. SA5 A3+B1 SET REG B1 TO FWA OF CC. SA5 A3+B1 SET REG B1 TO FWA OF CC. SA5 A3 A3+B1 SET REG B1 TO FWA OF CC. SA5 A3+B1 SET REG B1 TO FWA OF CC. SA5 A3 A3+B1 SET REG B1 TO FWA OF CC. SA5 A5-B1 STANDALIZE REWINT ADDRESS IN 68+B1 STA		::			AN WAY AN AN			
ADDNN BSS 1 ENTRY/EXIT POINT Substituting abounta, B, C, N, N, D, 1 N BY N MANKER. Substituting abounta, B, C, N, N, D, 1 N BY N MANKER. Substituting abounta, B, C, N, N, D, C, N, N, D, C, C, N, N, D, C, C, N, N, D, C, N, N, D, C, N, N, D, C, N, D,		::		٠. س	GUT - RESULTANT MATRIX.	:		
ADDIN BSS 1 ENTRY/EXIT POLITINE ADDIN BSS 1 ENTRY/EXIT POLIT SB1 1 SET REG B1 TO 1 REG B2 SA2 A1+R1 SET REG B1 TO REG B2 SA3 A2+B1 SET REG B1 TO REG B2 SA4 A2+B1 SET REG B1 TO REG B2 SA3 A3+B1 GET ADDRESS DF *N* IN3 X3*A CALCULATE NUMBER DF ELEMENTS IN *A* IN X1*X5 GET NEXT ELEMENT ADDRESS IN *A* FX6 X3*A CARPITE *A(1,J) * A(1,J)* NX6 X5 A4 NCPMILIZE RESULT NX6 X5 A7 SA4 B1 SET REG B1 TO REG B0 IN SA4 B1 SET REG B1 TO REG B1 COPPUTE *A(1,J) * A(1,J)* NX6 X6 X7 SA4 X7 SA5 B1 SET REG B1 TO REG B1 COPPUTE *A(1,J) * B(1,J)* ED ADDRESS IN *A* FX6 X3*A CAPPUTE *A(1,J) * B(1,J)* ED ADDRESS IN *BETUPN ED ADDR		::		4	IN - NUMBER OF KOMS IN	5		
ADDNN BSS 1 ENTRY/EXIT POINT SB1 1 SET REG B1 TO 1 SB2 1 SET REG B1 TO 1 SB2 1 SET REG B1 TO 1 SB3 2 A1+R1 SET REG B2 SB3 3 A3+B1 GFT CONTENTS OF NW. SB3 3 A3+B1 GFT NW. SB3 82+X3 SET REG B3 TO LWA+1 OF NG. SB3 82+X3 SET REG B3 TO LWA+1 OF NG. SB3 X1 GFT NEXT ELEMENT OF NW. SA4 X2 GFT NEXT ELEMENT OF NW. SA5 X5 ST NW. SA5 X5 ST NW. SA5 X5 ST NW. SA5 X6 NW. SA6 NW. SA6 NW. SA6 NW. SA6 NW. SA6 NW. SA7 NW. SA7 NW. SA6 NW. SA7 NW. SA6 NW. SA7 NW. SA6 NW. SA7 NW. SA6 NW. SA7 NW. SA7 NW. SA7 NW. SA7 NW. SA6 NW. SA7 NW.		::	2104		SALTING THE SALTING MAGTE			
ADDNN BSS 1 ENTRY/EXIT POINT SB1 1 SET REG B1 TO 1 SB2 A1+R1 SET REG B2 TO FWA DF 68- SB3 A2+B1 SET REG B2 TO FWA DF 68- SB3 A3+B1 GET CONTENTS OF 9- SB3 B2+X3 GET ADDRESS DF 9- SB3 B2-X3 SET REG B3 TO LWA! DF 9- SB3 B2-X3 A3+B1 GET CONTENTS OF 9- SB3 B2-X3 SET REG B3 TO LWA! DF 9- SB3 B2-X3 GET ADDRESS DF 9- SB3 B2-X3 GET ADDRESS DF 9- SB3 B2-X3 GET CONTENTS OF 9- SB3 B2-X3 GET ADDRESS DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB3 B2-X3 GET REG B3 TO LWA! DF 9- SB4 B3 COPPUTE WET ELEMENT ADDRESS DF 9- SB5 B3 F2-B3 F07P 10 COPPUTE RET ELEMENT ADDRESS OF 9-C+ B2-B3 F07P 10 RET ELEMENT ADDRESS OF 9-C+ B3-B3 F07P 10 RET ELEMENT ADDRESS OF 9-C+ B3		::	2100		THE PARTY OF THE P			
ADDNN BSS 1 ENTRY/EXIT POINT SB1 1 SET REG B1 TO 1 1 1 1 N		::		15	PAPELLY TINE ADDING A. B. C. N.			
### 10 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		:			MENSICH ACNON DOBONO CONTRA			
### 10 [1 1 1 1 1 1 1 1 1 1		:		30	10 Jelsk			-
### 10 C(I.J) = A(I.J) + B(I.J) ### ### ### ### ### ### ### ### ### #		:		36	10 1-10K		* 1-187.40	
### FETURN ### ###############################		:			11.3) . A(1,3) + B(1,3)		:	
### END ### ##############################		:		a a	N.		•	PATRIX
### ### ### ### ######################		:		E	•		•	
ADDNN BSS 1 ENTRY/EXIT POINT SB 1 SET REG B 1 TO 1 SA2 A1+R1 SET REG X 2 TO FWA OF +0.0 SA3 A2+B1 SET REG X 3 TO FWA OF +0.0 SA3 A3+B1 GET ADDRESS OF +0.0 SA3 X3 GATCHURTS OF +0.0 SA4 X2 GATCHURT OF +0.0 SA4 X2 GATCHURT ELEMENT OF +0.0 SA5 X2 GATCHURT ELEMENT OF +0.0 SA6 X2 CCMPUTE *4(I, J) + 6(I, J) +		:						
## SET REG B1 TO 1 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$		******	*	******	*******	******		-
\$81 1 5ET REG 81 TO 1 \$82		ADDAN	855	•	ENTRY/EXIT POINT			MATRIX
\$81 1 5ET REG 81 TO 1 \$82					Complete Parket States			MATRIX
SA2 A1+R1 SET PEG X2 TC FWA DF *8* SA3 A2+B1 SET PEG X3 TC FWA DF *6* SA3 A3+B1 GET AD DF *6* IX3 X3*X3 GET CONTENTS OF *N* IX3 X3*X3 CALCULATE NUMBER OF ELEMENTS IN *C* SA5 B1 SET REG B3 TC LWA+1 OF *C* SA5 B1 SET PEG X5 TO 1 LOOP.10 BSS O CAT NEXT ELEMENT OF *4* SA4 X2 GET NEXT ELEMENT OF *4* SA4 X2 GET NEXT ELEMENT OF *4* IX1 X1+X5 GET NEXT ELEMENT OF *4* NX6 X6 X3+X4 CCCPUTE *A[1,3] + B(1,3)* NX6 X6 X6 X6 SA6 B7 STORE IN NEXT ELEMENT OF *C* SA6 B7 STORE IN NEXT ELEMENT	110000001		581		REG 81			MATRIX
SA3 A2+81 SET PEG X3 TG FWA DF +C+ SA3 A3+81 GET ADDRESS OF +N+ SA3 X3 SA3 X3 SA3 X3 SA3 X3 CALCULATE NUMBER DF ELEMENTS IN +C+ SB3 B2+X3 SFT RFG B3 TG LWA+1 DF +C+ SA5 B1 SFT PEG X5 TG 1 LOOP.10 BSS 0 SA4 X2 SA4 X2 SA4 X2 SA4 X2 SA4 X3 SET PEG X5 TG 1 NXC X6 X6 SA4 X2 SA5 SA4 X2 SA5 SA4 X2 SA5 SA4 X2 SA5	54211		SAZ	A1+R1	REG Y2 TC FVA			MATRIX
SR2 X3	54321		SA3	42+81	SET PEG X3 TO FUA OF +C	•		MATRIX
SA3 A3+81 GET ADDRESS OF *N* SA3 X3 X3 X3 X3+X3 GET CONTENTS OF *N* SB3 B2+X3 SET REG B3 TO LWA+1 OF *C* SK5 B1 SET REG B3 TO LWA+1 OF *C* SX5 B1 SET REG K5 TO 1 LOOP.10 BSS 0 GET NEXT ELEMENT OF *A* SA4 X2 GET NEXT ELEMENT OF *B* IN1 X1+X5 GET NEXT ELEMENT OF *B* IX2 X2+X5 GET NEXT ELEMENT ADDRESS IN *A* NX6 X6 X6 X6 CCMPUTE *A*(I,J.) * B*(I,J.)* IX2 X2+X5 GET NEXT ELEMENT ADDRESS OF *C* SA6 B7 STORE IN NEXT ELEMENT OF *C* SA6 B7 STORE IN NEXT ELEMENT OF *C* SA6 B7 STORE IN NEXT ELEMENT OBDRESS OF *C* LT B2-R3. LOOP.10 LGCP UNTIL *C*(I,N.)* FOUND E0 ADDAN	3230		582	×3	MEVE FUA OF +C+ TO REG	82		MATRIX
SA3 X3 CALCULATE NUMBER OF ELEMENTS IN *C** SB3 B2+X3 SET REG B3 TO LWA+1 OF *C** SA5 B1 SET REG B3 TO LWA+1 OF *C** SA5 X2 GET NEXT ELEMENT OF *A** SA4 X2 GET NEXT ELEMENT OF *A** IX1 X1+X5 GET NEXT ELEMENT OF *B** IX1 X1+X5 GET NEXT ELEMENT OF *B** IX2 X2+X5 GET NEXT ELEMENT OF *C** SA6 B7 STORE IN NEXT ELEMENT OF *C** STORE IN NEXT ELEMENT OF *C** SA6 B7 STORE IN NEXT ELEMENT OF *C** STORE IN NEXT ELEMENT OF *C** STORE IN N	54331		SA3	A3+81	GET ADDRESS OF +N+			MATRIX
SAS X34X3 SAS X34X3 SAS X34X3 SET REG 83 TO LWA+1 OF 6C SAS X1 SAS X1 GET NEXT ELEMENT OF 6AP SAS X2 GET NEXT ELEMENT OF 6AP IN1 X1+X5 GET NEXT ELEMENT OF 6AP IN2 X2+X5 GET NEXT ELEMENT OF 6AP SAC X2 NCPPALIZE RESULT NXC X6 NCPPALIZE RESULT SAC 87 STORE IN NEXT ELEMENT OF 6C STORE 10 ST	53330		543	x3				MATRIX
S83 824x3 SET REG 83 TO LWA+1 DF 6Ce Sx5 81 SET PEG x5 TO 1 Sx6 x2 GET NEXT ELEMENT OF 44e Sx4 x2 GET NEXT ELEMENT OF 64e IX1 x1+x5 GET NEXT ELEMENT OF 66e IX2 x3+x4 CCMPUTE 44[x] + 8(1xJ)* NX6 x6 x6 Sx6 87 STORE IN NEXT ELEMENT OF 6Ce	42333		EX I	X34X3		Z	•••	MATRIX
SX5 B1 SET PEG X5 TO 1 LOOP.10 BSS 0 SA3 X1 GET NEXT ELEMENT OF *A* SA4 X2 GET NEXT ELEMENT OF *B* 171 X1+X5 GET NEXT ELEMENT OF *B* 172 X2+X4 CCPPUTE *A*[L] J + B*(I,J)* NX6 X6 X6 X6 X7 STORE IN NEXT ELEMENT ADDRESS IN *B* SA6 B7 STORE IN NEXT ELEMENT OF *C* SA6 B7 STORE IN NEXT ELEMENT OF *C* LT B2.R3.L07P.10 LOCP UNTIL *C(N,N)* FOUND 10 + E0 ADDRN	3332		583	82+X3		• • • •		MATRIX
SA3 X1 GET NEXT ELEMENT OF 44+ SA4 X2 GET NEXT ELEMENT OF 48+ SA4 X2 GET NEXT ELEMENT OF 48+ IN1 X1+X5 GET NEXT ELEMENT OF 48+ IN2 X3+X4 CCPPUTE 4A(I _p J) + 8(I _p J)* NX6 X6 NCPANITZE RESULT IX2 X2+X5 GET NEXT ELEMENT ADDRESS IN 48+ SA6 87 STORE IN NEXT ELEMENT OF 4C+ SA6 87 STORE IN NEXT ELEMENT OF 4C+ LT B2, R3, LOJP, 10 LOCP UNTIL 4C(I _p N)* FOUND 10 + E0 ADDNA	0250		SXS	81	SET PEG X5 TO 1			PATRIX
SA3 X1 GET NEXT ELEMENT OF 44 SA4 X2 GET NEXT ELEMENT OF 88 IX1 X1+X5 GET NEXT ELEMENT ADDRESS IN 4A+ EXCRPTE AGILJ) + 8(I_DJ)* NX6 X6 NCPMAIZE RESULT IX2 X2+X5 GET NEXT ELEMENT ADDRESS IN 88+ STGRE IN NEXT ELEMENT ADDRESS OF 4C+ SA6 87 STGRE IN NEXT ELEMENT ADDRESS OF 4C+ LT 82,83,107P,10 LGCP UNTIL 4C(N,N)* FQUND				,				MATRIX
SA3 X1 GET NEXT ELEMENT OF 44* SA4 X2 GET NEXT ELEMENT OF 88* IX1 X1+X5 GET NEXT ELEMENT ADDRESS IN 4A* KX6 X3+X4 CCMPUTE *A(I_J) + B(I_J)* NX6 X6 NCMALIZE RESULT IX2 X2+X5 GET NEXT ELEMENT ADDRESS IN *B* SA6 B2 STORE IN NEXT ELEMENT OF *C* LT 82*83*103P*10 LGCP UNTIL *C(N_N)* FQUND 10 + E0 ADDNA PETUPN		COOK - 10	622	0				MAIRIX
34	2210		643	;	THE PART OF TARRE			
34 FX6 X3+X5 GET NEXT ELEPTA ADDRESS IN 4A+ NX6 X6 NCPMALIZE RESULT IX2 X2+X5 GET NEXT ELFMENT ADDRESS IN +B+ SA6 87 STORE IN NEXT ELFMENT OF +C+ COMPUTE NEXT ELEMENT OF +C+ LT B2.83, LOJP.10 LOCP UNTIL +C(N,N)+ FOUND 10 + E0 ADDN.	53420		245	12.	NEXT CLEMENT OF			****
34 FX6 X3+X4 CCFPUTE *A(I ₂)) + B(I ₂) +	34116			*1446	בין הכיל בין הרבידה יסיים			
21	36113			X1+12		Z		MATRIX
1 N N N N N N N N N N N N N N N N N N N	30634		0 x 1	x3+x4		•		MATRIX
1X2 X2+X5 GET NEXT ELFMENT ADDRESS IN *B* SA6 87 STORE IN NEXT ELEMENT OF *C* S1 82 82+81 COPPUTE NEXT ELEMENT ADDRESS OF *C* 10 + E0 ADDNN PETUPN PETUPN	4000		NX P	42	NCPMALIZE RESULT			MATRIX
21 SA6 87 STORE IN NEXT ELEMENT OF *C* S82 R2+81 COPPUTE NEXT ELEMENT ADDRESS OF *C* 1	36225		1 x 5	X2+X5	GET NEXT ELFMENT ADDRES			PATRIX
21 S82 82+81 COMPUTE NEXT ELEMENT ADDRESS OF *C* LT 82,83,L03P.10 LOCP UNTIL *C(N,N)* FOUND 10 + E0 ADDNA PETUPN	56620		SA6	82	STORE IN NEXT ELEMENT D	•••		MATRIX
LT 62, R3, LOJP, 10 LOCP UNTIL +C(N,N)+ FOUND + E0 400hh	66221		285	82+81	COMPUTE NEXT ELEMENT	6	•3•	MATRIX
+ EO BOOM PETURA	723000114 +		-	82. R3. LO	.10 LOCP UNTIL .CIN,NI.			PATRIX
	0400000110 +		60	ANDOA	ETUPN			WATER

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	::	7	SEO 1	ALL ADDTREADN)			::	PATRIX
	::	1777.1704		7 70 77			::	MATRIX
	::	-	70		XI x		•	FATRIX
	:		2	IN - NUMBER CF	•		::	
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	:			1000			:	
	:		S	JBF DUTINE ACOTE (A,N)			:	
	:		•	DIMENSION A(N,N)			:	
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	•		10	N. L. I. J. K.			::	
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			11 6	20112121				MATRIX
•	:		•	TURN			•	MATPIX
			•	FND			:	MATRIX
						200		PATRIX
	ADDIE	B C C	-	:	*******			MATRIX
5021000001		SAZ	A1+1		OF +N+			MATRIX
53220		SAZ	xz	TENTS OF *N	-			MATRIX
		281	x 2	***				MATRIX
121 6120000001		582	1+041	85				MATRIX
66400		S 8 4	0.00	INNER LOOP COUNTER				MATRIX
6252777776		585	x2-1	SET 85 TO +N-1+				MATRIX
00999		286	90					MATRIX
		587	080	• • • • • • • • • • • • • • • • • • • •				FATRIX
123 44443	100F-12	228	86+83	TALLACTINE LOOP COUNT	,			KATATA
66760		587	86	I I I				MATRIX
66430		284	33	NER LOOP STARTS	AT VALUE OF	OUTED	1000	FATRIX
	LOOP . 11	BSS		•		-		MATRIX
124 53316		SA3	x1+86	GET A(I)				MATRIX
53417		SA4	x1+87	GET A(J)				MATRIX
30634		FX6	X3+X4	ADD A(I) TO A(J)				MATRIX
54606		9XN		NURMALIZE X6				MATRIX
125 10766		Px7	9x	CUEY X6 INTO X7				MATRIX
54630		SA6	h 3	STORE A(1)				PATRIX
4740		SA7	51	STORF A(J)				MATRIX
		586	86+82	1 • 1 • 1				MATRIX
126 66771		280	18/18	2 + 7 = 7				FATRIX
4 4610001440		* 0.	201-19-78	DIT END OF THE CO.	IN COON			TAIR I
127 46112		583	83482	•	TAILOR OF			XIXIVE
		1 2	83.P1.LOD	-	14007 10			******
130 0400000117 +		. 0	DOTE	:				MATOTA
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15.15.17.																•																			
12/08/78		3		NS IN A		NS IN B				H1, H2,C)				(K, J)					IN INTO X4	TO X2	TC X3		X2			4	***			INTE	1 10 86	INTO	INTO	INTO X5	
-428.	PATRICIES	BANISHES	N NZ PATRIX	OF COLUM	H2 HATRIX	OF CCLUM	M2 MATRIX	T KOUTINE		10 N 1 9 N 2 9 B 9 F				ACI,KI+B(K,			2	N 2	9 1 1	JE N.1	JF N2		F M2 IN	JF M2 1		ENT END	ENT FOR			1,1	5 OF 8(1,)		S OF BIKAJ	TS OF ACLIFE	
MPASS 3	1 48 2 03	TIAPNIPHE	7	- NUMBER	=	NON	7	FOUTVALEN		N ACNIENZ	1, N1	Je 1, M2	1. N.2	+ ((1))		TRY/EXIT	DOPEC	DRESS	DORFSS	INTENT	INTE	12 1	OPE	NIE	2 1	1 1 1 1	2		7 5	LOOR	PDD	LDDR	CONTEN	CONTEN	14.7
·	LI TIPLY TW	CALL MUL	٠.	N1 - IN	•	2	•	FOR TRAN		SUBRCUTI	00 10 I	00 10	DD 10 K	(71)	ENO	EN		20	PUT AC	2	רטיי	Į.	2.5	200	2	200	100		S.F.	PUT	UH	04	PU	TUA	110
	INE 19 P	ING SEC:	GUMENTS .					•						10		-	1 A 1 + R	A2+B		XS	~ ~		•	x2 x2	~ (٠.	E C	×		× C	· &	× ×	•
	knu T	CALL	ARGU					NOTE								858	581	SA3	SAS	SA2	SA3	\$83	SA2	SAZ	584	287	SBS	858	NA.	1x7	586	2XX	SAS	SAS	2 4 5
ATION		:::	:::	::	::	::	::	::	:	::	:	::	: :	::	::	FULT												100P.A				8 - 8UU I			
																-		54321			53330		64.331	1361		00299					63670				
NEGUS M																	54211	•	-	3220	•	63330	54251	•	63420	9			90	16747	•			2	40882
MATPIX - MISCELLANEGUS MATRIX MULI - MULIIPLY TWO MATRICIES																	6110000001		54431		61220	633		53220	634		96500	*****	43600			73710	56260	53570	
-																	1																		

MATRIX MULT -	MATRIX - MISCELLANFOUS MATRIX OPERATIONS. MULT - PULTIPLY INC MATPICIES			COMPASS 3.3-428.	28. 12/08/78 15.15.17.	15.15.17.	PAGE	2
	24606	NXA		NOPRALIZE X6			MATRIX	641
	67331	593	83-81	DECREMENT NZ			PATRIX	642
143	143 0703000141 +	19	83,8C,1 COP. P	-			MATRIX	643
	53635	SA6	X3+85	STORE C(1, J)			MATRIX	559
	66552	585	P5+B2	GET NEXT ELFPENT OF +C+	NT OF +C+		MATRIX	649
144	144 5021000002	SAZ	A1+2	PUT ADDRESS OF	PUT ADDRESS OF NZ INTO XZ AGAIN		MATRIX	949
	53220	242	x2	PLT CONTENTS OF M2 X2 AGAIN	F M2 X2 AGAIN		PATRIX	647
	63320	5 P 3	7.2	MUVE NZ INTO R3 AGAIN	3 AGAIN		MATRIX	949
145	145 66773	587	P7+B3	INCREMENT FOR	INCREMENT FOR NEXT COLUMN OF +B+		PATRIX	649
	57441	SP4	84-81	DECREMENT M2			PATRIX	650
	0704000137 +	19	84.9C.100P.				MATRIX	651
146	146 5021000005	SA2	A1+5	PUT ADDRESS OF M2 INTO X2	M2 INTO X2		MATRIX	652
	53220	SAZ	x2	PUT CENTENTS OF M2 INTE X2	F M2 INTC X2		PATRIX	653
	63420	204	x2	PUT M2 PACK INTO 84 AGAIN	TO 84 AGAIN		MATRIX	654
147	147 7200777776	SXO	x0-1	DECREMENT NI			MATRIX	659
	73111	Sx1	x1+81	INCREMENT FOR	WEXT ROW OF *A*		PATRIX	959
	73331	Sx3	x3+81	INCREMENT FOR NEXT ROW OF	NEXT ROW OF +C+		PATRIX	657
150	150 66500	SAS	08	RESET COLUMN I	÷	O ZERO	PATRIX	658
	66700	587	80	RESET COLUMN I	NCREMENT FOR +8+	TO 25R0	MATRIX	629
	0310000137 +	7 N	XO.LOUP.A				MATRIX	099
151	151 0400000131 +	60	MULT	RETURK			MATRIX	199

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Total I

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ULTABL	MULTART - MULTIPLY & PATRIX BY	DPERATIONS.	OSE OF	ANUTHER			.II.	51
			ROUT!	INE TO PULTE	POSSESSESSESSESSESSESSESSESSESSESSESSESSE	TRANSPOSE OF	*** PATRIX AN ** PATRIX ** PATRIX	666 665 665
		::	CALLING	NG SEOF	CALL MULTAPT (A.N.). NZ.B. MI. MZ.C	(34)		
		:::	APGUMENTS	FNTS .	NI -			
	,	:::			NI - IN - NUMBER OF COLUMNS	17.8		
		::			- 1 X			
		::			2 - IN - 00T		** MATRIX	
		::	MOTE	•	FORTRAN EQUIVALENT ROUTINE			
		::						
		::			DIMENSION A(NISNS) BR(MISHS)	2) 6 C (N 1 9 M 1)	** PATRIX	
		::				•		
		:			. 0.0 . (1,1)			
		::			DO 10 K-1942		** PATPIX	
		:		•	RETURN			
		::			END		** FATRIX	
			*****	*******		***************	**** MATRIX	
153	6110000001	4	85.5 SB1		TRY/E		PATRIX	
	54211		SAZ	+	IDPESS OF NI	x2	PATRIX	
184			SA3	+ 8	DRESS OF NZ	,	MATRIX	
121	5454		SAS	A4+81	PUT ADDRESS OF MILLAIN INTO	X5	MATRIX	
	53220		542	~	INTO X2		PATRIX	
155	53350		582	. x x	TAL		PATRIX	
	63330		Sea		INTC 83		PATRIX	
	54351		543	A5+81	DRESS		PATRIX	
156	53330		SA3	9 4	INTO X3	CX DINI	MATRIX	
	63430		584	x 3	INTO		MATRIX	
	76020		SXO	82	INTO		MATRIX	
157	96500		585	202	INCRE		MATRIX	
160		1 000 .	828				MATRIX	
160	4360		9Xe	٥;	x6	•	PATRIX	
	73710		SX7	: ;	PUT ADDRESS OF ACTAIN I	INTO 80	MATRIX	
161	676	1000.0	PSS	0			PATRIX	
101	53370		543	X X	CONTENTS OF BOLDK	INTO X2	FATRIX	
	40332		Fx3	x3+x2	INT		PATRIX	
162	162 73772		5 X Z	7+8	NEXT ELEMENT OF *8		MATRIX	
	30663		FX6	X+9	INTO C(ILA)		PATRIX	
	24404							

MATRIY NULTABI	MATRIY - MISCELLANEOUS MATRIX OPERATIONS. Multabt - multiply a matrix by the thanspuse of another	SE CF	ANOTHEP	CCMPASS 3.3-428.	12/08/78 15-15-17-	15.15.17.	PAGE	20
	67441	985	84-81	DECREMENT M2			MATRIX	720
163		15	84,80,LCDP.0				PATRIX	721
	655	SA6		STOKE C(1, J)			PATRIX	722
	6552	585	65+R2	GET NEXT ELEPENT OF +C+			FATRIX	723
164		542		PUT ADDRESS OF ME INTO	X2		MATRIX	724
	53220	SA2		PUT P2 INTO X2			MATRIX	725
	3420	584	x2	PUT RZ INTO R4 AGAIN			PATRIX	726
165		587	87-81	DECREMENT LOOP COUNT			MATRIX	727
	73441	5x4	X 4+91	GET NEXT ROW ELEMENT DF +8+	F +8+		PATRIX	728
	070700160 +	13	87,90,1 GOP.C				MATRIX	729
166		\$ W 6	A1+3	PUT ACOPESS OF RELATA INTE X4 AGAIN	INTC X4 AG	AIN	MATRIX	730
	73111	SXI	XI+81	INCREMENT FOR REXT ROW OF *A*	OF +A+		MATRIX	731
	3551	SXS	X5+81	INCREMENT FOR MEXT ROW	*3* JO		PATRIX	732
167		585	90	RESET COLUMN INCREMENT		O ZERO	PATRIX	733
	96730	587	63	RESET COLUMN INCREMENT	FOP +8+ T	TO ZERO	MATRIX	734
	200777776	230	70-1				MATRIX	735
170		71	X0,100P.C				MATRIX	736
	0000152 +	60	FUL TABT	RETURN			HATRIX	737

CALLING SEQ: CALL PULITORY AN BY K PAIRLY BY A CCNSTANT. CALLING SEQ: CALL PULITORY AN BY K PAIRLY BY A CCNSTANT. PEGINERIS I F - IN - SCALAR N - IN - NUMBER DE POUS IN B C - CUT - PFSULTANT MATRIX OF A*B NOTE I FORTRAN ECUIVALENT ROLINE SURFOUTINF MULTCIA, BA, P, C, D ON 10 1-1, N ENTRY EXIT FOUNDERSS OF RILLI) INTO X2 SAS A*B1 PUT ADDRESS OF CLIAI) INTO X5 SAS A*B1 PUT ADDRESS OF CLIAID X3		THE COURT OF THE C			***************************************		****
CALLING SEG: CALL WUITC(A.B.N.M.C) ***APPIX*** ***APPIX** ***APPIX*** ***APPIX** **APPIX** ***APPIX** ***APPI		:				•	PATRIX
### CALLING SEGI CALL MUITC(A,P,N,H,C) #### CALLING SEGI CALL MITC(A,P,N,C) #### CALLING SUPPLIES OF COLUMNS IN B #### CALLING SUPPLIES OF SUPPL		:	ROUTTA	IF TO MULTIP	IY AN N BY M PETRIX BY A CCN	ISTANT. **	MATRIX
### CALLING SEQ: CALL MUITC(APP, N, P, C) ### SEQUAR SEQUENTS I F - IN - SCALAR ### SEQUAR SEQUENTS IN B ### SEQUENTS IN B		:				:	MATRIX
### PEGIMENTS : # - IN - SCALAR # - IN - NUMBER OF ROUS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF A+B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF COLLUMNS IN B # - IN - NUMBER OF A+B # - IN - NUMBER OF ROUS IN B # - IN - NUMBER OF ROUS IN B # - IN - NUMBER OF ROUS IN B # - IN - IN IN IN COLLUMNS # - IN - NUMBER # - IN - IN COLLUMNS # - IN - NUMBER # - IN - IN COLLUMNS # - IN - NUMBER #		:	CALLIA		L MULTCIA, R, N, M, C)	:	PATRIX
### APGIMENTS : A - IN - SCALAR ### - IN - NUMBER OF POUS IN B ### - IN - NUMBER OF COLUNNS IN B ### - IN - NUMBER OF COLUNNS IN B ### - IN - NUMBER OF COLUNNS IN B ### - IN - NUMBER OF COLUNNS IN B ### - IN - NUMBER OF COLUNNS IN B ### - IN - NUMBER OF COLUNNS IN B ### - IN - NUMBER OF COLUNNS IN B ### - IN - NUMBER OF POUT IN COLUNNS ### - IN - NUMBER OF POUT IN COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT ON COLUNNS ### - IN - NUMBER OF POUT		:				:	FATRIX
### ### ##############################		:	APG1.ME	1	· ×	:	MATRIX
*** **********************************		:			- KATPIX	:	MATRIX
** - IN - NUMER OF COLUMNS IN B ** - IN - NUMER OF COLUMNS IN B ** - CUT - PFSULTANT MATRIX OF A+B ** SURPCUTINE MULTCIA, B, N, P, C) ** OI O J=1, P, OI O I=1, P, OI		:			- NUMPER OF ROWS IN	•	PATRIX
C - CUT - PFSULTANT MATRIX OF A+B *** *** *** *** *** *** ***		:			- NUMBER OF COLUMNS IN		MATRIX
SURPCUTINE HULTC(A,P,L,C) SURPCUTINE HULTC(A,P,		:			CUT - PESULTANT MATRIX OF		MATRIX
SURPUTINE MULTC(A,B,A,P,C) SURPUTINE MULTC(A,B,A,P,C) ON 10 J=1,N END A=FURN END A=FURN SA2 A A+81 SA3 A A+81 PUT ADDRESS OF R(1,1) INTO X3 SA4 A A+81 PUT ADDRESS OF R(1,1) INTO X3 SA4 A A+81 SA5 A A+81 PUT ADDRESS OF R(1,1) INTO X3 SA4 A A+81 PUT ADDRESS OF R(1,1) INTO X3 SA4 A A+81 PUT ADDRESS OF R INTO X3 SA4 A A+81 PUT ADDRESS OF R(1,1) INTO X5 SA4 A A+81 PUT ADDRESS OF R INTO X3 SA4 A A+81 PUT ADDRESS OF R(1,1) INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X3 SA4 A A+81 PUT ADDRESS OF R INTO X5 SA4 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT ADDRESS OF R INTO X5 SA5 A A+81 PUT A INTO X1 SA5 A A+81 PUT A INTO X5 SA5 A A+81 PUT A		:				•	MATPIX
SUPPUTINE MULTC(A,B,h,F,C) *** *** *** *** *** *** ***		:	NOTE	1 F09	TPAN ECUIVALENT ROLTINE	:	MATRIX
SURFULINF MULTC(A,B,A,F,C) 10 Jalen 10 Jalen 10 Jalen 10 C(I,J) = A*B(I,J) 4 FTURN 10 C(I,J) = A*B(I,J) 10 Talen 1		:				:	MATRIX
### DIT ### DIT #### DIT #### DIT ##########		:		SUR	PRUTINE MULTCIA, B, N. P.C.	:	MATRIX
20 10 J=1,P 00 10 [=1,P 10 C(I,J) = A*B(I,J) *** *** *** *** *** *** *** *		:		•10	ENSIGN R(Nom) C (Nom)	:	MATRIX
### 10 C(1,4) = A+8(1,4) ###		:		90	10 4-1.7	:	PATRIX
### 10 C(I,J) = A+B(I,J) ####################################		:		00	10 I-1,N	:	MATRIX
### FETURE ### ###############################		:			,J) = A*8(I,J)	•	MATRIX
######################################		:			NAO	•	MATRIX
######################################		:		END		:	PATRIX
######################################		:				:	PATRIX
SAS A1+81 PUT ADDRESS OF B(1,1) INTO X2 SA3 A2+81 PUT ADDRESS OF N INTO X3 SA4 A3+81 PUT ADDRESS OF N INTO X3 SA5 A4+81 PUT ADDRESS OF N INTO X4 SA5 X3 X3 SA1 X1 PUT A INTO X1 SA3 X3 SA4 X4 IX7 X3*X4 PUT N INTO X3 SA4 X4 IX7 X3*X4 PUT N INTO X4 IX7 X3*X4 PUT N**N INTO X7 SAS X7 PUT N**N INTO X7 SAS X7 PUT CONTENTS OF *8* INTO X3 FX6 X1*X3 PUT A**N INTO X6 SA5 X5 X5*X5 STORE *C* SA5 X5 X5*N INTO X6 SA5 X5*N INTO X8 SA5 X5*N INTO		•			***************************************	***************	PATRIX
SA2 A1+81 PUT ADDRESS OF R(1,1) INTO X2 SA3 A2+81 PUT ADDRESS OF N INTO X3 SA4 A3+81 PUT ADDRESS OF N INTO X4 SA5 A4+81 PUT ADDRESS OF N INTO X4 SA1 X1 SA3 X3 PUT ADDRESS OF C(1,1) INTO X5 SA4 X4 PUT N INTO X4 IX7 X34X4 PUT N INTO X4 IX7 X34X4 PUT N INTO X4 IX7 X34X4 PUT N INTO X4 SA5 X7 PUT CONTENTS OF +8# INTO X3 FX6 X10 X3 SYZ X2+81 GET NEXT ELEMENT OF +8# SX5 X5+81 GET NEXT ELEMENT OF +6# SX5 X5+81 GET NEXT ELEMENT OF +6# SX5 X5+81 GET NEXT ELEMENT OF +C#	1	2010	252	••	ENIKT/EXII		MATRIX
SA2 A1+81 PUT ADDRESS OF R(1,1) INTO X2 SA4 A3+81 PUT ADDRESS OF N INTO X4 SA5 A4+81 PUT ADDRESS OF N INTO X4 SA5 A4+81 PUT ADDRESS OF N INTO X4 SA1 X1 PUT A INTO X1 SA3 X3 PUT N INTO X4 IX7 X3+X4 PUT N INTO X4 IX7 X3+X4 PUT N+M INTO X7 SB2 X7 PUT CONTENTS OF +8+ INTO X3 FX6 X1+X3 PUT A+M INTO X6 SA5 X2 PUT CONTENTS OF +8+ INTO X3 FX6 X1+X3 STORE +C+ SA5 X2+81 GET PET ELEMENT OF +6+ SX5 X5+81 GET PET ELEMENT OF +C+ SX5 X5+81 GET PET ELEMENT OF +C+ SX5 X5+81 GET PET ELEMENT OF +C+	2 6110000001		281	-			MATRIX
SA3 A2+81 PUT ADDRESS OF N INTO X3 SA4 A3+91 PUT ADDRESS OF N INTO X4 SA5 A4+91 PUT ADDRESS OF N INTO X4 SA3 X3 SA4 X4 IX7 X3+X4 PUT N INTO X4 IX7 X3+X4 PUT N INTO X4 IX7 X3+X4 PUT N INTO X7 SB2 X7 40VE N*N TO B2 FX6 X1*X3 X2 PUT CONTENTS OF *8# INTO X3 FX6 X1*X3 X2 PUT CONTENTS OF *8# INTO X3 FX6 X1*X3 X2 SA6 X5 SA6 X5 SA6 X5 SA6 X5 SA6 X5 SA6 X5 SA7 GET PET ELEMENT OF *8# SX5 X5+81 GET PET ELEMENT OF *C* SX5 X5+81 GET PET ELEMENT OF *C* SX5 X5+81 GET PET ELEMENT OF *C*	54211		SAZ	A1+81	ADDRESS OF B(1,1)		MATRIX
\$4	54321		SA3	A2+81	ADDRESS OF N INTO		PATRIX
\$4.61 PUT ADDRESS OF C(1,1) INTO X5 \$4. X1 PUT A INTO X1 \$4. X2 PUT N INTO X3 \$5.4 X7 PUT N INTO X4 IX7 X34X4 PUT N+M INTO X7 \$8.2 X7 PUT N+M INTO X7 \$8.2 X7 PUT CONTENTS OF 484 INTO X3 \$7.0 PUT CONTENTS OF 484 INTO X3 \$7.0 PUT CONTENTS OF 484 INTO X3 \$7.0 PUT CONTENTS OF 484 \$7.0 PUT CONTENTS OT 484 \$7.0 PUT CONTENTS OF 484 \$7.0 PUT CONTENTS OT 484 \$7.0 PUT CONTENTS OT 484 \$7.0 PUT CONTENTS OT 484 \$7.0 PUT CONTENTS	3 54431		SA4	A3+81	ADDRESS OF M INTO		MATRIX
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		:	ARGUMENTS	NTS :		PATRIX	290
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		:			- IN - NUMBER OF ROWS IN A AND 8		262
		:			- NUMBER OF COLUMNS IN A A		193
		:			- GUT - RESULTANT MATRIX		194
		:					295
		:	NOTE		FORTRAN EQUIVALENT ROUTINE		196
		:				* PATRIX	197
		:			SURRCUTINE SUB(A, B, N, M,C)		798
		:			DIMENSION A(N,M), B(N,M), C(N,M)	PATRIX	199
		:			DO 10 J-1, H		800
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	73221		Sx2	X2+81	FOR NEXT ELEPENT OF	MATRIX.	824
	73551		SX5	X5+81	FOR NEXT ELEMENT OF	MATRIX	825
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SIGNATURE TOP VISCELLEAFERS CUI AFF CENTRED FUR DIPUT: NITURALLY DECUME FIGE FUR AFF CENTRED FUR DIPUT: SIGNATURE CONTRACTOR FURTHER PRINT INDICATOR. O . DO NOT PRINT MATPIX CHORTOLICE. TISCAL O . DO NOT PRINT MATPIX CHORTOLICE. O . DO NOT PRINT MATRIX CHORTOLICE. O . DO NOT PRINT MATRIX CHORTOLICE. O . DO NOT PRINT MATRIX CHORTOLICE	SIGNCHINE FOR PISCELLATED AGAINS THAID DO NGT PISCEL INDUBALLY DOCKELLANGE FEEL AF PESTREE FEED FEED THAID DO NGT PISCEL INDUBALLY DOCKELLANGE, ELI AF PESTRED FEED FEED THAID NGT PISCEL NISCEL COVARIANCE PARIX PRINT INDUCATES. SICH AS TARRING. COVARIANCE PARIX PRINT INDUCATOR. DIMENSION CAL48) *** A APRAY ECCHENT I — INTEGLATION VARIABLES. COMMON UNDIADOR CAL48 *** A APRAY ESCHENT I — INTEGLATION VARIABLES. COMMON UNDIADOR CALABATION TOUT AND THAID STOOT, NSPOOT *** A ARRAY SEGMENT I — INTEGLATION VARIABLES. COMMON UNDIADOR CALABATION TOUR PHINDIA PROCESSION PROFESSION	•	•	SCAL	5
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SICH AS IARAING, FUKCHING, ETC., FIT. INPUT ARGUMENTS COVARALMENT COVARALMENT COVARALMENT COVARALMENT CONTROL WITHER THE PRINT INDICATOR. *** RARAY SEGNENT 1 - INTEGALION VARIABLES. COPPON UNITAONIC GOOT JODGY, XAPPDOT, ZAPPOLI, DEPRPHY, XSPDCT, R APPAY SEGNENT 2 - DERIVATIVES. COPPON UNITAONIC GOOT JODGY, XAPPDOT, PRINTINGS *** RARAY SEGNENT 3 - SIATE VARIABLES. COPPON UNITAONIC GOOT JODGY, XAPPDOT, PRINTINGS *** RARAY SEGNENT 3 - SIATE VARIABLES. COPPON UNITAONIC GOOT JODGY, XAPPDO, XC, ZO, MO, UBASO, WASDO, *** RARAY SEGNENT 4 - PEF, VALUES FOR LOCAL LINEARIZATION. COPPON US, WASO, THETA, XAPP, ZAFP, OFF, XSP, THETAS, *** RARAY SEGNENT 5 - INPUT FFREES AND MCMENTS. COPPON US, WASO, THETA, XAPP, ZAFP, OFF, XSP, ZSP, THETAS, *** RARAY SEGNENT 5 - INPUT FFREES AND MCMENTS. COPPON WEIGHT GO, YN, YN, ZZ, ZA, ZA, ZA, ZA, ZA, ZA, ZA, ZA, ZA	SICH AS IARRING, FURCHING, ETC., FIT. INPUT ARGUMENTS COMMON LONG PRINT MATRIX CHICATOR. REPRAY ESCHENT 1 - INTEGATION VALABLES. COPHON UNITA-OND, SOUTH PRINT MATRIX CHICATOR. REPRAY ESCHENT 2 - DERIVATIVES. COPHON UNITA-OND, SOUTH PRINT MATRIX CHICATOR. REPRAY ESCHENT 2 - DERIVATIVES. COPHON UNITA-OND, SOUTH PRINT MATRIX CHICATOR. REPRAY ESCHENT 3 - SIATE VARIABLES. COPHON UNITA-OND, SOUTH PRINT MATRIX REPRAY SECHENT 3 - SIATE VARIABLES. COPPON UNITA-OND, SOUTH PRINT MATRIX REPRAY SECHENT 3 - SIATE VARIABLES. COPPON UNITA-OND, SOUTH MATRIX CONTOURS SOUNDS	C* NATURALLY OCCUR ELSEWHERE BUT ARE D	FUR OLIPUTA .	SCAL	9
INPUT ARGUMENTS	**************************************		•	7775	1
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NPRN COVARIANCE PAINT MAINT INDICATOR PISSAL	NPRN CUVARIANCE PATRIX PRINT INDICATOR. PISSAL		SIN .	SCAL	•
O = 00 hol Print Fairs on Output file. PISCAL DIMENSION CAL48) COPPON 11HE, 10-FILME, DITCUT, DIGUTE, THAN R APPAY SEGHENT 1 - INTEGRATION VARIABLES. COPPON 11HE, 10-FILME, DITCUT, DIGUTE, THAN R APPAY SEGHENT 2 - DERIVATIVES. COPPON 1000T, JODOT, JODOT, JODOT, JODOT, JODOT, VSPOOT P VOIDS OF COPPON SEGMENT 3 - 13 JET VARIABLES. R ARRAY SEGHENT 3 - STATE VARIABLES. COPPON US, MOST, VARPONT, PHILDOT, PRIDGIL, PSPOOT, PR R ARRAY SEGHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT 5 - INPUT FURCES AND HUMENTS. R ARRAY SEGMENT 5 - INPUT FURCES AND HUMENTS. R ARRAY SEGMENT 5 - INPUT FURCES AND HUMENTS. R ARRAY SEGMENT 5 - INPUT FURCES AND HUMENTS. COPPON SUFFOC, SUMPO, SUMFY, DET, SUMFY, DET, SUMP, DM. R ARRAY SEGMENT 7 - CONSTANTS. COPPON VEGGHENT 7 - CONSTANTS. COMPON PREAL, PEGAP, MULEN, MAP, LITOP, LOCAL DE, SUMPO, TALOP, PR R ARRAY SEGMENT 7 - CONSTANTS. COMPON PREAL, PEGAP, MULEN, MAP, LITOP, LOCAL DE, MOTO, PR R ARRAY SEGMENT 7 - CONSTANTS. COMPON PREAL, PEGAP, MULEN, MAP, LITOP, LOCAL DE, MOTO, PR R ARRAY SEGMENT 7 - CONSTANTS. COMPON PREAL, PEGAP, MULEN, MAP, LITOP, LOCAL DE, MOTO, PR R ARRAY SEGMENT 7 - CONSTANTS. COMPON PREAL, PEGAP, MULEN, MAP, LITOP, MOTO, PR R ARRAY SEGMENT 7 - CONSTANTS. COMPON PREAL, PEGAP, MULEN, MAP, LITOP, MOTO, PR R ARRAY SEGMENT 7 - CONSTANTS. COMPON PREAL, MOTO, POTO, POT	DIMENSION CALABI DIMENSION CALABI PARRAY SEGMENT 1 - INTEGRATION VAZIABLES. RAPRAY SEGMENT 2 - DERIVATIVES. COMPON 11ME, 10.7TIME, DITCUI, DITCUI, DARAN COMPON 10ME, 10.7TIME, DATCUI, DITCUI, DARAN COMPON 10ME, 10.7TIME, DATCUI, DATCUI, DEPPED, XSPDCT, RAPRAY SEGMENT 3 - DERIVATIVES. COMPON 10ME, 10.7TIME, DATCUI, DATCUI, DEPPED, XSPDCT, POUTT, DOUT, DOUD, DOUD, TODOI, YAPPOI, PHIDDI, PSIDDI, PSIDDI, YSPDOI COMPON 10ME, 10.7TIME, DATCUI, DATABLES. COMPON 10ME, 10.7TIME, DATCUI, DATABLES. COMPON 10ME, 10.7TIME, 10.7TIME	NPRNT COVARIANCE PATRIX PPINT	•	SCAL	10
### ##################################	PARPAY SEGRENT 1 - INTEGRATION VAZIABLES. COPPON INE,TO-FINE,TO-FINE,TOTOUZ,TMAX RAPPAY SEGRENT 2 - DERIVATIVES. COMPON UNDT, UDDI, UDDI, TODOUZ, TWAX RAPPAY SEGRENT 3 - STATE VARIABLES. COMPON UDON, UDDI, TODOUZ, TARAY RAPPAY SEGRENT 3 - STATE VARIABLES. COPPON UDA, MARCAY SEGRENT 3 - STATE VARIABLES. RAPPAY SEGRENT 3 - STATE VARIABLES. COPPON UDA, MARCAY SEGRENT 5 - THOUT FORCES AND HOMENTS. RAPPAY SEGRENT 5 - INPUT FORCES AND HOMENTS. RAPPAY SEGRENT 5 - CONSTANTS. COMPON UDFFORCES AND HOMENTS. RAPPAY SEGRENT 7 - CONSTANTS. COMPON WEIGHT-OFFILM STATES. RAPPAY SEGRENT 7 - CONSTANTS. RAPPAY SEGRENT 7 - CONSTANTS. COMPON WEIGHT-OFFILM STATES. RAPPAY SEGRENT 7 - CONSTANTS. RAPPAY SEGRENT 8 - RAPPAY SEGRENTS. RAPPAY SEGRENT 8	O . DO NOT PRINT MATRIX	•	SCAL	11
DIMENSION CALLES *** R ARRAY SEGRENT 1 - INTEGLATION VARIABLES. *** COPMON THE TO TIME DITUTIONIZATION VARIABLES. *** COPMON THE TO TIME DITUTIONIZATION VARIABLES. *** COPMON THE TO TIME DITUTIONIZATION VARIABLES. *** COPMON UNITABOOT SOUT SERVED VARIABLES. *** R ARRAY SEGRENT 3 - STATE VARIABLES. *** R ARRAY SEGRENT 3 - STATE VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SEGRENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORCES AND HOMENTS. *** R ARRAY SEGRENT 5 - INPUT FORC	DIMENSION CA149) *** RAPRAY SEGMENT 1 - INTEGRATION VAZIABLES. *** COPMON UTHE, TO-FITHE, DITUTIONIZ, THAX *** RAPRAY SEGMENT 2 - DERIVATIVES. *** COPMON UTHE, TO-FITHE, DITUTIONIZ, THAX *** RAPRAY SEGMENT 3 - STATE VARIABLES. *** RAPRAY SEGMENT 3 - STATE VARIABLES. *** RAPRAY SEGMENT 3 - STATE VARIABLES. *** RAPRAY SEGMENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** RAPRAY SEGMENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** RAPRAY SEGMENT 5 - INPUT FERCES AND MCMENTS. *** RAPRAY SEGMENT 5 - INPUT FERCES AND MCMENTS. *** RAPRAY SEGMENT 5 - INPUT FERCES AND MCMENTS. *** RAPRAY SEGMENT 5 - INPUT FERCES AND MCMENTS. *** RAPRAY SEGMENT 5 - INPUT FERCES AND MCMENTS. *** RAPRAY SEGMENT 5 - INPUT FERCES AND MCMENTS. *** RAPRAY SEGMENT 5 - CHASTANTS. *** CCMMOW WFIGHT, PIPELARIA, WHYLITM, LS, LTDS *** RAPRAY SEGMENT 7 - CHASTANTS. *** CCMMOW WFIGHT, PIPELARIA, WHYLITM, LS, LTDS *** RAPRAY SEGMENT 7 - CHASTANTS. *** CCMMOW WFIGHT, PIPELARIA, WHYLITM, LS, LTDS *** RAPRAY SEGMENT 7 - CHASTANTS. *** CCMMOW WFIGHT, PIPELARIA, WHYLITM, LS, LTDS *** RAPRAY SEGMENT 7 - CHASTANTS. *** CCMMOW WFIGHT, PIPELARIA, WHYLITM, LS, LTDS *** RAPRAY SEGMENT 7 - CHASTANTS. *** CCMMOW WFIGHT, PIPELARIA, WHYLITM, LS, LTDS *** RAPPAY SEGMENT 7 - CHASTANTS. *** CCMMOW WFIGHT, PIPELARIA, WHYLITM, PIPELARIA, PIPEL		•	SCAL	12
DIMENSION CAL48) *** R ARPAY SEGMENT 1 - INTEGRATION VARIABLES. *** R ARPAY SEGMENT 2 - DERIVATIVES. COMMON UNDITADOTATION TOTAL SAPPOLTA SPORT, SPORT, A VOITA PROTT REDOTATION SAPPOLTA SPORT, SPORT, R ARRAY SEGMENT 3 - STATE VARIABLES. COMMON USABAY SEGMENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT 4 - PEF. VALUES FOR HOLOSPORTANDO, THETALOPEN UNANDOMANDO, SUPER, SAPPOLA SOUNDO, R FALL MOALOON THETALO, RAPPOLA SPORTANDO, R RARAY SEGMENT 5 - INPUT FRACES AND MCMENTS. COMPON USABAY SEGMENT 5 - INPUT FRACES AND MCMENTS. COMPON USABAY SEGMENT 5 - LINEUT FRACES AND MCMENTS. R ARRAY SEGMENT 5 - LINEUT FRACES AND MCMENTS. COMPON SUPPROSENTED SOUNDO, SUPPROSEDED SOUNDON. R ARRAY SEGMENT 5 - CONTANTS. COMPON WEGGLIANDO SUPPROSED SOUNDO, SUPPROSEDED SOUNDON. R ARRAY SEGMENT 7 - CONTANTS. R ARRAY SEGMENT 8 - REPRESENTED SEGMENT SE	DIMENSION CAL48) *** R ARPAY SECHENT 1 - INTEGRATION VARIABLES. *** R APPAY SECHENT 2 - DERIVATIVES. *** COMMON 11HE, TO.FTIME, DITCUT2, THAY *** R APPAY SECHENT 2 - DERIVATIVES. *** COMPON UNDIT, DOOD, TD.DT. XAPPDOT, ZAPPOLT, DEPPH, XSPDCT, *** R ARRAY SECHENT 3 - STATE VARIABLES. *** R ARRAY SECHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SECHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SECHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 5 - INPUT FORCES AND WOMENTS. *** R ARRAY SECHENT 7 - CONSTANTS. *** R ARRAY SECHENT 8 - R ARRAY SECHENT 8	****************	*****	SCAL	13
*** R ARPAY SEGHENT 1 - INTEGRATION VARIABLES. *** COPPUN 11HE, TO.TITHE, DITCUT, DIGUTE, THAY *** R ARPAY SEGHENT 2 - DERIVATIVES. *** COPPUN 11HE, TO.TITHE, DITCUT, TRUTT, THAY *** R ARRAY SEGHENT 3 - STATE VARIABLES. *** R ARRAY SEGHENT 3 - STATE VARIABLES. *** R ARRAY SEGHENT 3 - STATE VARIABLES. *** R ARRAY SEGHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SEGHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SEGHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SEGHENT 5 - THPUT FFRCES AND MCMENTS. *** R ARRAY SEGHENT 5 - INPUT FFRCES AND MCMENTS. *** R ARRAY SEGHENT 5 - INPUT FFRCES AND MCMENTS. *** R ARRAY SEGHENT 7 - CLWSTANDS. *** R ARRAY SEGHENT 8 - SCONETAY. *** R ARRAY SEGHENT 7 - CLWSTANDS. *** R ARRAY SEGHENT 7 - CLWSTANDS. *** R ARRAY SEGHENT 8 - GEOFFINY. *** R ARRAY SEGHENT 8 - GEOFFINY. *** R ARRAY SEGHENT 7 - CLWSTANDS. *** R ARRAY SEGHENT 8 - GEOFFINY. *** R ARRAY SEGHENT 9 - THRUTTANDS. *** R ARRAY SEGHENT 9 - THRUTTANDS. *** R ARRAY SEGHENT 9 - THRUTTANDS. *** R ARRAY SEGHENT 9 - THRUT FFREEN. *** R ARRAY SEGHENT 9 - THRUTTANDS. *** R ARRAY SEGHENT 9	COMMON TIME, TO.FTIME, DITCUT, THAY *** R ARRAY SEGMENT 1 - INTEGRATION VARIABLES. *** R ARRAY SEGMENT 2 - DERIVATIVES. *** COMMON UDIT, DOTI, TODI, TAPPODT, ZAPPOLT, DERPHD, XSPDCT, *** R ARRAY SEGMENT 3 - STATE VARIABLES. *** R ARRAY SEGMENT 3 - STATE VARIABLES. *** COMPON UD, MED, COB, THETA, XAPP, ZAPP, DERPP, XSP, ZSP, THETAS, *** R ARRAY SEGMENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SEGMENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SEGMENT 5 - INPUT FORCES AND MCMENTS. *** R ARRAY SEGMENT 5 - INPUT FORCES AND MCMENTS. *** R ARRAY SEGMENT 5 - INPUT FORCES AND MCMENTS. *** R ARRAY SEGMENT 5 - CENSTANTS. *** R ARRAY SEGMENT 7 - CENSTANTS. *** CCMMON SUMFCO, SUMFO, SUMFX, DEP, SUMF, DEP, SUMP, DM, *** R ARRAY SEGMENT 7 - CCHSTANTS. *** CCMMON OFFGAT, OFFGAT, MEN, MERPH, MED, SUMP, DT, *** R ARRAY SEGMENT 7 - CCHSTANTS. *** CCHMON OFFGAT, OFFGAT, MEN, MERPH, MED, SUMP, DT, *** R ARRAY SEGMENT 7 - CCHSTANTS. *** CCHMON OFFGAT, OFFGAT, MED, MED, SUMP, SUMP, DT, *** R ARRAY SEGMENT 7 - CCHSTANTS. *** CCHMON OFFGAT, OFFGAT, MED, MED, MED, MED, MED, MED, MED, MED		P.1 S	SCAL	14
COMMON LUNGIADOR TO FILMES AT THE SEATION VARIABLES. *** R APPAY SEGHENT 1 - INTEGRATION VARIABLES. *** R APPAY SEGHENT 2 - DERIVATIVES. COMMON LUNGIADORI, DOUT, APPODIA, DAPPOLI, DEPPHANSPORT, A 25001/152001. *** R ARRAY SEGHENT 3 - STATE VARIABLES. *** R ARRAY SEGHENT 3 - STATE VARIABLES. COMPON LUBAGOR, THETA, XAPP, ZAPP, OFRPP, XSP, THETAS, A VOLFACO, DOUTHERA, XAPP, ZAPP, OSPP, OS	COMMON INE, TO. FILME, DITCUI, DIQUIZ, THAX R APRAY SEGMENT I - INTEGRATION VARIABLES. R APRAY SEGMENT Z - DERIVATIVES. COMMON UNDI, VUONI, VOONI, VOOTI, PER PROTI, PER PROLI, VSPOOTI P ZSPOUTI, TSPOOTI, NOVIGEN OF A SEGMENT J - STATE VARIABLES. COMPON USANGOR, THETA, XAPP, ZSP, STP, THETAS, A RARAY SEGMENT J - PEF VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT J - PEF VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT J - PEF VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT J - PEF VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT J - PEF VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGMENT J - REVUT FFREES AND MCMENTS. CCMMON USERSO, SUFFES, DEF SOUFE, DE SOUPE, DE SOUFI,				2
COPPON INF. TO.FITHE.DITUT.DITOUT2.THAX *** R APRAY SFGHENT 2 - DERIVATIVES. COMPON UDOT, UDOT, UDOT, TOOT, XAPPODT, ZAPPUCT, DERPFC, XSPDCT, A 25POUT.TSPDOT. *** R ARRAY SECHENT 3 - STATE VARIABLES. COPPON UB. MB. OB. THETA. XAPP. ZAFP. OFRPP. XSP. ZSP. THFTAS. A VB. PB. RB. YAPP. PHI.PSI.YSP *** R ARRAY SFCKENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R ARRAY SFCKENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R ARRAY SFCKENT 5 - INPUT FFRCES AND MCMENTS. CCMPON UD. WC. OO. THETA. O. YAPP. DF. S. SUMP. DM. R ARRAY SFCKENT 5 - INPUT FFRCES AND MCMENTS. CCMPON WEGHTG. SUMPOS. SUMPOS. SUMP. DF. S. SUMP. DM. *** R ARRAY SECKENT 5 - INPUT FFRCES AND MCMENTS. CCMPON WEGHTG. SIZELING. MF. S. DET. S. SUMP. DM. *** R ARRAY SECKENT 5 - CCMSTANTS. CCMPON WEGHTG. SIZELING. MF. S. LITES. CCMPON WEGHTG. MF. S. LITES. R ARRAY SECKENT 7 - CCMSTANTS. CCMPON WEGHTG. MF. S. LITES. CCMPON WEGHTG. WG. WG. WG. WG. WG. WG. WG. WG. WG. W	COMMON 11HE, TO.FITINE, DITCUT, DITCUT2, THAX *** R APRAY SFGHENT 2 - DEMINATIVES, COMMON UNDT, WDDT, COOT, TDDT, XAPPDDT, ZAPPDCT, DEMPHD, XSPDCT, A VOOT, PROCT, REDOIT, YAPPDDT, PHIDDT, PSIDDT, YSPDOT *** R ARRAY SEGFENT 3 - SIATE VARIABLES. COMPON UB, MB, CB, THETA, XAPP, PHI, PSI, PSI, DST, PTHETAS, A RARAY SEGFENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. COMPON UB, WB, CB, THETA, XAPP, ZAPP, CP, PP, SPP, THETAS, A RARAY SEGFENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R ARRAY SEGFENT 5 - INPUT FFRCES AND MCMENTS. COMPON SUMFYO, SUMFO, SUMFA, DET, SUMFA, DB, SUMP, DB, R ARRAY SEGFENT 5 - INPUT FFRCES AND MCMENTS. COMPON SUMFYO, SUMFO, SUMFA, DB, SUMFA, DB, SUMFA, DB, R ARRAY SEGFENT 7 - COMSTANTS. COMPON WEIGHT, G, IX, IY, IZ, IXZ, IM, WH, LITH, LS, LTDS R APRAY SEGFENT 7 - COMSTANTS. COMMON CHEGAL, PHEGAD, ML, ME, SH, MB, LTDE, MTDT, R APRAY SEGFENT 7 - COMSTANTS. COMMON CHEGAL, PHEGAD, ML, ME, ME, PRI, MS, LTDE, MTDT, R ARRAY SEGFENT 7 - COMSTANTS. COMMON CHEGAL, PHEGAD, MILLY, MB, MB, MB, MB, MB, MB, MB, MB, MB, MB	*** R ARPAY SEGMENT 1	•		m .
COMPON UDDIADOT, TDCT, XAPPDOT, ZAPPUCT, DERPED, XSPDCT, 2 SPDCT, SEGRENT 2 - DERIVATIVES. COMPON UDDIADOT, TDCT, XAPPDOT, PSIDOT, YSPDCT, 8 NOTIFICATION SOUTH STORY, PRINCE STORY, SSP, SSP, THETAS, A WB, PB, RB, TAPP, TAPP, TAPP, DERPENES, SSP, THETAS, 8 ARRAY SEGRENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. 8 COMPON UD, VC. 900, THETAS, XAPP, 22PPC, XC., ZO, MO, UBASO, MASDO, 1 HETAZO, PSIAO, PHIAO, PCDO, VO, PO, RO, YAPPC, FHIO, PSIO, YO, LO, 1 HETAZO, PSIAO, PHIAO, PCDO, VO, PO, RO, YAPPC, FHIO, PSIO, YO, LO, 1 HETAZO, SUMPO, SUMPO, SUMPO, SUMPO, SUMPO, DEAS, SUMPO, 1 RARAY SEGRENT 5 - INPUT FFREES AND MCMENTS. 1 COMPON SUMFXO, SUMPO, SUMPO, SUMPO, SUMPO, SOUP,	COMPON UNDITADOTATION OF THE STATE OF THE ST				• •
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A SEPULITISPOOT. *** R ARRAY SECHENT 3 - STATE VARIABLES. *** R ARRAY SECHENT 3 - STATE VARIABLES. *** R ARRAY SECHENT 3 - STATE VARIABLES. *** R ARRAY SECHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SECHENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. *** R ARRAY SECHENT 5 - INPUT FERCES AND WEMENTS. *** R ARRAY SECHENT 5 - INPUT FERCES AND WEMENTS. *** R ARRAY SECHENT 5 - INPUT FERCES AND WEMENTS. *** R ARRAY SECHENT 5 - INPUT FERCES AND WEMENTS. *** R ARRAY SECHENT 5 - CENTINAM, ITM, LS, LTDS *** R APRAY SECHENT 6 - GEOFFIRY. *** R APRAY SECHENT 7 - CLNSIANIS. *** R APRAY SECHENT 8 - CLNSIANIS. *** R APRAY SECHENT 8 - CLNSIANIS. *** R APRAY SECHENT 8 - CLNSIANIS. *** R APRAY SE	TOWER SECRET 3 - STATE VARIABLES. COMPON UB. WB.OB. THETA. XAPP. ZAFP.OFRPP. XSP. ZSP. THETAS. A VB.PB.RB. YAPP.PHI.PSI.YSP COMPON UB. WB.OB. THETA. XAPP. ZAFP.OFRPP. XSP. ZSP. THETAS. A FETALO. PEF. VALUES FOR LOCAL LINEARIZATION. RARRAY SFGKENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. RARRAY SFGKENT 5 - INPUT FFRCES AND WCMENTS. CCMMON SUMFYO. SUMFO. SUMFY.OFY. SUMFZ. DF. S. SUMM. DM. RARRAY SFGKENT 5 - INPUT FFRCES AND WCMENTS. CCMMON SUMFYO. SUMFO. SUMFY.OFY. SUMFZ. DF. S. SUMM. DM. RAPRAY SFGFENT 6 - GEOFFIFY. CCMMON VERGY. PEF. TH. IT. IZ. IX. Z. IM. MM. LITM. LS. LIDS RAPRAY SFGFENT 7 - CCM. SIMP. SUMFY. SUMFD. SUMFO. TALOD. RAPRAY SFGFENT 7 - CCM. SIMP. SUMFY. SUMFD. SUMFO. TALOD. RAPRAY SFGFENT 7 - CCM. SIMP. SUMFY. SUMFD. SUMFY. SUMFD. SUMFY. SU	CONTON			0
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COMPON UB. WB. OB. THETA. XAPP. ZAFE VARIABLES. COMPON UB. WB. OB. THETA. XAPP. ZAFP. DERPP. XSP. ZSP. THETAS. A VB. PB. RB. YAPP. PHI. PSI. YSP. COMPON UD. WG. OG. THETA. XAPP. ZAFP. DERP. XSP. ZSP. THETAS. R ARRAY SEGRENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R THETALO. PSIAO. PHIAO. PROS. XG. ZO. HO. UBASO. WBASO. WASDO. R FALL HO. LO. POSIAO. PHIAO. PROS. XG. ZO. HO. UBASO. WBASO. WASDO. R RALL HO. LO. POSIAO. PHIAO. PROS. XG. ZO. HO. UBASO. WBASO. WASDO. R RARAY SEGRENT 5 - INPUT FORCES AND HOMENTS. COMPON VEIGHTO. SUMPO. SUMPO. SUMPY. DEP. SUMP. DM. SUMPTO. SUMPTO. SUMPO. SUMPY. DEP. SUMP. DM. R ARPAY SEGRENT 6 - GEOFETRY. COMPON VEIGHTO. SUMPO. SUMPY. DEP. SUMP. DM. R ARPAY SEGRENT 7 - COMSTANTS. COMPON VEIGHTO. PREGAUNU. KW. KRAPP. KCOM. TALENG. TALCOM. TALD. R APPLY SEGRENT 7 - COMSTANTS. COMPON VEIGHTO. PREGAUNU. KW. KRAPP. KCOM. TALENG. TALCOM. TALD. R APPLY SEGRENT 7 - COMSTANTS. COMPON VEIGHTO. PREGAUNU. KW. KRAPP. KCOM. TALCOM. TALO. R APPLY SEGRENT 7 - COMSTANTS. COMPON VEIGHTO. PROS.	RARRAY SECHENT 3 - STATE VARIABLES. COPPON UB.MB.OB.THETA.XAPP.ZAFP.DFRPP.XSP.ZSP.THETAS. A VB.PB.RB.THETA.XAPP.ZAFP.DFRPP.XSP.ZSP.THETAS. RARRAY SFCKENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. RARRAY SFCKENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. REAL HO.LO.POS.THETAO.XAPPO.ZAPPO.XC.ZO.NO.UBASO.WBASO.WASDO. RFAL HO.LO.POS.THETAO.XAPPO.ZAPPO.XC.ZO.NO.UBASO.WBASO.WASDO. RFAL HO.LO.POS.THETAO.XAPPO.ZAPPO.XC.ZO.NO.UBASO.WBASO.WBSO.WBSO.WBSO.WBSO.WBSO.WBSO.WBSO.WB				::
COPPON UB, MB, CB, THETA, XAPP, ZAFP, DFRPP, XSP, ZSP, THFTAS, A VB, PB, RB, YAPP, PHI, PSI, YSP COMPON UB, MB, CB, THETA, XAPP, ZAFP, DFRPP, XSP, ZSP, THFTAS, R ARRAY SFGRENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R THETALO, PSIAO, PHIAO, PCDO, VO, PC, RO, YAPPC, FHIO, PSIO, YO, LO, PR NO, VBSO RFAL MO, LO, MC, CO, THETAO, XBP, CDO, VO, PC, RO, YAPPC, FHIO, PSIO, YO, LO, PR RFAL MO, LO, MC, CO, SUMMO, SUMFX, DFY, SUMFZ, DFZ, SUMM, DM, R ARRAY SEGRENT 5 - INPUT FFRCES AND MCMENTS. CCMMON SUMFYO, SUMFO, SUMFY, DFY, SUMFZ, DFZ, SUMM, DM, SUMFYO, SUMIO, SUMFY, DFY, SUMFZ, DF, SUMM, DM, R APPAY SEGFENT 6 - GEOFFTY. CCMMON WIGHT, G, IX, IY, IZ, IXZ, LM, MM, LTDM, LS, LTDS R APRAY SEGFENT 7 - CONSTANTS. CCMMON OMEGIL, PREGADANU, KN, KREPP, KCIN, TAUENG, TAUCON, TAUD, R APRAY SEGFENT 7 - CONSTANTS. CCMMON OMEGIL, PREGADANU, KN, KREPP, KCIN, TAUENG, TAUCON, TAUD, R APPAY SEGFENT 7 - CONSTANTS. COMPONDED, POR, MCG, KCIN, KC	COPPON UB, MB, CB, THETA, XAPP, ZAPP, DERPP, XSP, ZSP, THETAS, A VB, PB, RB, YAPP, PHI, PSI, YSP COMPON UB, MB, CB, THETA, XAPP, ZAPP, DERPP, XSP, ZSP, THETAS, A THETACO, PSIAO, PHI, PSI, YSP A THETACO, PSIAO, PHI, PSI, YSP A THETACO, PSIAO, PHI, PSI, YSP, SO, MO, UBASO, WBASO, WBASO	*** R ARRAY SEGMENT 3			13
COMPON UB.WB.CB.THETA.XAPP.ZAFP.DFRPP.XSP.ZSP.THFTAS, WB.PB.RB.YAPP.PHI.PSI.YSP COMPON UD.WC.CO.THETA.XAPP.ZAPPC.XC.ZO.MC.UBASO.WBASO.WASDO. THETALO.PSIAO.PHIAO.PC.XC.ZO.PC.YO.PC.FHIO.PSIO.YO.LO. RFAL MO.LO.MO OC.VESSO RFAL MO.LO.MO COMPON UD.WC.CO.THETA.C.SUPHO.SUPFX.DFX.SUPFZ.DFZ.SUPM.DM. RARAY SECKENT 5 - INPUT FCRCES AND MCMENTS. COMPON SUPFXO.SUPFZO.SUPFY.DFX.SUPFZ.DFZ.SUPM.DM. SUMFXO.SUPFZO.SUPFZO.SUPFY.DFY.SUPFZ.DFZ.SUPM.DM. COMPON VEIGHT.G.IX.IY.IZ.IXZ.HW.MM.ITTM.LS.LTDS RFAL G.IX.IY.IZ.IXZ.HW.KE.WFRPM.KCCM.TAUENG.TAUCDM.TALD. COMMON OFFICER.TO.T.C.SUPFZO.SUPFZO.TH.DFX.TDS.KOTDE.WOTDT. RAPPAY SECFENT 7 - CONSTANTS. COMMON OFFICER.TO.T.C.SUPFZO.TM.TO.T.S.LTDS RFAL G.IX.IY.IZ.IXZ.HW.YEW.WCCM.TAUENG.TAUCDM.TALD. R APPAY SECFENT 7 - CONSTANTS. COMMON OFFICER.MCCA.MCCM.TAUENG.TA.MCTM.RCTDE.WOTDT. R APPAY SECFENT 7 - CONSTANTS. R APPAY SECFENT 8 - R APPAY 8 - R AP	COMPON UB, WB, CB, THETA, XAPP, ZAPP, DFRPP, XSP, ZSP, THETAS, WB, PB, RB, YAPP, PHI, PSI, YSP COMPON UD, WC, GO, THETA, XAPP, LAPP, DFR, VALUES FOR LOCAL LINEARIZATION. REAL NO, VEASO REAL NO, LO, NO SUMFXO, SUMFZO, XAPPO, ZAPPC, XC, ZO, MO, UBASO, WASOO, WASOO, REAL NO, LO, NO SUMFXO, SUMFZO, SUMPO, SUPFX, DFX, SUMFZ, DFZ, SUMP, DM, SUMFYO, SUMFZO, SUMPO, SUMFY, DFY, SUMP, DL, SUPP, DM, COMPON VEIGHT, G, IX, IY, IZ, IXZ, LM, MM, ITM, LS, LTDS REAL G, IX, IY, IZ, IXZ, LM, LM, ITM, LS, LTDS REAL G, IX, IY, IZ, IXZ, LM, LM, ITM, LS, LTDS REAL G, IX, IY, IZ, IXZ, LM, LM, ITM, LS, LTDS REAL WO, WW, WFERPEN KCON, TALENG, TALED, ROLL, PDEM, KDEC, PDEM, KD, WC, WC, WC, WC, WC, WC, WC, WC, WC, WC	•			4
*** R ARRAY SFGRENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R *** R ARRAY SFGRENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R *** R ARRAY SFGRENT 4 - PEF. VALUES FOR LOCAL LINEARIZATION. R *** NO.VEASO *** R ARRAY SEGRENT 5 - INPUT FFRCES AND MCMENTS. *** R ARRAY SEGRENT 5 - INPUT FFRCES AND MCMENTS. *** R ARRAY SEGRENT 5 - INPUT FFRCES AND MCMENTS. *** R ARRAY SEGRENT 6 - GEOPETRY. *** R ARRAY SEGRENT 6 - GEOPETRY. *** R ARRAY SEGRENT 6 - GEOPETRY. *** R ARRAY SEGRENT 7 - CLNSTANTS. *** R ARRAY SEGRENT 7 - CLNSTANTS. *** R ARRAY SEGRENT 7 - CLNSTANTS. *** R ARRAY SEGRENT 6 - GEOPETRY. *** R ARRAY SEGRENT 7 - CLNSTANTS. *** R ARRAY SEGRENT 6 - GEOPETRY. *** R ARRAY SEGRENT 6 - GEOPETRY. *** R ARRAY SEGRENT 7 - CLNSTANTS. *** R ARRAY SEGRENT 7 - CLNSTANTS. *** R ARRAY SEGRENT 8 - CLNSTANTS. *** R ARRAY SEGRENT 8 - CLNSTANTS. *** R ARRAY SEGRENT 8 - CLNSTANTS. *** R ARRAY SEGRENT 9 - R R R R R R R R R R R R R R R R R R	**	COPPON	S,		15
COMPON UD, WC, OD, THETAD, XAPPO, ZAPPC, XC, ZO, MC, UBASO, WEASO, WASDO, A THETALO, PSIAO, PHIAO, PCDO, VO, PC, RO, YAPPC, FHIO, PSIO, YO, LO, P R RO, VASO *** *** *** *** *** *** ***	COMPON UDANGAGOATHETADAXAPPOAZAPPGAKGAGOANGASOANGASOANGAGOATHETAGOASAPASOANGAGOATHETAGOASAPASOANGAGOATHETAGOASAPASOANGAGOATHETAGOASAPASOANGAGOATHETAGOASAGOANGAGOATHETAGOASAGOATHETAGOASAGOATHETAGOASAGOATHETAGOASAGOATHETAGOASAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHETAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOATHAGOAT	•			16
COMPON UD, WO, WO, WO, WO, WO, WO, WO, WO, WO, WO	COMPON UO, WC. DO. THETALO. XAPPO. ZAPPO. XC. ZO, MO, URASO, WASDO, P. T.	A TABLETON OF THE PARTY OF THE			12
COMPON UDANCADOATHETADAXAPPOAZAPPOAXOADANDAUBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASOANBASO	CCMPCN UOAVCAOO,THETAO,XAPPO,ZAPPO,XC,ZO,MO,UBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOO,WBASOOOO,WBASOOO,WBASOOOO,WBASOOOO,WBASOOOO,WBASOOOO,WBASOOOO,WBASOOOOO,WBASOOOO,WBASOOOO,WBASOOOO,WBASOOOO,WBASOOOO,WBASOOOOO,WBASOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO	* AKKAT STOREN 4 - PET. VALUES			9 0
THETALO.PSIAO.PHIAO.PCDO.VO.PC.RO.YAPPC.FHIO.PSIO.YO.LO. P REAL MO.LO.PO. CCPMON SUMFXO.SUMFZO.SUMFY.DFY.SUMFZ.DFZ.SUMM.DM. SUMFYC.SUMFZO.SUMFY.DFY.SUMFZ.DFZ.SUMM.DM. SUMFYC.SUMLO.SUMFY.DFY.SUMFZ.DFZ.SUMM.DM. REAL SUMFYC.SUMLO.SUMFY.DFY.SUMFZ.DFZ.SUMM.DM. CCPMON VEIGHT.G.IX.IX.IX.IX.LM.WM.LITM.LS.LIDS REAL G.IX.IX.IX.IX.IX.LM.WM.LITM.LS.LIDS REAL G.IX.IX.IX.IX.IX.LM.WM.LITM.LS.LIDS REAL G.IX.IX.IX.IX.IX.LM.WM.LT.NM.LT.LD. CCMON OMEGAL. PEGAW.MU.KW. KRPPM.KCCN.IAUENG.TAUCO.TAUD. REAL G.IX.IX.IX.LM.LM.NT.NM.CO.TV.KD.TD.W.CDD.YORDI. ROBEL.POEL.ROE.YOET.ROEY.ROEZ.ROEZ.ROED.YOEDI. ROBEL.POEL.ROEW.ROET.ROEX.ROEZ.ROED.YOEDI. ROBEL.POEL.ROEW.ROEM.ROEX.ROEZ.ROED.YOEDI. ROBEL.POEL.ROEW.ROEM.ROEX.ROEZ.ROEM.ROEDE.YOEDI. ROBEL.ROEW.ROEW.ROEM.ROEX.ROEZ.ROEM.ROEDE.YOEDI. ROBEL.ROEW.ROEW.ROEM.ROEX.ROEZ.ROEM.ROEDE.ROEDI. ROBEL.ROEM.ROEW.ROEM.ROEX.ROEZ.ROEM.ROEDE.ROEDI. ROBEL.ROEW.ROEW.ROEM.ROEM.ROEX.ROEZ.ROEM.ROEDE.ROEDI. ROBEL.ROEM.ROEM.ROEM.ROEM.ROEM.ROEM.ROEM.ROEM	THETALO, PSIAO, PHIAO, PCDO, VO, PC, RO, YAPPC, FHIO, PSIO, YO, LO, PRAL NO, VEBSO # FAL NO, VEBSO # FAL NO, VEBSO # TARRAY SECRENT 5 - INPUT FCRCES AND MCMENTS. # SUMFYO, SUMFO, SUMFY, DFY, SUMFZ, DFZ, SUMM, DM, R * CCMMON SUMFYO, SUMFY, DFY, SUMFZ, DFZ, SUMM, DM, R * CCMMON SUMFYO, SUMFY, DFY, SUMFY, DFY, SUMFZ, DFZ, SUMM, DM, R * CCMMON WEIGHT, G, IX, IY, IZ, IX, LM, WH, LITM, LS, LIDS RFAL G, IX, IY, IZ, IX, LM, MM, LITM, LS, LIDS * RAPRAY SEGMENT 7 - CONSTANTS. * CCMMON OMEGAL, PREGAM, ML, KW, KFRPM, KCCN, TAUCN, TAUCN, TAUCN, R * CCMMON OMEGAL, PREGAM, ML, KW, KFRPM, KCCN, TAUCN, TAUCN, R * MOEU, FORL, MCDA, KI, MCD, MCD, MCD, MCD, MCD, MCD, MCD, MCD	COMPON			50
#FAL MOSLOSON ### R ARRAY SEGMENT 5 - INPUT FURCES AND MCMENTS. ### R ARRAY SEGMENT 5 - INPUT FURCES AND MCMENTS. ### R ARRAY SEGMENT 5 - INPUT FURCES AND MCMENTS. ### R ARRAY SEGMENT 6 - GEDMETRY. #### R ARRAY SEGMENT 6 - GEDMETRY. #### R ARRAY SEGMENT 6 - GEDMETRY. #### R ARRAY SEGMENT 7 - CONSTANTS. #### GAIXAIYAIZAIXALMALTOMALSALTDS #### R ARRAY SEGMENT 7 - CONSTANTS. ###################################	### R ARRAY SECHENT 5 - INPUT FURCES AND MUMENTS. ### R ARRAY SECHENT 5 - INPUT FURCES AND MUMENTS. ### R ARRAY SECHENT 5 - INPUT FURCES AND MUMENTS. ### R APPAY SECHENT 6 - GEDMETKY. ### R APPAY SECHENT 6 - GEDMETKY. #### R APPAY SECHENT 6 - GEDMETKY. #### R APPAY SECHENT 7 - CONSTANTS. #### R APPAY SECHENT 7 - CONSTANTS. ###################################				21
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CCMMON WFIGHTS GIXPIY, IZPIXZPLM, LTDM, LTDS *** R APRAY SEGMENT 7 - CGNSTANTS. *** CCMMON OHEGAL, PHEGAL, NU, RW, RRPM, RCCN, TAUENG, TAUCON, TAUD, R R L ROLL, POEL, POEL, RDT, RDT, RDT, RDT, RDT, RDT, RDT, RDT	CCMMON WFIGHTS GIXPIY, IZPIXZPLM, LTDM, LT	0 1010000000000000000000000000000000000	* 6		3.0
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CCMMON OMEGAL, IMEGAW, NU, NW, NERPR, NCCN, TAUENG, TAUCON, TALD, NOEU, NCOEU, NC	CCMMON OMEGAL, PMEGAN, NU, NEW, NERPP, NCCN, TAUENG, TAUCON, TAUD, CCMMON OMEGAL, PMEGAN, NU, NEW, NERPP, NCCN, TAUENG, TAUCON, TAUD, NOEU, POEL, NOEU, NO	REAL			33
CCMMON OMEGAL, OMEGAN, NEW PROPERTORN, TALENG, TALCON, TALO, R KOEU, POEC, POEC, POET, NO ET, NO ET	CCMMCN OMEGAL, OPEGAN, N. S.	***************************************	• (34
CCMMON OMEGAL, PPEGAD, NU, NEW, NEWP, NCCN, TAUCON, TAUD, R NOEU, NOEU, NOEC, NOET, NOET, NOET, NOET, NOEV, NOED, NOED, NOEU, NOEC, NOET, NOTT,	CCMMON OMEGAL, IMEGAW, NEW PROPERSON, TALENG, TALCON, TALO, R LOEU, POEC, NOET, NOE	A APRAT SECTENT	~ ~		35
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DF 70 J=1,MCURVS REAGINLIST1.030) LEGEND, NDATA.NCCLX, MCDLY, ISYM, SCALEX, SCALEY FCRATI(4A10, 315, 2X,R1, 2X, 2E10, 3) IF(APPNT.GT.0) PRIFE(6, 2030) LEGEND, NDATA.NCDLY, NCOLY, ISYM, SCALEX, PRNPLT FCRMT(5X,4A10, 315, 2X,R1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(6X,P1, 5X, 4A10, 315, 2X, P1, 2X, 2E12, 5) FCRMT(7X,P1, P1, P1, P1, P1, P1, P1, P1, P1, P1,		אנשר שאת ברניו רבו אני	-	17.	60
PRINCE P				- Ida	98
FCRMAT(4A10-315-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R11-2X,R1	7 70	Sydnow-tell Co		TIGN	87
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TARROCT(10) TXV(6) TXV(6) TXCON(6) 15 27-48 -			4 - COVARIANCE PODT(17,17), GM 6 - STANDARD DE	- AIRWAKE	VYY(5,5,3) VYY(5,5,3) VZZ(5,5,3) SVXX(5,5,3) SVXX(5,5,3) SVZZ(5,5,3)		

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	TFMP4 = 4.*KITTLI/(TAUD+TAUA) TFMP5 = 81 - TLI/TAUA TFMP6 = 4.*K2*TL2/(TAUD+TAUA) TFMP7 - 82 - 4.*K2*TL2/(TAUD+TAUA)	4 0 0 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	25 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
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SUBROUTINE PROP	900	-74/74 - 0PT-1	FTN 4-6+428 12/08/78 15-13-13	•13 PAGE
5		CALL LAYIN(F,1,14,NFA,G1,6,4,0) CALL LAYIN(F,7,7,NPA,A,7,7,0) CALL LAYIN(F,14,1,NP4,C,4,6,0)	FROP 132 FROP 133	
2	.:	CALL LAYINF, 14, 14, NPA, PL, 4, 4, 0) GM MATRIX		9
	• •	CALL LAYINGER, 1, 1, NGP, R, 7, 4, 0)	PFCP 138 PFCP 139 PPCP 139	
8	:.	ON MATRIX		
			PROP 1144	
09	:	******** PROPAGATE COVARIANCE		313
\$		CALL MULTAGICM, NOM, NOM, GM, KGM, NOM, WK2) CALL MULTIGM, KGF, NOF, WK2, NOF, NGF, G2) IF (ICEES.EO.1.AND.NOINT.EO.0)		
e e		CALL ADDIR(PDCT, NPA) CALL ADDIR(PDCT, NPA) CALL ADDIR(PDCT, G2, PDCT, NPA, NGM) RETURN	PROP 154 PROP 156 PROP 156 PROP 157	

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	S	REDUTIN	SURROUTINE RUTATE		41.14	0PT-1					FTN 4.6+428	9+458	7	12/08/78	15.13.13		PAGE
	-			SURROUTI	NF RO	TATEON	INF ROTATE(X, YAANGAIT, YP, YR)	11, 38,	YR.			INF ROTATE(XrYsANGrIT;XP,YR)	1.	RCTATE	N m 4		
	•			TAPUT AR	TINE TO REUMENTS	S KCTA	RCTATE AND	TEANSE	OR* 10	ANGTHER	COORD	TINE TO KCTATE AND TEANSFORM TO ANGTHER COORDINATE SYSTEM RGUMENTS — X COORDINATE	£	RCTATE PCTATE ROTATE PCTATE			
	2		88888	9 L	111	ANGLE SWITCH 11 - N	Y CORDINATE ANGLE OF RCTATION SWITCH FOR CALCUL IT - NEGATIVE: N IT - ZERO!	TTION CAL	TRANSFO	Y CORDINATE ANGLE OF RCTATION SWITCH FOR CALCULATING TEANSFORMATION DELTAS IT — NEGATIVE: NO TRANSFORMATION IT — ZERD: CALCULATE TRANSFORMATION DEL	TION DI	NING TEANSFORMATION DELTAS NO TRANSFORMATION CALCULATE TRANSFORMATION DELTAS	•••••	PUTATE PUTATE ROTATE	112		
	2		-	DUTPUT A	ARGUMENTS - X C	. 88	CORDINATE A	AFTER AFTER	ROTATIC	AFTER ROTATION AND TRANSFORMATION AFTER ROTATION AND TRANSFORMATION	AS RANSFO RANSFO	PHATICN	• • • • • •	RCTATE RCTATE RCTATE RCTATE	1191181		
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	8	. 444	8	CONTINUE YR YR FETURN END	× × × × × × × × × × × × × × × × × × ×	NA KG	- X+COSANG - Y+SIMANG + DX - X+SIMANG + Y+COSANG + DY	+ SANG +	× >					ROTATE ROTATE ROTATE ROTATE	2 2 2 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		

14174 OPT-1

SUBROUTINE RUNGE

SUPPOUTINE PLNGE

ROUTINE TO PERFORM FOURTH OPOER RUNGE-KUTTA INTEGRATION.

REAL VARIABLES (PROBLEM DEPENCENT).

COPPON F (6)

2

INTEGRATION VARIABLES (LUCATIONS ARE PROBLEM DEPENDENT).

EQUIVALENCE (T1,R(1)), (T0,R(2)), (OT,R(3)), (OTCUT,R(4)), (CTGUT2,R(5)), (TMAX,R(5))

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I ARRAY SEGMENT 1 - INTEGER VAFIABLES.

COMMON/INTEGER/ICEES, NEOU, NSTATES, NPA, HOM, NGM, NPE, NPY, NOAW, NGINIT

I APPAY SEGMENT 4 - DERIVATIVE INDICES.

COMMUN/INTEGER/ INDXPD.INDXP, INDXPE, INDXPE, INDXPXD.INDXPX

I ARRAY SEGMENT 6 - VAPIOUS INDICES.

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I ARRAY SEGRENT 5 - STATE INDICES.

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COMPON/INTEGER/ INDX2(14)

CCMMOK/INTEGEP/ INDX1(14)

TEMPORARY INTEGRATION STORAGE. DIMENSION - NEOU - NSTATES + NPA++2 + NPX++2 + NPE++2

COMPLETE FIRST STAGE AT THIS INTEGRATION STEP.

· 0.16666666667*DT

COPPOR/INTFG/ RI(21E7), PT(2167)

. RICES + TEMPI+RCINOXICES

NSTATES + 1

CONTINUE

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- INDXP - .R(12)

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20 I-NL1, KU1

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- R(1N0X2(1))

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September 1

P ARRAY SEGNENT B - WIND, ALTITUDE, AIRSP COMPON ALT, VAIR-LUBS, VARBS, VERS, ALTOHA, VIDWA,	FIN 4.6+428 12/08/78 15-13-1		DUMZAVSAPSISAXIDUS, R DAPSIMODAPSISAPSISP, R AAPHIAASIGHAVA, R EANAURAUMHNOD, R ISSAPSISCAPSISTATSIAR SADYMZ45, ZGSP, R			~ ~ (P. ZFRPH, ZCON, ZPOIGV, R. E., P. NR,		ac ac 1	W. ETHETA. R	∝ ∝ •	D.DRID.DRZO R	TABLE LOOKUPS.	 LIDOP COMMAND TABLE L R	~ ~	~ ~	~ ~ .	GAINDR	~~ •	
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R ARRAY SEGMENTS 63-80 - OPTIMAL CONTROLLER GAINS

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UBROUTINE SOLVR	SOLVR 74/74	4 OPT=1 FTN 4.6+428	12/08/78	15.13.13
	. CALL MULTNA	CALL MULTHW(P,PHI,PSI,B)	SCLVR	29
	CALL MULTT	N(PHI, PSI, DELP, N)	SCLVR	09
3	CALCULATE FFI	CALCULATE WEN VALUE OF P.	SCLVR	61
	CALL ADDWN	CALL ADDINGPODELP, PAN)	SOLVR	62
•	CHECK FOR CONVERGENCE	NVFFGFNCE	SOLVR	63
	DC 42 K-15N		SCLVR	*9
	DC 42 L-K.F.	-	SOLVR	69
	IF(P(K,L).	IFIPIK, L).E0.0.0. AND. ABSIDELPIK, L)). GE.1.0E-07) 60 TO 43	SOLVR	99
	IF (P(K,L)	IF (P(K,L) .EQ. 0.0) 60 TC 42	SOLVR	67
	JF (ARS (DEL!	JF(ABSIDELP(K,L)/P(K,L)) .GE. 0.01) GO TO 43	SCLVP	89
	42 CUNTINUE		SOLVR	69
u	CONVERGENCE.	CONVERGENCE. RETURN TO CALLING PROGRAM.	SOLVR	70
	WRITE(6, 1002) LGOP	102) LGOP	SOLVR	11
1	1002 FCRMAT(/36)	FCRMATI/36H SOLVR CONVERGED ON ITERATION NUMBER,13,1H.1	SCLVR	72
	PFTURN		SPLVR	73
	43 CONTINUE		SOLVR	7.4
•	11	ITERATION HAS NOT CONVERGED.	SOLVR	75
	CALL MULTE	CALL MULTEN(PHI,PHI,DELP,N)	SOLVR	16
	00 44 I-1,N		SOLVR	11
	00 44 3-14		SOLVR	78
	44 PHI(1,1).	DELP(1,J)	SCLVR	62
	40 CONTINUE		SCLVR	08
•	:	ITERATION LOOP	SCLVR	18
	PRINT 1001		SOLVR	29
-	1001 FCPMAT(/63)	FCPMATI/63H SOLVR FAILED TO CONVERGE - P WILL BE RESET TO	RESET TO ORIGINAL SOLVP	83
	1 PATRIX.1		SOLVR	**
	E . Z . X		SOLVR	82
	00 46 1-16		SOLVR	98
	00 45 3-16		SOLVR	87
		IF(I.LT.K.OR.I.NE.J) P(I,J) . 0.0	SOLVR	88
45			SOLVR	80
94			SOLVR	06
	RETURN		SOLVR	7
	END		SOLVR	26

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APPENDIX C

LISTING FOR OPTIMAL CONTROLLER PILOT MODEL ONLY SUBROUTINES DEQU, MISCAL, PROP, AND SETUP ARE LISTED, THE OTHER ROUTINES ARE THE SAME AS THE CLASSICAL PILOT MODEL (APPENDIX B)

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74/74 OPT-1 FTN 4.6+428	SUBPOUTINE DEOU ************************************	R ARRAY SEGMENT 1 - INTEGRATION VARIARIES.	HE, TO, DTIME, DTOUT, DTOUTS,	COMMON UDGT. WOOT, KOOT, TCOT, XAPPROT, ZAPPONT, DFRPMD, XSPDOT, ZSPOOT, ZSPOOT, SPOOT	ARRAY SEGMENT 3 - STATE VAPIABLES.	COMMON UR, WB, OB, THETA, XAPP, ZAPP, DFRPM, XSP, TSP, THETAS R ARRAY SEGMENT 4 - REF. VALUES FOR LOCAL LINEARIZATION.	COMMON UG, WO, OO, THETAO, XAPPO, ZAPPO, XO, ZO, MG, UBASG, WBASO, WASOO, THETAAO, PSIAO, PHIAO, RCOO REAL MO	R ARPAY SEGMENT 5 - INPUT FORCES AND MOMENTS.	N SUMFXO, SUMFZO, SUPMO, SUMF	R APRAY SEGMENT 6 - GEOMETPY. COMMON WEIGHT, 6, IX, IX, IX, IX, IM, WM, LTOM, LS, LTOS	PEAL GAINAIYAIZAINZALMALTOMALSALTOS R ARRAY SEGMENT 7 - CONSTANTS.	COMMON DMEGAU, CMEGAW, KU, KW, KFRPM, KCDN, TAUENG, TAUCDN, TAUD, KDEU, KDEW, KOEG, KOET, KDEY, KDEZ, KDEN, KDEDE, KDFDT, KOTU, KOTU, KOTO, KOTTI, KOTT, KOTZ, KOTN, KOTOE, KOTOT KOTO, KOTOT KOEW, KFRPM, KCON, CON, KOEW, KDEW, KDEW, KDEW, KOEW, KO	R ARRAY SEGMENT 8 - WIND, ALTITUDE, AIRSPEED AND AIRWAKE.	COMMON ALTEVAIRE UBASEVBASE UBHAFBETAEPSIEPHIE VSEPSISE XIOUSE YIOMSEVAMBEPSIANSE XIONAE YIONAE ZIONAE VUIDE PSIMODEPSISSE PSISEDX45 DO VASE OTASE XMEYNE ZMEPSIAE THE TAREPHIAE SIGMAVXE SIGMAVYESIGMAVZEVXAME VVAME VZAMEUMINDE UMENEURE UMENEURE VANEURE VMENEVE VERMEVER VAMMENDENENEMEMEMEMENEENEMENEENEMESE PSISSEPSISSE TSSETSES TSSETSES TRIEDXENEMESE OVMIASSED VASSES	P ARRAY SEGMENT 9 - OPEN LOOP PARAMETERS. COMMON THETAC, OFRPMIL, OCONOL, OFPL, GAMMAGS, RANSE, VAIRC		Comment Control Contro
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. 52	C * UMIND * UMEAN + UAW UMIND * WFEAN + VAW C INITIALIZE INETIAL SPEEDS FROM AIRSPEEDS, ONE TIME ONLY. IF(ICEES.EO.1) UB * UBAS + UMIND IF(ICEES.EO.1) WB * WBAS + WWIND	0 6 0 C C C C C C C C C C C C C C C C C	25 6 6 6 6 8 8
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552	* MAAS - WEASO * SORT(URAS*UBAS + WEAS*WEAS) A * ATANZ(WEAS*UBAS)		22222
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	SURRDUTINE DEOU 74/74 OPT-1 FTN 4.6+428 08/08/78	C ** LONGITUDINAL POSITION ERROR. C * XAPCOM XSP - RC ERRX XAPPOOT - XAPCOM KAPPOOT - UR*COST + W8*SINT ERRXD ** XAPPOOT - XSPOOT + RCO	C +++ GLIDE SLOPE (POSITION AT COMMANDED RANGE) C + ZGSP = ZSP - (RC)+TAN(0.01745329+GAMMAGS)+ZRIASP C +++ VERTICAL POSITION ERPOR	IF (FLAG.FG.1 CR. TIME.GT.1 EPRZ. ZAPP - ZGSP ZAPPOCT - WB+COST - UB+SINT EPRZO. ZAPPOCT - ZSPOCT + (C *** ATTITUDE AND SPEED FRORS C * ETHETA THETA - THETAC COST * COS(THETA) SINT * SIN(THETA) ERRU * ERRXD * COST - ERRZD * SINT EPRW * ERRXD * SINT * ERRZD * COST	C *** PITCH CONTROL. C * DED* -KDEU*ERRU - KDEO*08 - KDET*ETHETA 1 - KDEX*ERRX - KDEZ*ERRZ - KDEN*DFRPM - KDEDE*DE - KDEDT*DT C * THRUST CONTROL.	DTD - KDT 1 - KDT	C + COMMANDED AIRSPEED (HACKED FOR REFERENCE DNLY) C + ROCOMRCD SINC - SIN(THETAC) COSTC - COS(THETAC) XNC - RDCOM + XSPDOT	LDC = XDC = XDC + LDS Y + CARPERGS) UASC = COSTC + XDC - SUTTC + XDC - WIND VAIRC = SORT (UASC + WASC + WASC + WASC + CAPPERGS) C + A REFRAME.	XAPPOOT = UB+COST + WB+SINT ZAPPOOT = WB+COST - UB+SINT DI = OFRPM + OFRPMCL
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	74/74 OPT=1 URROUTINE MISCAL(MPPNT) ************************************	SUCH AS TABBING, PUNCHING, ETC., ETC. INPUT ARGUMENTS NPRNT COVARIANCE MATRIX PRINT INDICATOR. O = DO NOT PRINT MATRIX ON OUTPUT FILE.	DIMFNSION CA(48) *** R ARRAY SEGMENT 1 - INTEGRATION VARIABLES. COMMON TIME, TC, DTIME, DTCUT, DTCUT2, TMAX *** R ARPAY SEGMENT 2 - DERIVATIVES.	COMMON UDDI, MDOT, DDOT, TOOT, XAPPDOT, ZAPPDOT, DFR *** R ARRAY SEGMENT 3 - STATE VARIABLES. *** COMMON UB, WB, QB, THETA, XAPP, ZAPP, DFRPM, XSP, ZSP, *** R ARRAY SEGMENT 4 - REF. VALUES FOR LOCAL	COMMON UO, VO, OO, THE A THETAAO, PSI REAL HO *** R ARRAY SEGMEN COMMON SUMFXO, SUMF	REAL G. IX. IY. IZ. REAL G. IX. IY. IZ. REAL G. IX. IY. IZ. COMMON OMEGAU. CHE COMMON OMEGAU. CHE COMMON COMEGAU. CHE COMMON COMEGAU. CHE COMMON COMM	COMMON ALTSVANDS VOND ALTITUDE AIRSPEED AND AIRWAKE. COMMON ALTSVAND VOND VOND VOND VOND VOND VOND VOND VO
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	R ARPAY SEGMENT 13 - SPEED TABLE FOR AERO TABLE LOUKUPS.
	COPMON TABVICAS
000	R APRAY SEGMENT 14 - SPEED TABLE FOR OPEN LOOP COMMAND TABLE LOOKUPS.
	COMPON TABVZ(10)
	R ARRAY SEGMENT 15 - FLIGHT ABOVE SHIP TABLE FOR EZ LOOKUP.
	COMMON TABEZP(7)
,,,	R ARRAY SEGMENT 16 - EZ TABLE.
	COMMON TABEZ(7)
	R ARRAY SEGMENT 17 - SHIP MOTION
	COMMON KXS,ZETAXS,WNXS,KZS,ZETAZS,WNZS,KTS,ZETATS,WNTS, KYS,ZETAYS,WNYS,KRS,ZETAPS,WNRS,KPS,ZETAPS,WNPS,TAUPRT RFAL KXS,KZS,KTS,KYS,KRS,KPS
	R ARRAY SEGMENTS 20-23 - OPEN LOOP COMMAND TABLES.
	COMPON TARTC(10) COMMON TRPHOL(10) COMMON TCONGL(10) COMMON TDEOL(10)
	R AFRAY SEGMENTS 24-25 - NOZZLE TABLES.
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	*** R ARPAY SEGMENT 107 - MORE OPTIMAL CONTROLLER GAINS (NOISE RELATED)	~ ~ ~
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	P ARRAY SEGMENTS 108-119	~ ~
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υ (COMMON/INTEGER/ INOXI(14)	
	. I ARRAY SEGMENT 5 - STATE INDICES.	
	COMMON/INTEGER/ INDX2(14)	. .
	I ARRAY SEGMENT 6 - VARIOUS INDICES.	
	COMMON/INTEGER/ INDXPD, INDXP, INDXPED, INDXPE, INDXPXO, INDXPX	5
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	*** R ARRAY SEGMENT 1 - INTEGRATION VAPIABLES.	v m v
	COMMON TIME, TO, DTINE, DTOUT, DTOUTZ, THAX	
	*** R ARRAY SEGMENT 2 - DERIVATIVES.	
	COMMON UCOTS LOOT . TOOT , XAPPOOT, ZAPPOOT, OFAPHO, KSPOOT.	
	*** R ARRAY SEGMENT 3 - STATE VARIABLES.	177
•	COMMON UB.WR. CB. THETA, XAPP, ZAPP, DFRPM, XSP, ZSP, THETAS	E 21
	*** R ARRAY SEGMENT 4 - REF. VALUES FOR LOCAL LINEARIZATION.	
. 62	COMMON UC. WO.OC. THETAD, YAPPO. ZAPPO. XO. ZO.MO. UBASO. WBASO. WASDO.	
	97	
	*** R ARRAY SEGMENT 5 - INPUT FORCES AND MOMEN'S.	22 8
	COPMON SUMFXO, SUMFZO, SUMPX, DFX, SUMFZ, DFZ, SUMM, DM	
	B ARRAY SEGMENT 6 - GEOMETRY.	782
	COMMON WEIGHT, G. IX. IV. IZ. IXZ. LM. WM. LTDM. LS. LTDS REAL G. IX. IY. IZ. IXZ. LM. LTDM. LS. LTDS	
,	** R ARRAY SEGMENT 7 - CONSTANTS.	310
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*	1 KOEU, KOEW, KOEO, KOET, KOEZ, KOEZ, KOEO, KOEOE, KOEOT, 2 KOTU, KOTW, KOTT, KOTX, KOTZ, KCTN, KOTOE, KOTOT	
	*** R ARRAY SEGMENT 8 - WIND, ALTITUDE, AIRSPEED AND AIRWAKE.	
	COMMON ALT, VAIR, URAS, VBAS, WAAS, ALPHA, BETA, PSI, PHI, V5, PSI5, X10WS, A Y10WS, VAMB, PSIAMP, X10WA, Y10WA, ZNOVA, VWOO, PSIWOO, PSI3, PSISP, B PSIS, DYES, DYES, DYES, VA. VM. ZN. DSIA, THETAL, DHIA, CICMANY	
	C SIGMAYY, SIGMAYZ, VYAM, VYAM, VZAM, UNIND, UFEAR, UR, UNANNIND, VMEAN, VYR, VAM, WAIND, WR, WAW, WNSF, PSISS, PSIST, TSI, TSZ, TSZ, TSZ, TSZ, TSZ, TSZ, TSZ, TSZ	
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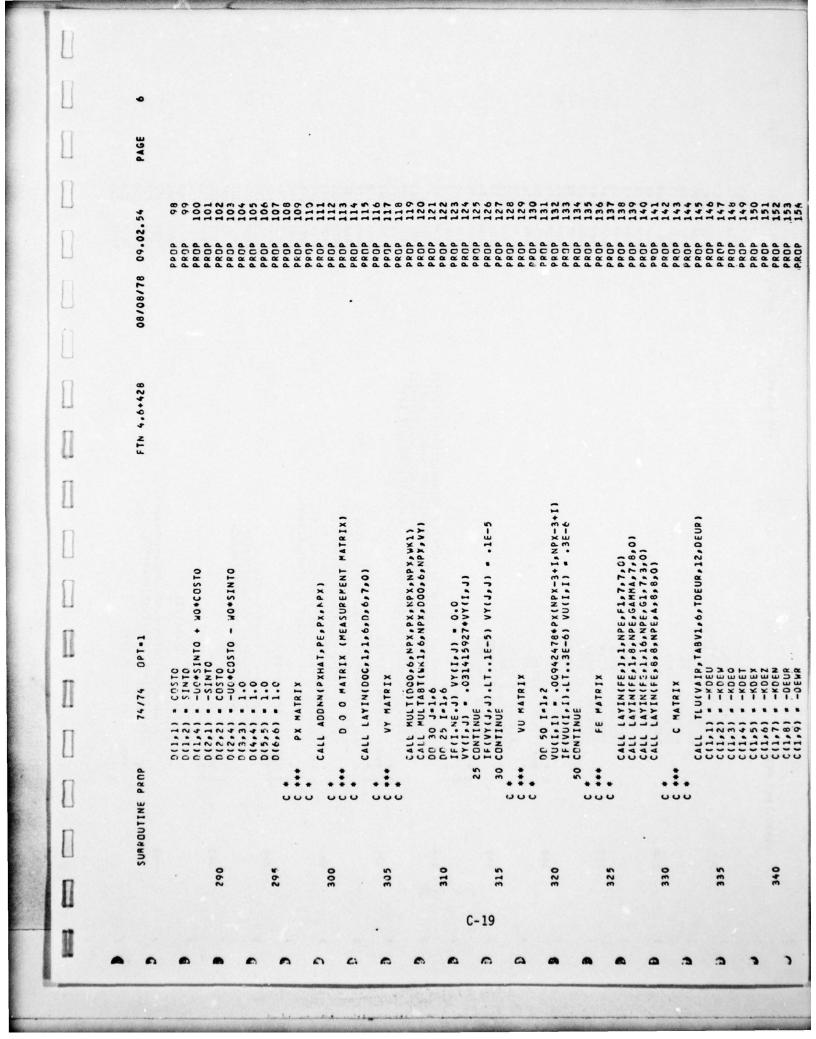
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APPENDIX D

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DESCRIBING FUNCTIONS OF

GENERAL SINGLE-VALUED NONLINEARITIES REPRESENTABLE

BY STRAIGHT-LINE SEGMENTS

APPENDIX D

DESCRIBING FUNCTIONS OF

GENERAL SINGLE-VALUED NONLINEAPITIES REPRESENTABLE BY STRAIGHT-LINE SEGMENTS

D.1 Decomposition Into Odd and Even Components

The general nonlinearity is represented by N straight-line segments. The number of segments in the odd component is also N, and there are also N segments in the even component.

Denoting the general nonlinearity by v = f(x): then the odd and even components are respectively given by

$$y_0(x) = 1/2 y(x) - y(-x)$$

$$y_E(x) = 1/2 y(x) + y(-x)$$

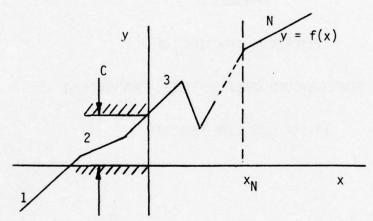


Figure D.1 General Nonlinearity Considered

Note that for x = 0 this gives $y_0(0) = 0$; $y_E(0) = y(0)$. It is convenient to separate out the offset C, as indicated by the following equations

$$y_0' = y_0(x) = f_0'(x)$$

$$y_{E}'(x) = y_{E}(x) - C = f_{E}'(x)$$

where C = y(0), as shown in Figure D.1.

We split the nonlinear characteristic as indicated in Figure D.2.

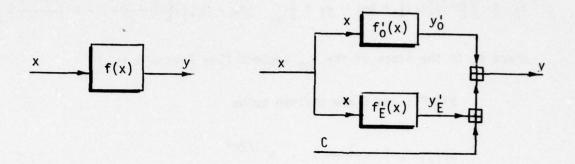


Figure D.2 Separation of the Nonlinearity Into Even, Odd, and Bias Components

D.2 Approximation to the Odd Component

The input is assumed to consist of a bias, B, plus a random Gaussian component of variance σ^2 , denoted by x_R . The general form of the odd component is shown in Figure A.5.3.

$$x(t) = B + x_R(t)$$

The best least-squares approximation to y_0 ' is

$$y_{OA}' = N_B B + N_R x_R(t)$$

where $N_{\rm B}$ and $N_{\rm R}$ are given by the expressions overleaf (from p. 579 of Reference D.1).

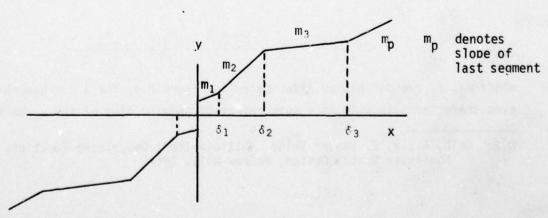


Figure D.3 General Piecewise-Linear Odd Memoryless Nonlinearity

$$N_{R} = 2\frac{D}{\sigma} PE(\frac{B}{\sigma}) + 2m_{p} - m_{1} + \sum_{i=1}^{p-1} (m_{i} - m_{i+1}) \left[PI(\frac{\delta_{i} + B}{\sigma}) + PI(\frac{\delta_{i} - B}{\sigma}) \right]$$

$$N_{B} = \frac{D}{B} \left[2PI\left(\frac{B}{\sigma}\right) - 1 \right] + 2m_{p} - m_{1} + \frac{\sigma}{B} \sum_{i=1}^{p-1} (m_{i} - m_{i+1}) \left[G\left(\frac{\delta_{i} + B}{\sigma}\right) - G\left(\frac{\delta_{i} - B}{\sigma}\right) \right]$$

where m_i is the slope of the i_{th} segment (See Figure D.3)

PF, PI; and G are defined below

$$PF(w) = (\frac{1}{2\pi}) \cdot e^{-1/2w^2}$$

$$PI(w) = \int_{-\infty}^{w} PF(\Omega) d\Omega$$

$$G(w) = wPI(w) + PF(w)$$

Note that D = 0, because we have separated out the bias C.

D.3 Approximation to the Even Component

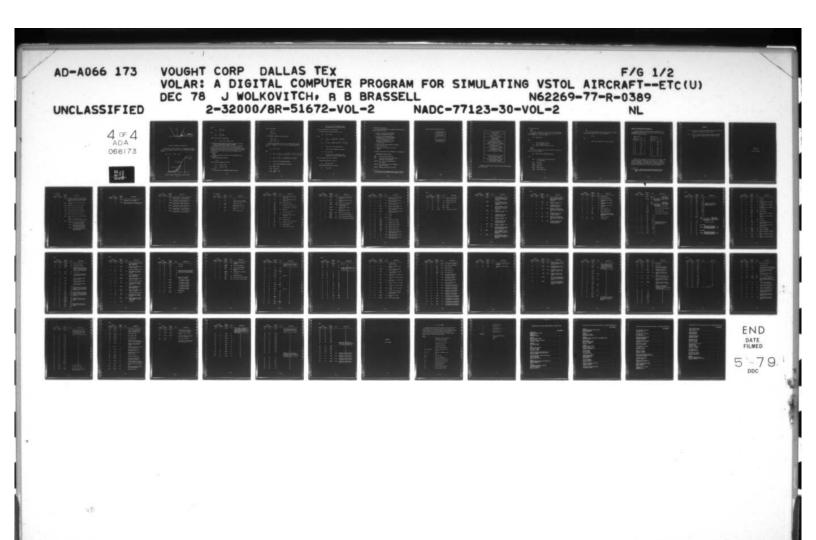
The best least-squares approximation to $y_{\rm E}'$ is obtained by subtracting two describing functions given on p 585 and 586 of Reference D.1. The results of subtracting describing function No. 55 from describing function No. 52 reduce to:

$$N_{R}(j) = m_{j} PI \left(\frac{\delta_{j} + B}{\sigma}\right) - m_{j} PI \left(\frac{\delta_{j} - B}{\sigma}\right)$$

$$N_{B}(j) = -2m_{j} \frac{\delta_{j}}{B} + m_{j} \frac{\sigma}{B} G(\frac{\delta_{j} + B}{\sigma}) + \frac{m_{j} \sigma}{B} G(\frac{\delta_{j} - B}{\sigma})$$

where m_j , δ_j are defined as illustrated in Figure D.4, for a non-general even characteristic with only one breakpoint on each side of the v_F axis.

D.1. Gelb, A., W. E. Vander Velde, Multiple-Input Describing Functions and Nonlinear System Design, McGraw-Hill, 1968.





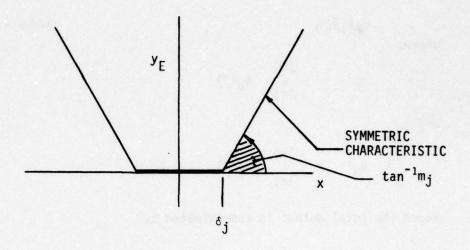


Figure D.4 Non-General Even Characteristic

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In Figure D.4 δ_j is the only breakpoint. For the <u>general</u> even component there will be Q breakpoints as shown in Figure A.5, hence the overall approximation is:

$$y_{0A}' = N_{B}' \cdot B + N_{R}' \cdot x_{R}(t)$$
 y_{E}
 $m_{1} + m_{2} + m_{3}$
 $m_{2} + m_{1}$
 $m_{3} + m_{4}$
 $m_{5} + m_{2}$
 $m_{1} + m_{2} + m_{3}$
 $m_{2} + m_{3}$
 $m_{3} + m_{4}$
 $m_{4} + m_{5} + m_{5}$
 $m_{5} + m_{5}$
 $m_{5} + m_{5}$
 $m_{5} + m_{5}$

Figure D.5 General Even Characteristic with Zero Offset

where:

$$N_{R}' = \sum_{J=1}^{j=Q} N_{R}(j)$$

and

$$N_B' = \sum_{j=1}^{j=Q} N_B(j)$$

Hence the total output is approximated by:

$$y_A = B (N_B' + N_B) + x_R(t)(N_R' + N_R) + C$$

D.4 Routines for Computing Describing Functions of General Single-Valued Nonlinearities Represented by Straight-Line Segments

Three FORTRAN routines, TABRD, DESCRIB and ERF provide a capability for generating describing functions for general single-valued nonlinearities which can be expressed as functions of as many as three independent variables.* One COMMON block is required to transfer data between routines. The procedures for invoking the proper routines and initializing the COMMON block are described below.

Method

For ease of reference the key formulas of the preceding section are repeated below.

Denoting the general nonlinearity by

$$Y = F(X)$$

then the odd and even components are given by

$$Y_0(X) = 1/2(Y(X) - Y(X))$$

$$Y_e(X) = 1/2(Y(X) + Y(-X))$$

^{*}For VOLAR purposes only one independent variable is assumed.

for X = 0, this yields

$$Y_{\alpha}(0) = Y(0)$$

It is convenient to separate out the offset yielding

$$Y_0(X) = Y_0(X)$$

$$Y_0(X) = Y_0(X) - Y(0)$$

Assuming the input consists of a bias, B, and a random Gaussian component of variance σ^2 , denoted by X_r , the best linear least squares approximation to y_0' is:

$$Y_{o_a}^{\prime} = N_b B + N_r X_r(t)$$

where:

$$N_b = 2M_p - M_1 + \frac{\sigma}{B} \sum_{i=1}^{P-1} (M_i - M_{i+1}) \left[G(\frac{\delta_i + B}{\sigma}) - G(\frac{\delta_i + B}{\sigma}) - G(\frac{\delta_i - B}{\sigma}) \right]$$

$$N_r = 2M_p - M_1 + \sum_{i=1}^{P-1} (M_i - M_{i+1}) \left[PI(\frac{\delta_i + B}{\sigma}) + PI(\frac{\delta_i - B}{\sigma}) \right]$$

$$G(W) = WPI(W) + PF(W)$$

$$PI(W) = -\frac{W}{\infty} PF(\Omega) d\Omega$$

$$PF(W) = \frac{1}{\sqrt{2\pi}} e^{-\frac{1}{2}W^2}$$

δ_i = Max value of the first independent variable associated with the ith odd component segment

NOTE: Only segments where $\delta_i > 0$ are considered.

The best linear least squares approximation to Y_e' is:

$$Y_{ea}^{\prime} = N_{b}^{\prime} B + N_{r}^{\prime} X_{r}(t)$$

where:

$$N'_{r} = \sum_{i=1}^{P-1} (M_{i+1} - M_{i}) \left[PI(\frac{\delta_{i} + B}{\sigma}) - PI(\frac{\delta_{i} - B}{\sigma}) \right]$$

$$N_b' = \prod_{i=1}^{P-1} (M_{i+1} - M_i) \left[\frac{-2\delta_i}{B} + \frac{\sigma}{B} (G(\frac{\delta_i + B}{\sigma}) + G(\frac{\delta_i - B}{\sigma})) \right]$$

 M_i = Slope of the ith even component segment

P = Index of last even component linear segment

G, PI, PF as defined above

δ_i = Min value of the first independent variable associated with the ith even component segment

NOTE: Only segments where $\delta_{i} \ge 0$ are considered.

The approximated output bias is given by

$$\overline{Y}_a = B(N_b + N_b') + Y(0)$$

The approximated output variance is given by

$$\sigma_a^2 = \sigma^2 (N_r + N_r^i)^2$$

D.5 Common Block Initialization

It can be seen from the discussion on methodology above that the data that must be preserved includes:

- (1) Values of the second and third independent variables for interpolation purposes.*
- (2) A subset of the first indepent variable. When generating the even and odd components of the nonlinearity, the x values are symetrically disposed around x = 0. Once generated, only the disposed values of x ≥ 0 need be kept.
- (3) Slopes of the even and odd components corresponding to the stored values of x.
- (4) The offset that was separated out of the even components.

The method of data storage within the COMMON block is discussed below.

COMMON/GDF/NTABLE, INDEX(m), TABLE(n)

NTABLE - Number of tables that were read.

INDEX - Array holding pointers into TABLE (must be dimensioned at least 3*NTABLE+1).

INDEX(3*(I-1)+1) - Index into TABLE where data for table I begins.

INDEX(3*(I-1)+2) - Number of values of 2nd independent variables in table I.

INDEX(3*I) - Number of saved values of x in table I.

^{*}For VOLAR purposes only one independent variable is used. Zeros were input in the table for the second and third independent variables.

TABLE is arranged in the following manner:

DATA FOR TABLE 1

DATA FOR TABLE 2

O

DATA FOR TABLE N

	X3 VALUE (1 ENTRY)
	X ₂ VALUES (INDEX(3*(I-1)+2) ENTRIES)
	SAVED X ₁ VALUES (INDEX(3*I) ENTRIES)
	OFFSET SEPAPATED FROM EVEN NENTS (INDEX(3*(I-1)+2) ENTRIES)
lst	ODD COMPONENT SLOPES FOR Y VALUE(INDEX(3*I)-1 ENTRIES)
1st	EVEN COMPONENT SLOPES FOR Y VALUE(INDEX(3*I)-1 ENTRIES)
	c 0
	SLOPES FOR INDEX(3*(1-1)+2) th VALUE (INDEX(3*I)-1 ENTRIES)
	SLOPES FOR INDEX(3*(I-1)+2) th VALUE(INDEX(3*I)-1 ENTRIES)

Contract of the last

TABLE must be dimensioned large enough to hold required data generated from all input tables.

D.6 Routine Description

TABRD

This routine is responsible for calculating the even and odd components of the nonlinearity, calculating the component slopes and storing the data into the COMMON block. The calling statement is:

CALL TABRD(X,Y,NPTS)

where:

Array of independent variables.

Y - Array of dependent variables.

NPTS - Number of elements in the X and Y arrays.

DESCRIB

This routine is responsible for calculating elements of the describing function. The calling statement is:

CALL DESCRIB(ITAB, BIAS, SIGMA, ØBIAS, ØVAR, REPRØ)

where:

ITAB = Table number for which describing function
 is to be generated.

BIAS = Input BIAS.

SIGMA = Input SIGMA.

ØBIAS = Output BIAS.

ØVAR = Output variance.

REPRØ = Gain on output sigma.

ERF

This is an internal FUNCTION subroutine to evaluate the error function associated with the normal curve. The calling sequence is:

X = ERF(Y)

where:

Y = Upper limit of integration for the error function.

EXAMPLE: AV-8A NONLINEARITY FROM REFERENCE D.2

For checkout purposes, a describing function was generated for the $\underline{\text{CM vs ALPHA}}$ nonlinearity with DH = 6 deg, $VJ/V\emptyset$ = 5.4 and a 15 deg. nozzle. The following data were considered.

NOZZLE = 0 deg

CM
14
165
190
24
27
32
0.39

NOZZLE = 30 deg

ALPHA	(DEG)	СМ	
-5		055	
0		024	
5		03	
8		034	
10		038	
12		042	
15		036	
20		018	

The input, ALPHA, consisted of a bias of 10 deg. and a variance of 1 deg. The describing function yielded a mean for the output, CM, of -.139988 and a variance of 0.000052097. An alternate method of inputting 1000 Gaussian-distributed random numbers with a mean of 10 and a variance of 1 was checked yielding an output mean for CM of -.14 and a variance of 0.00005279.

D.2. Nave, R. L., "Progress Toward a Computerized VSTOL/Small Platform Landing Dynamics Investigation Model," NADC Report 77024-30, 1977.

REFERENCES

- D.1. Gelb, A., and W. E. Vander Velde, Multiple-Input Describing Functions and Nonlinear System Design, McGraw-Hill, 1968.
- D.2. Nave, R. L., "Progress Toward a Computerized VSTOL/Small Platform Landing Dynamics Investigation Model," NADC Report 77024-30, 1977.

APPENDIX E

THE I AND R ARRAYS

E.1 The I Array

I A	IRRAY	VARIABLE	DESCRIPTION			
SEGMENT	ELEMENT	NAME				
1	1	ICEES	An internal 'flag' to keep track of what stage the integration is in and to identify the very first pass through the program (ICEES = 1).			
1	2	NEQU	Total number of differential equations to integrate.			
1	3	NSTATES	Number of mean equations to integrate.			
1	4	NPA	Order of the P matrix (NPA by NPA).			
1	5	NQM	Order of the QM matrix (NQM by NQM).			
1	6	NGM	Row dimension of GM matrix (NGM by NQM).			
1	7	NPE	Order of the PE matrix (NPE by NPE).			
1	8	NPX	Order of the PXHAT matrix (NPX by NPX).			
1	9	NØAW	User specified control of airwake calculations. NØAW = 0, calculate airwake NØAW = 1, no airwake calculations desired			
1	10	NØINIT	User specified control of program flow NØINIT = -1, fix means and integrate covariance matrices only NØINIT = 0, call SOLVR to calculate steady state value of P at the conditions defined by means NØINIT = 1, no special initialization calculations desired - run a normal time history			

I A	I ARRAY		DESCRIPTION		
SEGMENT	ELEMENT	NAME	DESCRIPTION		
4	1-14	INDX1	R array locations of elements to be integrated. Setup by Option 6.		
5	1-14	INDX2	R array locations of elements that are the outputs of integrators. Setup by Option 6.		

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SEG	I MENT	ARRAY ELEMENT	VARIABLE NAME	DESCRIPTION		
	6	1	CAXONI	R array location of the first element of the PDØT matrix. Setup by Option 6.		
	6	2	INDXP	R array location of the first element of the P matrix. Setup by Option 6.		
	6	3	INDXPED	R array location of the first element of the PED matrix. Setup by Option 6.		
	6	4	INDXPE	R array location of the first element of the PE matrix. Setup by Option 6.		
	6	5	INDXPXD	R array location of the first element of the PXHATD matrix. Setup by Option 6.		
	6	6	INDXPX	R array location of the first element of the PXHAT matrix. Setup by Option 6.		

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E.2 The R	Array RRAY	VARIABLE			
SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION	
1	1	TIME	t	Time	
1	2	ТО	t	Initial time; time for which reference values are defined	
1	3	DTIME	t	Integration interval	
1	4	DTØUT	t	Output file written every DTØUT seconds	
1	5	DTØUT2	t	Print interval for MISCAL output	
1	6	TMAX	t	Upper integration limit	

R SEGMENT	ARRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
3	1	UB	1/t	Inertial speed along airplane X body axis
3	2	WB	1/t	Inertia! speed along airplane Z body axis
3	3	QB	rad/t	Airplane pitch rate
3	4	THETA	rad	Airplane pitch attitude
3	5	XAPP	1	Firplane position, X earth axis
3	6	ZAPP	1	Airplane position, Z earth axis
3	7	DFRPM	rpm	Engine rpm
, 3	8	XSP	1	Ship position, X earth axis
3	9	THETAS	rad	Ship pitch attitude
3	10	VB	1/t	Inertial speed along airplane Y body axis
3	11	PB	rad/t	Airplane roll rate
3	12	RB	rad/t	Airplane yaw rate
3	13	YAPP	1	Airplane position, Y earth axis
3	14	PH1	rad	Airplane roll attitude
3	15	PSI	rad	Airplane heading
3	16	YSP	1	Ship position, Y earth axis

R A	R ARRAY		EACT E	PARE 1	
SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION	
2	1	UDØT	1/t ²	Airplane acceleration along X body axis	
2	2	WDØT	1/t ²	Airplane acceleration along Z body axis	
2	3	QDØT	rad/t ²	Airplane pitch acceleration	
2	4	TDØT	rad/t	Airplane pitch attitude rate-of-change	
2	5	XAPPDØT	1/t	Airplane velocity along X earth axis	
2	6	ZAPPDØT	1/t	Airplane velocity along Z earth axis	
2	7	DFRPMD	rpm/t	Engine rpm rate-of-change	
2	8	XSPDØT	1/t	Ship velocity along X earth axis	
2	9	ZSPDØT	1/t	Ship velocity along Z earth axis	
2	10	TSPDØT	rad/t	Ship pitch attitude rate-of-change	

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R AI SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
4	1	UO	1/t	Reference value of UB used for local linearization
4	2	₩O	1/t	Reference value of WB used for local linearization
4	3	QO	rad/t	Reference value of QB used for local linearization
4	4	THETAO	rad	Reference value of THETA used for local linearization
4 2001	5	XAPPO	1	Reference value of XAPP used for local linearization
4	6	ZAPPO	1	Reference value of ZAPP used for local linearization
4	7	ХО	1/t ²	ΣF _X /mass
4	8	ZO	1/t ²	ΣF _Z /mass
4	9	МО	rad/t ²	ΣMy/Iy
4	10	UBAS0	1/t	Reference value of UBAS
4	11	WBASO	1/t	Reference value of VBAS
4	12	WASDO	1/t²	Reference value of WASD
4	13	THETAAO	rad	Reference value of THETAA
4	14	PSIAO	rad	Reference value of PSIA
4	15	PHIAO	rad	Reference value of PHIA
4	16	RCDO	1/t	Reference value of RCD
4	17	ov	1/t	Reference value of VB used for local linearization
4	18	PO	rad/t	Reference value of PB used for local linearization
4	19	ко	rad/t	Reference value of RB used for local linearization

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R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
4	20	YAPPO	1	Reference value of YAPP
4	21	PHIO	rad	Reference value of PHI
4	22	P\$10	rad	Reference value of PSI
4	23	YO	1/t ²	EF _y /mass
4	24	LO	rad/t^2	ΣM'/I _X
4	25	NO	rad/t^2	ΣM'Z/IZ
4	26	VBAS0	1/t	Reference value of VBAS

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R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
5	er es 1	SUMFXO	f	Initial summation of forces along the airplane body axis. Required input if means are propagated.
5	2	SUMFZ0	f	Initial summation of forces along the airplane body axis. Required input if means are propagated.
5	3	SUMMO	fl	Initial summation of moments about the airplane body axis. Required input if means are propagated.
5	4	SUMFX	1/t ²	Summation of 'forces' along airplane X body axis.
5	5	DFX	1/t ²	Incremental 'force' due to airplane departure from reference trajectory.
5	6	SUMFZ	1/t ²	Summation of 'forces' along airplane Z body axis.
5	7	DFZ	1/t ²	Incremental 'force' due to airplane departure from reference trajectory.
5	8	SUMM	rad/t ²	Summation of 'moments' about airplane Y body axis.
5	9	DM	rad/t ²	Incremental pitching 'moment' due to airplane departure from reference trajectory.
5	10	SUMFY0	f	Initial summation of forces along the airplane Y body axis. Required input if means are propagated.
5	11	SUMLO	fl	Initial summation of moments about the airplane X body axis. Required input if means are propagated.

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R AR SEGMENT	RAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
5	12	SUMNO	fl	Initial summation of moments about the airplane Z body axis. Required input if means are propagated.
5	13	SUMFY	1/t ²	Summation of 'forces' along airplane Y body axis.
5	14	DFY	1/t ²	Incremental 'force' due to airplane departure from reference trajectory.
5	15	SUML	rad/t ²	Summation of 'moments' that produce angular acceleration only about the airplane X body axis.
5	16	DL	rad/t ²	Incremental 'moment' due to airplane departure from reference trajectory.
5	17	SUMN	rad/t ²	Summation of 'moments' that produce angular acceleration only about the airplane Z body axis.
5	18	DN	rad/t ²	Incremental 'moment' due to airplane departure from reference trajectory.

R ARRAY		VARIABLE UNITS	DESCRIPTION		
SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION	
6	1	WEIGHT	ml/t2	Airplane weight	
6	2	G	1/t ²	Gravitational constant	
6	3	IX	m12	Airplane body axis inertia component	
6	rigger (4 Fr.) Eleka ybog	IY	ml ²	Airplane body axis inertia component	
6	5	IZ	m12	Airplane body axis inertia component	
6	6	IXZ	m12	Product of inertia	
6	7	LM	1	Overall length of ship	
6	8	WM	1	Maximum beam of ship	
6	9	LTDM	1	Distance from bow to landing pad center measured along ship centerline	
6	10	LS	1	Scaled ship length	
6	11	LTDS	1	A scaled LTDM	

1	R A	R ARRAY		UNITS	DESCRIPTION
П	SEGMENT	ELEMENT	NAME	01113	DESCRIPTION
Ц	7	1	ØMEGAU	WHITE	DRYDEN TURBU-
	7	2	ØMEGAW	NOISE	KU PLANE X BODY AXIS S + ØMEGAU
	7	3	KU	WHITE	DRYDEN TURBU-
	7	4	KW	NOISE	LENCE ALONG AIR- PLANE Z BODY AXIS
n	7	5	KFRPM		Gain on input to engine model
U	7	6	KCDN		Gain on input to nozzle actuator
П	7	7	TAUENG	t	Engine time constant
П	7	8	TAUCDN	t	Nozzle actuator time constant
	7	9	TAUD	t	Nozzle actuator time constant
П	7	10	KDEU	1/1	
Ц	7	11	KDEW	1/1	
n	7	12	KDEQ	1/rad	
L	7	13	KDET	1 t rad	Longitudinal optimal pilot
	7	14	KDEX	$\frac{1}{t}$	feedback gains on states into pitch control
Π	7	15	KDEZ	1 t 1	
П	7	16	KDEN	1 t rpm	
D	7	17	KDEDE	$\frac{1}{t}$	18
0	7	18	KDEDT	1 t	
O				ر	

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R ARRAY		VARIABLE	UNITO	DECOMPTION		
SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION		
7	19	KDTU	1/1			
7	20	KDTW	1/1			
7	21	KDTQ	1/rad			
7	22	KDTT	1 t rad	Longitudinal optimal pilot feedback gains on states		
7	23	KDTX	$\frac{1}{t}$	into thrust control		
7	24	KDTZ	1 t 1	54		
7	25	KDTN	1 t rpm	80		
7	26	KDTDE	$\frac{1}{t}$			
7	27	KDTDT	1/t			
7	28	ØMEGAV	WHITE NOISE	DRYDEN TURBU- LENCE ALONG AIR-		
7	29	κV		S + ØMEGAV PLANE Y BODY AXIS		
7	30	TAUA	t	Actuator time constant		
7	31	K1	DOLL CONT			
7	32	K2	ROLL CONT			
7	33	KY	ERPHI	K1(TL1*S+B1)(-S+2/TAUD) (TAU*S+1)(S+2/TAUD) DAP		
7	34	B1				
7	35	B2	YAW CONTR	OL:		
7	36	TL1	ERPSI	K2(TL2*S+B2)(-S+2/TAUD) (TAU*S+1)(S+2/TAUD) DRP		
7	37	TL2				

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	R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
4	8	1	ALT	1	Altitude
Ц	8	2	VAIR	1/t	Airspeed
]	8	3	UBAS	1/t	Airplane X body axis component of airspeed
	8	4	VBAS	1/t	Airplane Y body axis component of airspeed
Â	8	5	WBAS	1/t	Airplane Z body axis component of airspeed
	8	6	ALPHA	rad	Angle-of-attack
	8	7	BETA	rad	Sideslip angle
8	8	8	DUM1		Dummy variable, this location unused
	8	9	DUM2		Dummy variable, this location unused
_	8	10	V5	1/t	Ship speed
	8	11	PSI5	rad	Ship heading
	8	12	X1DWS	1/t	Earth axis component of ship's relative wind
1	8	13	Y1DWS	1/t	Earth axis component of ship's relative wind
	8	14	VAMB	1/t	Ambient wind speed
	8	15	PSIAMB	rad	Ambient wind heading
П	8	16	X1DWA	1/t	Earth axis component of ambient wind
	8	17	Y1DWA	1/t	Earth axis component of ambient wind
	8	18	Z1DWA	1/t	Earth axis component of ambient wind

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R ARRAY		VARIABLE	UNITE	DECOMPTION	
SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION	
8	19	VWØD	1/t	Wind-over-deck speed	
8	20	PSIWOD	rad	Wind-over-deck heading	
8	21	PSI3	rad	Orientation of ship wing axis; angle of rotation about the Z earth axis to point ship X wind axis into the wind-over-deck	
8	22	PSISP	rad	= PSI3 - PSI5	
8	23	PSIS	rad	= -PSIP; this is the angle ψ_{SS} in the airwake math model of Reference 12	
8	24	DX45	1	Earth axis distance between airplane and ship	
8	25	DY 45	1	Earth axis distance between airplane and ship	
8	26	DZ45	1	Earth axis distance between airplane and ship	
8	27	XM	1]		
8	28	YM	1 >	Airplane position in space with respect to the ship wind axis system (i.e., the airwake model	
8	29	ZM	1]	reference point)	
8	30	PSIA	rad	Euler type angles relating the	
8	31	THETAA	rad	airplane to the ship wind axis system. It is assumed that the	
8	32	PHIA	rad	ship wind axis does not pitch and/or roll.	
8	33	SIGMAVX	1/t]		
8	34	SIGMAVY	1/t >	Standard deviations of the airwake in the ship wind axis	
8	35	SIGMAVZ	1/t	system	
8	36	VXAW	1/t]		
8	37	VYAW	1/t >	Mean components of the ship airwake in the ship wind axis	
8	38	VZAW	1/t]	system	

	R ARRAY		VARIABLE	LINITE	DECEDITION
	SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION
	8	39	UWIND	1/t	Total wind component along air plane X body axis; UWIND = UMEAN + UAW
	8	40	UMEAN	1/t	Ambient wind component along airplane X body axis
	8	41	UR		Random wind component; unused
	8	42	UAW	1/t	Mean component of airwake disturbance along airplane X body axis
]	8	43	VWIND	1/t	Total wind component along airplane Y body axis; VWIND = VMEAN + VAW
	8	44	VMEAN	1/t	Ambient wind component along airplane Y body axis
1	8	45	VR		Random wind component; unused
]	8	46	VAW	1/t	Mean component of airwake disturbance along airplane Y body axis
]	8	47	WWIND	1/t	Total wind component along airplane Z body axis; WWIND = WMEAN + WAW
I	8	48	WMEAN	1/t	Ambient wind component along airplane Z body axis
1	8	49	WR		Random wind component; unused
	8	50	WAW	1/t	Mean component of airwake disturbance along airplane Z body axis
]	8	51	WNSF	rad/t	Natural frequency of second order shaping filter used in airwake model
	8	52	PSISS		sin (PSIS)

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R ARRAY		VARIABLE	UNITS	DECCRIPTION
SEGMENT	ELEMENT	NAME	ONTIS	DESCRIPTION
8	53	PSISC		cos (PSIS)
8	54	PSIST		tan (PSIS)
8	55	TS1	1	
8	56	TS2		Temporary storage for preliminary
8	57	TS3		calculations involving wind-over- deck and airwake shaping functions
8	58	TS4		
8	59	TS5	153	
8	60	TR1)	Scale factor on SIGMAVX, SIGMAVY, and SIGMAVZ
8	61	DXM145		= cos (PSISP)* cox (PSI5) - sin (PSIP)* sin (PSI5)
8	62	DXM245		= cos (PSIP)* sin (PSI5) + sin (PSIP)* cos (PSI5)
8	63	DYM145		= -sin (PSIP)* cos (PSI5) - cox (PSIP)* sin (PSI5)
8	64	DYM245		= cos (PSIP)* cos (PSI5) - sin (PSIP)* sin (PSI5)
8	65	ZGSP	1	Commanded ZA/P
8	66	ZBIASP	1	Bias term

R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
9	1	THETAC	rad	Commanded airplane pitch attitude
9	2	DFRPMØL	rpm	Open loop rpm command
9	3	DCDNØL	rad	Open loop nozzle command
9	4	DEØL	units	Open loop pitch control command
9	5	GAMMAGS	deg	Commanded glide slope angle
9	6	RANGE	1	∆ X's - XA/P
9	7	VAIRC	1/t	Commanded airspeed
9	8	DAØL	units	Open loop roll control command
9	9	DRØL	units	Open loop yaw control command

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R A	ARRAY	RAY VARIABLE	UNITC	DESCRIPTION		
SEGMENT	ELEMENT	NAME .	UNITS	DE.S	CRIPTION	
10	1	XU	1/t	Airplane longi derivatives; re look up	tudinal dimensional esults of table	
10	2	XM	1/t	160.32		
10	3	XO	1/t			
10	4	XFRPM	t ² *rpm		4	
10	5	XCDN	$\frac{1}{t^2}$			
10	6	XPDIGV		Not used	9	
10	7	XDE	1/t²		F	
10	8	7.U	1/t			
10	9	ZW	1/t			
10	10	ZQ	1/t			
10	11	ZFRPM	$\frac{1}{t^{2*}rpm}$			
10	12	ZCDN	$\frac{1}{t^2}$			
10	13	ZPDIGV		Not used		
10	14	ZDE	1/t ²			
10	15	MU	1 t			
10	16	MW	1 1 t			
10	17	MWDØT	1			
10	18	MQ	$\frac{1}{t}$			
10	19	MFRPM	$\frac{1}{t^2 * rpm}$			
10	20	MCDN	$\frac{1}{t^2}$		1	

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R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
10	21	MPDIGV		Not used
10	22	MDE	1/t ²	
10	23	YV	1/t	Airplane lateral/directional dimensional derivatives; results of table look up
10	24	ΥP	1/t	
10	25	YR	1/t	
10	26	YCA	1/t²	
10	27	YDR	1/t	
10	28	LV	$\frac{1}{1 t}$	T T
10	29	LP	$\frac{1}{t}$	
10	30	LR	1/t	
10	31	LDA	rad t ²	
10	32	LDR	rad t ²	
10	33	NV	1 1 t	
10	34	NP	$\frac{1}{t}$	
10	35	NR	$\frac{1}{t}$	
10	36	NDA	rad t ²	
10	37	NDR	rad t ²	

R ARRAY		VARIABLE	* Alexandra	
SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION
11	1 0 10	RC	18.12.08	Commanded range;
				range ≜ X's - X'A/P
11	2	RCD	1/t	Commanded range time rate-of- change
11	3	XAPCØM	1	Airplane commanded position along X earth axis
11	4	ERRX	1	= XA/p - XAPCOM; longitudinal position error
11	5	ERRU	1/t	Airplane body axis component of error rate
11	6	ERRZ	1	= Z _{A/P} - ZGSP; vertical position error
11	7	EKRW	1/t	Airplane body axis component of error rate
11	8	ETHETA	rad	= THETA - THETAC; pitch altitude error
11	9	ERY	1	= YCØM - YA/P; lateral position error
11	10	ERPHI	rad	= PHICØM - PHI; roll altitude error
11	11	ERPSI	rad	= PSICOM - PSI; heading error
11	12	YCØM	1,58	Airplane commanded Y earth axis position
11	13	PHI CØM	rad	Airplane roll altitude command
11	14	PSICOM	rad	Airplane heading command

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R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
12	1	DE	units	Pitch control displacement
12	2	DT	units	Thrust control displacement
12	3	DCDN	rad	Nozzle position
12	4	DED	1/t	Pitch control rate
12	5	DTD	1/t	Thrust control rate
12	6	DCDND	rad/t	Nozzle angle rate
12	7	DA	units	Roll control displacement limited output value
12	8	DR	units	Yaw control displacement limited output value
12	9	D,4P	units	Roll control displacement, input to limiter
12	10	DRP	units	Yaw control displacement, input to limiter
12	11	DA1	units	Intermediate variable used in calculation of roll control
12	12	DA2	units	Intermediate variable used in calculation of roll control
12	13	DR1	units	Intermediate variable used in calculation of yaw control
12	14	DR2	units	Intermediate variable used in calculation of yaw control
12	15	DA1D	1/t	Intermediate rate variable use in calculation of roll control
12	16	DA2D	1/t	Intermediate rate variable use in calculation of roll control
12	17	DR1D	1/t	Intermediate rate variable use in calculation of yaw control
12	18	DR2D	1/t	Intermediate rate variable use in calculation of yaw control

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R ARRAY		VARIABLE	UNITS	DESCRIPTION	
SEGMENT	ELEMENT	NAME	UN113	DESCRIPTION	
13	1-6	TABV1	1/t	Independent variable table of airspeeds	
14	1-10	TABV2	t	Independent variable table of	

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R	R ARRAY		VARIABLE UNITS	DESCRIPTION
SEGMENT	ELEMENT	NAME	UNITS	DESCRIP: TON
16	1	SIGDAP	units	Standard deviation of roll control displacement at input to limiter
16	2	SIGDRP	units	Standard deviation of yaw control displacement at input to limiter
16	3	SIGDA	units	Standard deviation of roll cortrol displacement after limiter
16	4	SIGDR .	units	Standard deviation of yaw control displacement after limiter
16	5	GAINDA		Gain on random component of roll control, from describing function representation of limiter
16	5	GAINDR		Gain on random component of yaw control, from describing function representation of limiter

R SEGMENT	ARRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
17	javan 1 0.75	KXS	1	Gains, damping ratios, and
17	2	ZETAXS		natural frequency for the transfer functions which
17	3	WNXS	rad/t	describe ship surge, heave, pitch, sway, roll, and yaw perturbations
17	4	KZS	2 Page 1	AGUS S
17	5	ZETAZS		
17	6	WNZS	rad/t	mails 80
17	7	KTS	rad	
17	8	ZETATS		Agricus 8 (g
17	9	WNTS	rad/t	
17	10	KYS	1	
17	11	ZETAYS		
17	12	WNYS	rad/t	
17	13	KRS	rad	
17	14	ZETARS		
17	15	WNRS	rad/t	
17	16	KPS	rad	
17	17	ZETAPS		
17	18	WNPS	rad/t	
17	19	TAUPRT	t	Time constant of first order lag. Output of this filter modifies pilots altitude command.

R ARRAY		VARIABLE UNITS	DESCRIPTION		
SEGMENT	ELEMENT	NAME	ONTIS	DESCRIPTION	
18	None	N/A	N/A	Open segment	
19	None	N/A	N/A	Open segment	
20	1-10	TABTC	rad	Dependent variable table of pitch altitude commands	
21	1-10	TRPMØL	rpm	Dependent variable table of rpm open loop inputs	
22	1-10	TCDNØL	deg	Dependent variable table of nozzle position open loop inputs	
23	1-10	TDE £ L	units	Dependent variable table of pitch control open loop inputs	
24	1-10	TABR		Dependent variable table of range commands; not currently in use	
25	1-10	TABRDØT		Dependent variable table of rate-of-closure; not currently in use	
27	1-6	ניאד		Dependent variable tables of longitudinal dimensional derivatives. Units are consistent with output values	
28	1-6	TXW			
29	1-6	TXQ			
30	1-6	TXRºM			
31	1-6	TXCDN			
32	1-6	TXPIGV			
33	1-6	TXDE			
34	1-6	TZU			
35	1-6	TZW		1	

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R ARRAY		VARIABLE	UNITE	250012		
SEGMENT	ELEMENT	NAME	UNITS	DESCRIP	ITON	
36	1-6	TZQ)	9/10/7		
37	1-6	TZRPM		97-1		
38	1-6	TZCDN				
39	1-€	TZPIGV		31-3		
40	1-6	TZDE		93-5		
41	1-6	TMU				
42	1-6	TMW		01-4		
43	1-6	TMWD				
44	1-6	TMQ		0.3		
45	1-6	TMRPM				
46	1-6	TMCON				
47	1-6	TMPIGV				
48	1-6	TMDE		76.7		
49	None	None	N/A Open s	segment		

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R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
50	varies	F		Overall system matrix
51	varies	Р		Covariance matrix
52	varies	PDØT		Covariance matrix time rate-of- change; PDØT=F*P + P*FT + GM*QM*GMT
53	varies	GM		Matrix relating external white noise disturbances to state equations
5 4 .	varies	QM		Covariance matrix of external white noise sources
55	1-50	SICMA	varies	Array of standard deviations
56	1-50	SIGMAXY	varies	Array of cross correlations with a given element (used when plotting ellipses); see subroutine MISCAL
57	1-75	VXX	1/t	Table of mean components of airwake along x ship wind axis
58	1-75	VYY	1/t	Table of mean components of airwake along y ship wind axis
59	1-75	VZZ	1/t	Table of mean component of airwake along z ship wind axis
60	1-75	SVXX	1/t	Table of standard deviation components of airwake along X ship wind axis
61	1-75	SVYY	1/t	Table of standard deviation components of airwake along Y ship wind axis
62	1-75	SVZZ	1/t	Table of standard deviation components along Z ship wind axis

R A	ARRAY	AY VARIABLE		DECONINTION					
SEGMENT	ELEMENT	NAME	UNITS	DESCRIPTION					
63	1-6	TKDEU		Dependent variable tables of pilot feedback gains. Units are consistent with previously defined output values.					
64	1-6	TKDEW		(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)					
65	1-6	TKDEQ							
66	1-6	TKDET							
67	1-6	TKDEX							
68	1-6	TKDEZ							
69	1-6	TKDEN							
70	1-6	TKDEDE							
71	1-6	TKDEDT							
72	1-6	TKDTU							
73	1-6	TKDTW							
74	1-6	TKDTQ							
75	1-6	TKDTT							
76	1-6	TKDTX							
77	1-6	TKDTZ							
78	1-6	TKDTN							
79	1-6	TKDTDE							
80	1-6	TKDTDT							
81	varies	F1		Aircraft system matrix					
82	varies	G1		Aircraft control matrix					
83	varies	GAMMA		Matrix relating colored noise inputs to aircraft					

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R A	RRAY	VARIABLE	LINITE DECORPORA
SEGMENT	ELEMENT	NAME	UNITS DESCRIPTION
84	varies	A	Colored noise shaping matrix
85	varies	В	Matrix relating white noise inputs to shaping filters
86	varies	M1	Not currently used
87	varies	M2	Not currently used
88	varies	B H	Not currently used
89	varies	D	Measurement matrix
90	varies	C	Feedback matrix operating on states in control rate equation
91	varies	RL	Feedback matrix operating on controls in control rate equation
92	varies	W	Covariance matrix of white nois external disturbances
93	varies	VU	Covariance matrix of white neuromuscular noise
94	varies	VY	Covariance matrix of white measurement noise
95	varies	VYI	Inverse of matrix VY
96	varies	S	Ship motion system matrix
97	varies	FE	System matrix for estimator covariance calculation
98	varies	QE	Covariance matrix for driving estimator covariance calculation
99	varies	PE	Covariance matrix for estimator error
100	varies	PED	Time rate-of-change of estimate error covariance matrix
101	varies	KG	Kalman gain matrix

Cont'd

R A	RRAY	VARIABLE	INITE	regionals Tealspain					
SEGMENT	GMENT ELEMENT NAME UNITS		DESCRIPTION						
102	varies	FXHAT		System matrix for estimated state covariance calculations					
103	varies	PXHAT		Estimated states covariance matrix					
104	varies	PXHATD		Time rate-of-change of estimated states covariance matrix					
105	varies	PX		State covariance matrix					
106	varies	CS		A sub matrix in F related to the modified pilot altitude command due to ship motion					

	R A	RRAY	VARIABLE	INITE	DESCRIPTION					
١,	SEGMENT	ELEMENT	NAME	UNITS						
	107	1	DEUR	1	These additional feedback gains in the optimal pilot model operate on the estimated colored noise disturbances; results of table look-up					
	107	2	DEWR	1	60 and 30 and 4					
	107	3	DEVX	1						
	107	4	DEVXD	t						
	107	5	DEVZ	1	and the second					
	107	6	DEVZD	t 1	Att Att					
	107	7	DTUR	1	900					
	107	8	DTWR	1						
	107	9	DTVX	1						
	107	10	DTVXD	<u>t</u>						
	107	11	DTVZ	1						
	107	12	DTVZD	t 1						

R . SEGMENT	ARRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION							
108	1-6	TDEUR		Dependent variable tables for pilot feedback gains. Units are consistent with the output values.							
109	1-6	TDEWR	9630	9 702							
110	1-6	TDEVX		Later to the state of the state							
111	1-6	TDEVXD									
112	1-6	TDEVZ									
113	1-6	TDEVZD									
114	1-6	TDTUR		1 10							
115	1-6	TDTWR		1 10							
116	1-6	TDTVX									
117	1-6	TDTVXD									
118	1-6	TDTVZ		0 306							
119	1-6	TDTVZD		10 21 18							
120	1-6	TYV		Dependent variable tables for lateral/directional dimensional derivatives. Units are consistent vith output values.							
121	1-6	ТҮР									
122	1-6	TYR									
123	1-6	TYDA									
124	1-6	TYDR									
125	1-6	TLV									
126	1-6	TLP									
127	1-6	TLR		•							

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R A SEGMENT	RRAY ELEMENT	VARIABLE NAME	UNITS	DESCRIPTION
128	1-6	TLDA		
129	1-6	TLDR		
130	1-6	TNV		
131	1-6	TNP		
132	1-6	TNR		
133	1-6	TNDA		
134	1-6	TNDR		
135	1-10	TABUB	1/t	Dependent variable tables of longitudinal parameters required in a lateral/directional run.
136	1-10	TABWB	1/t	
137	1-10	TXAPP	1	
138	1-10	TZAPP	1	
139	1-10	TXSP	1	
140	1-4	TDAIN	units	Independent variable table for defining roll control limiter.
141	1-4	TDAØUT	units	Dependent variable table for defining roll control limiter.
142	1-4	TDRIN	units	Independent variable table for defining yaw control limiter.
143	1-4	TDRØUT	units	Dependent variable table for defining yaw control limiter.

APPENDIX F

(contract)

LIST OF SYMBOLS

F.O LIST OF SYMBOLS

Throughout the text several equations appear in vector-matrix format. In these equations lower case letters represent vectors and upper case letters are matrices. For scalar quantities, upper case letters are nominal or mean values and lower case letters represent perturbation values. The test clearly distinguishes between variables, as to whether they are matrices, vectors, or scalars, when they are used.

Symbols |

σ

ψ, Θ, φ (˙)

(-)

(

Subscripts

0

g

Standard deviation.

Euler angles.

Time derivative of ().

Mean value of ().

Expected value of ().

Denotes reference value or condition.

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